

# PCT

## NOTIFICATION OF ELECTION

(PCT Rule 61.2)

From the INTERNATIONAL BUREAU

To:

United States Patent and Trademark  
Office  
(Box PCT)  
Crystal Plaza 2  
Washington, DC 20231  
ETATS-UNIS D'AMERIQUE

in its capacity as elected Office

Date of mailing:

03 September 1998 (03.09.98)

International application No.:

PCT/US98/03688

Applicant's or agent's file reference:

105-030PCT

International filing date:

25 February 1998 (25.02.98)

Priority date:

26 February 1997 (26.02.97)

Applicant:

FARIS, Sadeg, M. et al

1. The designated Office is hereby notified of its election made:

☒ in the demand filed with the International preliminary Examining Authority on:

08 July 1998 (08.07.98)

☐ in a notice effecting later election filed with the International Bureau on:

2. The election ☒ was

☐ was not

made before the expiration of 19 months from the priority date or, where Rule 32 applies, within the time limit under Rule 32.2(b).

The International Bureau of WIPO  
34, chemin des Colombettes  
1211 Geneva 20, Switzerland

Facsimile No.: (41-22) 740.14.35

Authorized officer:

J. Zahra

Telephone No.: (41-22) 338.83.38

## PATENT COOPERATION TREATY

## PCT

## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

(PCT Article 36 and Rule 70)

09/380256

REC'D 05 AUG 1999

WIPO

PCT

Applicant's or agent's file reference 105-030PCT	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/US98/03688	International filing date (day/month/year) 25 FEBRUARY 1998	Priority date (day/month/year) 26 FEBRUARY 1997
International Patent Classification (IPC) or national classification and IPC IPC(6): G02F 1/1335, 1/13 and US Cl.: 349/13, 14, 15, 16, 115, 117, 176		
Applicant REVEO, INC.		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.
2. This REPORT consists of a total of 4 sheets.
- ☒ This report is also accompanied by ANNEXES, i.e., sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority. (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).

These annexes consist of a total of 30 sheets.

3. This report contains indications relating to the following items:

- I ☒ Basis of the report
- II ☐ Priority
- III ☐ Non-establishment of report with regard to novelty, inventive step or industrial applicability
- IV ☐ Lack of unity of invention
- V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☐ Certain defects in the international application
- VIII ☐ Certain observations on the international application

Date of submission of the demand 08 JULY 1998	Date of completion of this report 12 JULY 1999
Name and mailing address of the IPEA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231	Authorized officer WILLIAM SIKES
Facsimile No. (703) 305-3230	Telephone No. (703) 308-0956

## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US98/03688

## I. Basis of the report

1. This report has been drawn on the basis of *(Substitute sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to the report since they do not contain amendments)*:

☐ the international application as originally filed.

☒ the description, pages (See Attached), as originally filed.

pages \_\_\_\_\_, filed with the demand.

pages \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

pages \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

☒ the claims, Nos. (See Attached), as originally filed.

Nos. \_\_\_\_\_, as amended under Article 19.

Nos. \_\_\_\_\_, filed with the demand.

Nos. \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

Nos. \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

☒ the drawings, sheets/fig (See Attached), as originally filed.

sheets/fig \_\_\_\_\_, filed with the demand.

sheets/fig \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

sheets/fig \_\_\_\_\_, filed with the letter of \_\_\_\_\_.

2. The amendments have resulted in the cancellation of:

☒ the description, pages NONE.

☒ the claims, Nos. NONE.

☒ the drawings, sheets/fig NONE.

3. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed, as indicated in the ~~Supplemental Box~~ Additional observations below (Rule 70.2(c)).

4. Additional observations, if necessary:

NONE

## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US98/03688

**V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement****1. STATEMENT**

Novelty (N)

Claims 1-101 YESClaims NONE NO

Inventive Step (IS)

Claims 1-101 YESClaims NONE NO

Industrial Applicability (IA)

Claims 1-101 YESClaims NONE NO**2. CITATIONS AND EXPLANATIONS**

Claims 1-101 meet the criteria set out in PCT Article 33(2)-(4), because the prior art does not teach or fairly suggest an electro-optical glazing structure having reflection and transmission mode of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, comprising various elements as claimed, more specifically, optical state switching means for switching the electro-optical glazing panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical glazing panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation.

----- NEW CITATIONS -----  
NONE



INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US98/03688

**Supplemental Box**

(To be used when the space in any of the preceding boxes is not sufficient)

Sheet 10

Continuation of: Boxes I - VIII

**I. BASIS OF REPORT:**

This report has been drawn on the basis of the description,  
pages, 1-92, as originally filed.  
pages, NONE, filed with the demand.  
and additional amendments:  
NONE

This report has been drawn on the basis of the claims,  
numbers, NONE, as originally filed.  
numbers, NONE, as amended under Article 19.  
numbers, NONE, filed with the demand.  
and additional amendments:  
Claims 1-101, filed with the letter of 05 April 1999

This report has been drawn on the basis of the drawings,  
sheets, 1-37, as originally filed.  
sheets, NONE, filed with the demand.  
and additional amendments:  
NONE

# PCT

## REQUEST

The undersigned requests that the present international application be processed according to the Patent Cooperation Treaty.

For receiving Office use only

09/380256

International Application No.

International Filing Date

Name of receiving Office and "PCT International Application"

Applicant's or agent's file reference  
(if desired) (12 characters maximum)

<b>Box No. I</b>	<b>TITLE OF INVENTION</b> ELECTRO-OPTICAL GLAZING STRUCTURES HAVING REFLECTION AND TRANSPARENT MODES OF OPERATION		
<b>Box No. II</b>	<b>APPLICANT</b>		
Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i>  REVEO, INC. 8 Skyline Drive Hawthorne, New York 10532 USA		<input type="checkbox"/> This person is also inventor.  Telephone No. 914-345-9555  Facsimile No. 914-345-9558  Teleprinter No.	
State (i.e. country) of nationality: US		State (i.e. country) of residence: US	
This person is applicant for the purposes of: <input type="checkbox"/> all designated States <input checked="" type="checkbox"/> all designated States except the United States of America <input type="checkbox"/> the United States of America only <input type="checkbox"/> the States indicated in the Supplemental Box			
<b>Box No. III</b>	<b>FURTHER APPLICANT(S) AND/OR (FURTHER) INVENTOR(S)</b>		
Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i>  FARIS, SADEG M. 24 Pocantico River Road Pleasantville, New York 10570 USA		This person is: <input type="checkbox"/> applicant only <input checked="" type="checkbox"/> applicant and inventor <input type="checkbox"/> inventor only <i>(If this check-box is marked, do not fill in below.)</i>	
State (i.e. country) of nationality: US		State (i.e. country) of residence: US	
This person is applicant for the purposes of: <input type="checkbox"/> all designated States <input type="checkbox"/> all designated States except the United States of America <input checked="" type="checkbox"/> the United States of America only <input type="checkbox"/> the States indicated in the Supplemental Box			
<input checked="" type="checkbox"/> Further applicants and/or (further) inventors are indicated on a continuation sheet.			
<b>Box No. IV</b>	<b>AGENT OR COMMON REPRESENTATIVE; OR ADDRESS FOR CORRESPONDENCE</b>		
The person identified below is hereby/has been appointed to act on behalf of the applicant(s) before the competent International Authorities as:		<input checked="" type="checkbox"/> agent <input type="checkbox"/> common representative	
Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i>  PERKOWSKI, THOMAS J. Soundview Plaza 1266 East Main Street Stamford, CT 06902		Telephone No. 203-357-1950  Facsimile No. 203-357-1959  Teleprinter No.	
<input type="checkbox"/> Mark this check-box where no agent or common representative is/has been appointed and the space above is used instead to indicate a special address to which correspondence should be sent.			

Continuation of Box No. III FURTHER APPLICANTS AND/OR (FURTHER) INVENTORS

If none of the following sub-boxes is used, this sheet is not to be included in the request.

<p>Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i></p> <p>LI, LE 3491 Overlook Avenue Yorktown Heights, New York 10598</p>	<p>This person is:</p> <p><input type="checkbox"/> applicant only</p> <p><input checked="" type="checkbox"/> applicant and inventor</p> <p><input type="checkbox"/> inventor only <i>(If this check-box is marked, do not fill in below.)</i></p>
--	---

State (i.e. country) of nationality: Peoples Republic of China	State (i.e. country) of residence: Peoples Republic of China
---	---

This person is applicant for the purposes of: ☐ all designated States ☐ all designated States except the United States of America ☒ the United States of America only ☐ the States indicated in the Supplemental Box

<p>Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i></p> <p>LI, JIAN-FENG Yorkridge Apartments, 8L Yorktown Heights, New York 10598</p>	<p>This person is:</p> <p><input type="checkbox"/> applicant only</p> <p><input checked="" type="checkbox"/> applicant and inventor</p> <p><input type="checkbox"/> inventor only <i>(If this check-box is marked, do not fill in below.)</i></p>
---	---

State (i.e. country) of nationality: Peoples Republic of China	State (i.e. country) of residence: Peoples Republic of China
---	---

This person is applicant for the purposes of: ☐ all designated States ☐ all designated States except the United States of America ☒ the United States of America only ☐ the States indicated in the Supplemental Box

<p>Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i></p>	<p>This person is:</p> <p><input type="checkbox"/> applicant only</p> <p><input type="checkbox"/> applicant and inventor</p> <p><input type="checkbox"/> inventor only <i>(If this check-box is marked, do not fill in below.)</i></p>
--	--

State (i.e. country) of nationality:	State (i.e. country) of residence:
--------------------------------------	------------------------------------

This person is applicant for the purposes of: ☐ all designated States ☐ all designated States except the United States of America ☐ the United States of America only ☐ the States indicated in the Supplemental Box

<p>Name and address: <i>(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)</i></p>	<p>This person is:</p> <p><input type="checkbox"/> applicant only</p> <p><input type="checkbox"/> applicant and inventor</p> <p><input type="checkbox"/> inventor only <i>(If this check-box is marked, do not fill in below.)</i></p>
--	--

State (i.e. country) of nationality:	State (i.e. country) of residence:
--------------------------------------	------------------------------------

This person is applicant for the purposes of: ☐ all designated States ☐ all designated States except the United States of America ☐ the United States of America only ☐ the States indicated in the Supplemental Box

☐ Further applicants and/or (further) inventors are indicated on another continuation sheet.

**Box N . V DESIGNATION OF STATES**

The following designations are hereby made under Rule 4.9(a) (mark the applicable check-boxes: at least one must be marked):

**Regional Patent**

- ☒ **AP ARIPO Patent:** KE Kenya, LS Lesotho, MW Malawi, SD Sudan, SZ Swaziland, UG Uganda, and any other State which is a Contracting State of the Harare Protocol and of the PCT
- ☒ **EA Eurasian Patent:** AZ Azerbaijan, BY Belarus, KZ Kazakhstan, RU Russian Federation, TJ Tajikistan, TM Turkmenistan, and any other State which is a Contracting State of the Eurasian Patent Convention and of the PCT
- ☒ **EP European Patent:** AT Austria, BE Belgium, CH and LI Switzerland and Liechtenstein, DE Germany, DK Denmark, ES Spain, FR France, GB United Kingdom, GR Greece, IE Ireland, IT Italy, LU Luxembourg, MC Monaco, NL Netherlands, PT Portugal, SE Sweden, and any other State which is a Contracting State of the European Patent Convention and of the PCT
- ☒ **OA OAPI Patent:** BF Burkina Faso, BJ Benin, CF Central African Republic, CG Congo, CI Côte d'Ivoire, CM Cameroon, GA Gabon, GN Guinea, ML Mali, MR Mauritania, NE Niger, SN Senegal, TD Chad, TG Togo, and any other State which is a member State of OAPI and a Contracting State of the PCT (if other kind of protection or treatment desired, specify on dotted line)

**National Patent (if other kind of protection or treatment desired, specify on dotted line):**

- |  |  |
|--|--|
| <input checked="" type="checkbox"/> AL Albania                               | <input checked="" type="checkbox"/> MD Republic of Moldova                       |
| <input checked="" type="checkbox"/> AM Armenia                               | <input checked="" type="checkbox"/> MG Madagascar                                |
| <input checked="" type="checkbox"/> AT Austria                               | <input checked="" type="checkbox"/> MK The former Yugoslav Republic of Macedonia |
| <input checked="" type="checkbox"/> AU Australia                             |  |
| <input checked="" type="checkbox"/> AZ Azerbaijan                            | <input checked="" type="checkbox"/> MN Mongolia                                  |
| <input checked="" type="checkbox"/> BB Barbados                              | <input checked="" type="checkbox"/> MW Malawi                                    |
| <input checked="" type="checkbox"/> BG Bulgaria                              | <input checked="" type="checkbox"/> MX Mexico                                    |
| <input checked="" type="checkbox"/> BR Brazil                                | <input checked="" type="checkbox"/> NO Norway                                    |
| <input checked="" type="checkbox"/> BY Belarus                               | <input checked="" type="checkbox"/> NZ New Zealand                               |
| <input checked="" type="checkbox"/> CA Canada                                | <input checked="" type="checkbox"/> PL Poland                                    |
| <input checked="" type="checkbox"/> CH and LI Switzerland and Liechtenstein  | <input checked="" type="checkbox"/> PT Portugal                                  |
| <input checked="" type="checkbox"/> CN China                                 | <input checked="" type="checkbox"/> RO Romania                                   |
| <input checked="" type="checkbox"/> CZ Czech Republic                        | <input checked="" type="checkbox"/> RU Russian Federation                        |
| <input checked="" type="checkbox"/> DE Germany                               | <input checked="" type="checkbox"/> SD Sudan                                     |
| <input checked="" type="checkbox"/> DK Denmark                               | <input checked="" type="checkbox"/> SE Sweden                                    |
| <input checked="" type="checkbox"/> EE Estonia                               | <input checked="" type="checkbox"/> SG Singapore                                 |
| <input checked="" type="checkbox"/> ES Spain                                 | <input checked="" type="checkbox"/> SI Slovenia                                  |
| <input checked="" type="checkbox"/> FI Finland                               | <input checked="" type="checkbox"/> SK Slovakia                                  |
| <input checked="" type="checkbox"/> GB United Kingdom                        | <input checked="" type="checkbox"/> TJ Tajikistan                                |
| <input checked="" type="checkbox"/> GE Georgia                               | <input checked="" type="checkbox"/> TM Turkmenistan                              |
| <input checked="" type="checkbox"/> HU Hungary                               | <input checked="" type="checkbox"/> TR Turkey                                    |
| <input checked="" type="checkbox"/> IS Iceland                               | <input checked="" type="checkbox"/> TT Trinidad and Tobago                       |
| <input checked="" type="checkbox"/> JP Japan                                 | <input checked="" type="checkbox"/> UA Ukraine                                   |
| <input checked="" type="checkbox"/> KE Kenya                                 | <input checked="" type="checkbox"/> UG Uganda                                    |
| <input checked="" type="checkbox"/> KG Kyrgyzstan                            | <input checked="" type="checkbox"/> US United States of America                  |
| <input checked="" type="checkbox"/> KP Democratic People's Republic of Korea |  |
| <input checked="" type="checkbox"/> KR Republic of Korea                     | <input checked="" type="checkbox"/> UZ Uzbekistan                                |
| <input checked="" type="checkbox"/> KZ Kazakhstan                            | <input checked="" type="checkbox"/> VN Viet Nam                                  |
| <input checked="" type="checkbox"/> LK Sri Lanka                             |  |
| <input checked="" type="checkbox"/> LR Liberia                               |  |
| <input checked="" type="checkbox"/> LS Lesotho                               |  |
| <input checked="" type="checkbox"/> LT Lithuania                             |  |
| <input checked="" type="checkbox"/> LU Luxembourg                            |  |
| <input checked="" type="checkbox"/> LV Latvia                                |  |

Check-boxes reserved for designating States (for the purposes of a national patent) which have become party to the PCT after issuance of this sheet:

<input type="checkbox"/>	
<input type="checkbox"/>	
<input type="checkbox"/>	
<input type="checkbox"/>	

In addition to the designations made above, the applicant also makes under Rule 4.9(b) all designations which would be permitted under the PCT except the designation(s) of \_\_\_\_\_

The applicant declares that those additional designations are subject to confirmation and that any designation which is not confirmed before the expiration of 15 months from the priority date is to be regarded as withdrawn by the applicant at the expiration of that time limit. (Confirmation of a designation consists of the filing of a notice specifying that designation and the payment of the designation and confirmation fees. Confirmation must reach the receiving Office within the 15-month time limit.)

## Box No. VI PRIORITY CLAIM

Further priority claims are indicated in the Supplemental Box ☐

The priority of the following earlier application(s) is hereby claimed:

Country (in which, or for which, the application was filed)	Filing Date (day/month/year)	Application No.	Office of filing (only for regional or international application)
item (1)  US	26/2/1997	08/805,603	
item (2)			
item (3)			

Mark the following check-box if the certified copy of the earlier application is to be issued by the Office where for the purposes of the present international application is the receiving Office (a fee may be required)

☒ The receiving Office is hereby requested to prepare and transmit to the International Bureau a certified copy of the earlier application(s) identified above as item(s) (1)

## Box No. VII INTERNATIONAL SEARCHING AUTHORITY

Choice of International Searching Authority (ISA) (If two or more International Searching Authorities are competent to carry out the international search, indicate the Authority chosen; the two-letter code may be used)

ISA / RO/US

Earlier search Fill in where a search (international, international-type or other) by the International Searching Authority has already been carried out or requested and the Authority is now requested to base the international search, to the extent possible, on the results of that earlier search. Identify such search or request either by reference to the relevant application (or the transaction thereof) or by reference to the search request.

Country (or regional Office):

Date (day/month/year):

Number:

## Box No. VIII CHECK LIST

This international application contains the following number of sheets:

1. request : 5 sheets  
 2. description : 92 sheets  
 3. claims : 27 sheets  
 4. abstract : 1 sheets  
 5. drawings : 37 sheets

Total : 132 sheets

This international application is accompanied by the item(s) marked below:

1. ☐ separate signed power of attorney  
 2. ☐ copy of general power of attorney  
 3. ☐ statement explaining lack of signature  
 4. ☐ priority document(s) identified in Box No. I, as used(s)  
 5. ☒ fee calculation sheet  
 6. ☐ separate indications concerning deposited microorganisms  
 7. ☐ nucleotide and/or amino acid sequence listing (diskette)  
 8. ☐ other (specify):

Figure No. IA of the drawings (if any) should accompany the abstract when it is published.

## Box No. IX SIGNATURE OF APPLICANT OR AGENT

Next to each signature, indicate the name of the person signing and the capacity in which the person signs. If such capacity is not obvious from reading the request:

  
 THOMAS B. PERKOWSKI, AGENT FOR APPLICANT

For receiving Office use only

1. Date of actual receipt of the purported international application:	2. Drawings:  <input type="checkbox"/> received:  <input type="checkbox"/> not received:
3. Corrected date of actual receipt due to late but timely received papers or drawings completing the purported international application:	
4. Date of timely receipt of the required corrections under PCT Article 11(2):	
5. International Searching Authority specified by the applicant: ISA	6. <input type="checkbox"/> Transmittal of search copy delayed until search fee is paid

For International Bureau use only

Date of receipt of the record copy by the International Bureau:

# PCT

## FEE CALCULATION SHEET

Annex to the Request

For receiving Office use only

International application No.

Date stamp of the receiving Office

Applicant's or agent's  
file reference

105-030PCT

Applicant

REVEO, INC.

### CALCULATION OF PRESCRIBED FEES

1. TRANSMITTAL FEE . . . . . \$230.00 T

2. SEARCH FEE . . . . . \$440.00 S

International search to be carried out by RO/US  
(If two or more International Searching Authorities are competent in relation to the international application, indicate the name of the Authority which is chosen to carry out the international search.)

### 3. INTERNATIONAL FEE

#### Basic Fee

The international application contains 162 sheets.

first 30 sheets . . . . . \$677.00 b<sub>1</sub>

132 x \$13.00 = \$1716.00 b<sub>2</sub>  
remaining sheets additional amount

Add amounts entered at b<sub>1</sub> and b<sub>2</sub> and enter total at B . . . . . \$2393.00 B

#### Designation Fees

The international application contains 74 designations.

11 x \$164.00 = \$1804.00 D  
number of designation fees amount of designation fee  
payable (maximum 11)

Add amounts entered at B and D and enter total at I . . . . . \$4197.00 I

(Applicants from certain States are entitled to a reduction of 75% of the international fee. Where the applicant is (or all applicants are) so entitled, the total to be entered at I is 25% of the sum of the amounts entered at B and D.)

4. FEE FOR PRIORITY DOCUMENT . . . . . \$15.00 P

### 5. TOTAL FEES PAYABLE

Add amounts entered at T, S, I and P, and enter total in the TOTAL box . . . . . \$4882.00  
TOTAL

☐ The designation fees are not paid at this time.

### MODE OF PAYMENT

☐ authorization to charge  
deposit account (see below)

☐ bank draft

☐ coupons

☒ cheque

☐ cash

☐ other (specify):

☐ postal money order

☐ revenue stamps

### DEPOSIT ACCOUNT AUTHORIZATION (this mode of payment may not be available at all receiving Offices)

The RO/ US ☐ is hereby authorized to charge the total fees indicated above to my deposit account.

☒ is hereby authorized to charge any deficiency or credit any overpayment in the total fees indicated above to my deposit account.

☐ is hereby authorized to charge the fee for preparation and transmittal of the priority document to the International Bureau of WIPO to my deposit account.

16-1340

25/2/1998

Deposit Account Number

Date (day/month/year)

Signature

09/380256

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/03688**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(6) : G02F 1/1335, 1/13

US CL : 349/13, 14, 15, 16, 115, 117, 176

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 349/13, 14, 15, 16, 115, 117, 176

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X — Y — A	US 4,749,261 A (MCLAUGHLIN ET AL) 07 June 1988 (07/06/88), see column 4, line 19-column 7, line 11, and column 12, lines 61-66.	83, 84, 98, 99 — 1-10, 12, 13, 15-26, 28-31, 68, 69, 70-75, 76a, 76b, 77, 79, 80, 82, 85-97 — 32-46

☒ Further documents are listed in the continuation of Box C.
 ☐ See patent family annex.

* *A* *B* *L* *O* *P*	Special categories of cited documents: document defining the general state of the art which is not considered to be of particular relevance earlier document published on or after the international filing date document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) document referring to an oral disclosure, use, exhibition or other means document published prior to the international filing date but later than the priority date claimed	*T* *X* *Y* *A*	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art document member of the same patent family
--------------------------------------	---	--------------------------	--

Date of the actual completion of the international search 07 JUNE 1998	Date of mailing of the international search report 08 JUL 1998
Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230	Authorized officer ANITA PELLMAN GROSS <i>M. Kelly</i> Telephone No. (703) 308-0956

## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US98/03688

## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y ---- A	US 5,437,811 A (DOANE ET AL) 01 August 1995 (01/08/95), see 1, line 48-column 2, line 50, column 3, lines 18-23, column 4, lines 13-21, and column 6, line 3-7.	1, 7-13, 15-17, 23-31, 68, 69, 75, 76a, 76b, 77-80, 82, 95-97, 100 ----- 32-46
Y	US 5,399,390 A (AKINS) 21 March 1995 (21/03/95), see column 5, lines 46-63.	7, 8, 13, 68, 69, 75, 76a, 80
Y	US 3,711,181 A (ADAMS, JR. ET AL) 16 January 1973 (16/01/73), see entire document, particularly the abstract.	2-6, 18-22, 70-74, 85-94
X --- Y	US 4,475,031 A (MOCKOVCIK, JR.) 02 October 1984 (02/10/1984)	1, 9, 10, 23, 25, 26, 95, 98, 99 ----- 12, 16, 79, 83, 84
Y	US 5,015,086 A (OKAUE ET AL) 14 May 1991 (14/05/91), see entire document.	11, 27, 78, 100
X,P ---- Y	US 5,686,979 A (WEBER ET AL) 11 November 1997 (11/11/97), see entire document.	1-3, 6, 9, 15-20, 23, 24, 26, 28, 30, 31, 47, 50, 51, 68, 70, 71, 76b, 82-88, 91, 95, 99 ----- 12, 29, 69, 96, 97
A	US 5,699,133 A (FURUTA) 16 December 1997 (16/12/97), see entire document.	14, 81
A	US 4,641,922 A (JACOB) 10 February 1987 (10/02/87), see entire document.	47-67



## INTERNATIONAL SEARCH REPORT

09/380256

International application No.  
PCT/US98/03688

## Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This international report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. ☐ Claims Nos.  
because they relate to subject matter not required to be searched by this Authority, namely:
2. ☒ Claims Nos.: 95  
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:  
  
Claim 95 includes a phrasing structure "of the present invention". Since the claims define the invention, a recitation of "the present invention" in the claim renders the scope of claim 95 completely undefined.
3. ☐ Claims Nos.  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort requiring an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims, it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.  
☐ No protest accompanied the payment of additional search fees.

## PATENT COOPERATION TREATY

PCT

From the INTERNATIONAL BUREAU

BEST AVAILABLE COPY

PERKOWSKI, Thomas, J.  
 Soundview Plaza  
 1266 East Main Street  
 Stamford, CT 06902  
 ETATS-UNIS D'AMERIQUE

NOTIFICATION CONCERNING  
SUBMISSION OF PRIORITY DOCUMENTS

(PCT Administrative Instructions, Section 411)

Date of mailing (day/month/year) 28 April 1998 (28.04.98)		IMPORTANT NOTIFICATION	
Applicant's reference 105-030PCT			
International application No. PCT/US98/03688	International filing date (day/month/year) 25 February 1998 (25.02.98)	Priority date (day/month/year) 26 February 1997 (26.02.97)	
Applicant REVEO, INC. et al			

The applicant is hereby notified of the date of receipt by the International Bureau of the priority document(s) relating to the following application(s):

Priority application No.	Priority date	Priority country	Date of receipt of priority document
08/805,803	26 Feb 1997 (26.02.97)	US	23 Apr 1998 (23.04.98)

THOMAS J. PERKOWSKI, ESQ., PC  
 RECEIVED ON

MAY 07 1998

Authorized officer

R. E. Stone

Telephone No. (41-22) 338.53.30

The demand must be filed directly with the competent International Preliminary Examining Authority - if two or more Authorities are competent with the one chosen by the applicant. The full name or two-letter code of that Authority may be indicated by the applicant on the line below

IPEA/ US

09/380256

PCT

CHAPTER II

DEMAND

under Article 31 of the Patent Cooperation Treaty.  
The undersigned requests that the international application specified below be the subject of international preliminary examination according to the Patent Cooperation Treaty.

For International Preliminary Examining Authority use only	
Identification of IPEA	Date of receipt of DEMAND
<b>Box No. I IDENTIFICATION OF THE INTERNATIONAL APPLICATION</b>	
Applicant's or agent's file reference 105-030PCT	
International application No. PCT/US98/03688	International filing date (day/month/year) 25 FEB 1998 (Earliest) Priority date (day/month/year) 26 FEB 1997
Title of invention ELECTRO-OPTICAL GLAZING STRUCTURES HAVING REFLECTION AND TRANSPARENT MODES OF OPERATION	
<b>Box No. II APPLICANT(S)</b>	
Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)  REVEO, INC., 8 SKYLINE DRIVE HAWTHORNE, NEW YORK 10532 US	
Telephone No.: (914) 345-9555 Facsimile No.: (914) 345-9558 Teleprinter No.:	
State (i.e. country) of nationality: US	State (i.e. country) of residence: US
Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)  FARIS, SADEG M. 24 POCANTICO RIVER ROAD PLEASANTVILLE, NEW YORK 10570 US	
State (i.e. country) of nationality: US	State (i.e. country) of residence: US
Name and address: (Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)  LI, LE 3491 OVERLOOK AVENUE YORKTOWN HEIGHTS, NEW YORK 10598 US	
State (i.e. country) of nationality: People's Republic of China	State (i.e. country) of residence: US
<input checked="" type="checkbox"/> Further applicants are indicated on a continuation sheet.	

## Continuation of Box N. II APPLICANT(S)

*If none of the following sub-boxes is used, this sheet is not to be included in the demand.*

Name and address: *(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)*

LI, JIAN-FENG  
YORKRIDGE APARTMENTS, 8L  
YORKTOWN HEIGHTS, NEW YORK 10598  
US

State (i.e. country) of nationality:

People's Republic of China

State (i.e. country) of residence:

US

Name and address: *(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)*

State (i.e. country) of nationality:

State (i.e. country) of residence:

Name and address: *(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)*

State (i.e. country) of nationality:

State (i.e. country) of residence:

Name and address: *(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)*

State (i.e. country) of nationality:

State (i.e. country) of residence:

☐ Further applicants are indicated on another continuation sheet.

**Box No. III AGENT OR COMMON REPRESENTATIVE; OR ADDRESS FOR CORRESPONDENCE**The following person is ☒ agent ☐ common representativeand ☒ has been appointed earlier and represents the applicant(s) also for international preliminary examination.☐ is hereby appointed and any earlier appointment of (an) agent(s)/common representative is hereby revoked.☐ is hereby appointed, specifically for the procedure before the International Preliminary Examining Authority, in addition to the agent(s)/common representative appointed earlier.Name and address: *(Family name followed by given name; for a legal entity, full official designation. The address must include postal code and name of country.)*PERKOWSKI, THOMAS J.  
SOUNDVIEW PLAZA  
1266 EAST MAIN STREET  
STAMFORD, CONNECTICUT 06902  
US

Telephone No.:

(203) 357-1950

Facsimile No.:

(203) 357-1959

Teleprinter No.:

☐ Mark this check-box where no agent or common representative is/has been appointed and the space above is used instead to indicate a special address to which correspondence should be sent.**Box No. IV STATEMENT CONCERNING AMENDMENTS**

The applicant wishes the International Preliminary Examining Authority\*

(i) ☒ to start the international preliminary examination on the basis of the international application as originally filed.(ii) ☐ to take into account the amendments under Article 34 of☐ the description (amendments attached).☐ the claims (amendments attached).☐ the drawings (amendments attached).(iii) ☐ to take into account any amendments of the claims under Article 19 filed with the International Bureau (a copy is attached).(iv) ☐ to disregard any amendments of the claims made under Article 19 and to consider them as reversed.(v) ☐ to postpone the start of the international preliminary examination until the expiration of 20 months from the priority date unless that Authority receives a copy of any amendments made under Article 19 or a notice from the applicant that he does not wish to make such amendments (Rule 69.1(d)). *(This check-box may be marked only where the time limit under Article 19 has not yet expired.)*

\* Where no check-box is marked, international preliminary examination will start on the basis of the international application as originally filed or, where a copy of amendments to the claims under Article 19 and/or amendments of the international application under Article 34 are received by the International Preliminary Examining Authority before it has begun to draw up a written opinion or the international preliminary examination report, as so amended.

**Box No. V ELECTION OF STATES**☒ The applicant hereby elects all eligible States *(that is, all States which have been designated and which are bound by Chapter II of the PCT)* except .....*(If the applicant does not wish to elect certain eligible States, the name(s) or country code(s) of those States must be indicated above.)*

**Box No. VI CHECKLIST**

The demand is accompanied by the following documents for the purposes of international preliminary examination:

- |  |               |
|--|---------------|
| 1. amendments under Article 34                     |               |
| description  | <u>      </u> |
| claims   | <u>      </u> |
| drawings   | <u>      </u> |
| 2. letter accompanying amendments under Article 34 | <u>      </u> |
| 3. copy of amendments under Article 19             | <u>      </u> |
| 4. copy of statement under Article 19              | <u>      </u> |
| 5. other (specify):                                | <u>      </u> |

For International Preliminary Examining Authority use only

received                      not received

<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>
<input type="checkbox"/>	<input type="checkbox"/>

The demand is also accompanied by the item(s) marked below:

- |  |  |
|--|--|
| 1. <input type="checkbox"/> separate signed power of attorney      | 4. <input checked="" type="checkbox"/> fee calculation sheet |
| 2. <input type="checkbox"/> copy of general power of attorney      | 5. <input type="checkbox"/> other (specify):                 |
| 3. <input type="checkbox"/> statement explaining lack of signature |  |

**Box No. VII SIGNATURE OF APPLICANT, AGENT OR COMMON REPRESENTATIVE**

Next to each signature, indicate the name of the person signing and the capacity in which the person signs (if such capacity is not obvious from reading the demand).

Thomas J. Perkowsky, Esq.  
Thomas J. Perkowsky, Esq., agent for Applicants

For International Preliminary Examining Authority use only

1. Date of actual receipt of DEMAND:
2. Adjusted date of receipt of demand due to CORRECTIONS under Rule 60.1(b):
3. ☐ The date of receipt of the demand is AFTER the expiration of 19 months from the priority date and item 4 or 5, below, does not apply. ☐ The applicant has been informed accordingly.
4. ☐ The date of receipt of the demand is WITHIN the period of 19 months from the priority date as extended by virtue of Rule 80.5.
5. ☐ Although the date of receipt of the demand is after the expiration of 19 months from the priority date, the delay in arrival is EXCUSED pursuant to Rule 82.

For International Bureau use only


Demand received from IPEA on:

## PCT

## FEE CALCULATION SHEET

Sheet 5 of 5

Annex to the Demand for international preliminary examination

<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; padding: 5px;"> International application No. <b>FCT/US98/03688</b> </td> <td style="width: 50%; padding: 5px;"> For International Preliminary Examining Authority use only </td> </tr> <tr> <td style="padding: 5px;"> Applicant's or agent's file reference <b>105-030PCT</b> </td> <td style="padding: 5px;"> Date stamp of the IPEA </td> </tr> </table>	International application No. <b>FCT/US98/03688</b>	For International Preliminary Examining Authority use only	Applicant's or agent's file reference <b>105-030PCT</b>	Date stamp of the IPEA									
International application No. <b>FCT/US98/03688</b>	For International Preliminary Examining Authority use only												
Applicant's or agent's file reference <b>105-030PCT</b>	Date stamp of the IPEA												
Applicant <b>Reveo, Inc.; Sadeg M. Faris; Le Li, Jian-Feng Li</b>													
<b>Calculation of prescribed fees</b> <table style="width: 100%; margin-top: 20px;"> <tr> <td style="width: 60%;">1. Preliminary examination fee .....</td> <td style="width: 20%; text-align: right;">\$490.00</td> <td style="width: 20%; text-align: center; border: 1px solid black;">P</td> </tr> <tr> <td>2. Handling fee (<i>Applicants from certain States are entitled to a reduction of 5% of the handling fee. Where the applicant is (or all applicants are) so entitled, the amount to be entered at H is 25% of the handling fee.</i>) .....</td> <td style="text-align: right;">\$162.00</td> <td style="text-align: center; border: 1px solid black;">H</td> </tr> <tr> <td>3. Total of prescribed fees Add the amounts entered at P and H and enter total in the TOTAL box .....</td> <td style="text-align: right; border: 1px solid black;">\$652.00</td> <td></td> </tr> <tr> <td></td> <td style="text-align: center; border: 1px solid black;">TOTAL</td> <td></td> </tr> </table>		1. Preliminary examination fee .....	\$490.00	P	2. Handling fee ( <i>Applicants from certain States are entitled to a reduction of 5% of the handling fee. Where the applicant is (or all applicants are) so entitled, the amount to be entered at H is 25% of the handling fee.</i> ) .....	\$162.00	H	3. Total of prescribed fees Add the amounts entered at P and H and enter total in the TOTAL box .....	\$652.00			TOTAL	
1. Preliminary examination fee .....	\$490.00	P											
2. Handling fee ( <i>Applicants from certain States are entitled to a reduction of 5% of the handling fee. Where the applicant is (or all applicants are) so entitled, the amount to be entered at H is 25% of the handling fee.</i> ) .....	\$162.00	H											
3. Total of prescribed fees Add the amounts entered at P and H and enter total in the TOTAL box .....	\$652.00												
	TOTAL												
<b>Mode of Payment</b> <table style="width: 100%; margin-top: 10px;"> <tr> <td><input checked="" type="checkbox"/> authorization to charge deposit account with the IPEA (see below)</td> <td><input type="checkbox"/> cash</td> </tr> <tr> <td><input checked="" type="checkbox"/> cheque</td> <td><input type="checkbox"/> revenue stamps</td> </tr> <tr> <td><input type="checkbox"/> postal money order</td> <td><input type="checkbox"/> coupons</td> </tr> <tr> <td><input type="checkbox"/> bank draft</td> <td><input type="checkbox"/> other (specify):</td> </tr> </table>		<input checked="" type="checkbox"/> authorization to charge deposit account with the IPEA (see below)	<input type="checkbox"/> cash	<input checked="" type="checkbox"/> cheque	<input type="checkbox"/> revenue stamps	<input type="checkbox"/> postal money order	<input type="checkbox"/> coupons	<input type="checkbox"/> bank draft	<input type="checkbox"/> other (specify):				
<input checked="" type="checkbox"/> authorization to charge deposit account with the IPEA (see below)	<input type="checkbox"/> cash												
<input checked="" type="checkbox"/> cheque	<input type="checkbox"/> revenue stamps												
<input type="checkbox"/> postal money order	<input type="checkbox"/> coupons												
<input type="checkbox"/> bank draft	<input type="checkbox"/> other (specify):												
<b>Deposit Account Authorization</b> ( <i>this mode of payment may not be available at all IPEAs</i> ) The IPEA: <u>US</u> <input type="checkbox"/> is hereby authorized to charge the total fees indicated above to my deposit account.  <input checked="" type="checkbox"/> ( <i>this check-box may be marked only if the conditions for deposit accounts of the IPEA so permit</i> ) is hereby authorized to charge any deficiency or credit any overpayment in the total fees indicated above to my deposit account.													
16-1340 Deposit Account Number	08 July 1998 Date (day/month/year)												
<div style="text-align: right;">   Signature </div>													

## PATENT COOPERATION TREATY

09/380256

From the  
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

PCT

NOTIFICATION OF RECEIPT  
OF DEMAND(PCT Rule 61.1(b), first sentence  
and Administrative Instructions, Section 601)

To:	THOMAS J. PERKOWSKI, ESQ., P.C. RECEIVED ON AUG 07 1998
THOMAS J. PERKOWSKI SOUNDVIEW PLAZA 1266 EAST MAIN STREET STAMFORD CT 06902	

Date of mailing  
(day/month/year)

04 AUG 1998

Applicant's or agent's file reference  
105-030PCT

## IMPORTANT NOTIFICATION

International application No.  
PCT/US98/03688International filing date (day/month/year)  
25 FEB 98Priority date (day/month/year)  
26 FEB 97

Applicant

REVEO, INC.

1. The applicant is hereby notified that this International Preliminary Examining Authority considers the following date as the date of receipt of the demand for international preliminary examination of the international application:

08 JUL 1998

2. This date of receipt is:



the actual date of receipt of the demand.



the date on which the proper corrections to the demand were timely received.

3. ☐ This date is AFTER the expiration of 19 months from the priority date.

**Attention:** The election(s) made in the demand does (do) not have the effect of postponing the commencement of the national phase until 30 months from the priority date (or later in some Offices) (Article 39(1)). Therefore, the acts for entry into the national phase must be performed within 20 months from the priority date (or later in some Offices) (Article 22).

For details, see Annex B to Form PCT/IB/301 sent by the International Bureau and Volume II of the PCT Applicant's Guide.



This notification confirms the information given in person or by telephone on:

4. Only where paragraph 3 applies, a copy of this notification has been sent to the International Bureau.

Name and mailing address of the IPEA/US Assistant Commissioner for Patents Box PCT Washington, D.C. 20231 Facsimile No.	Attn: IPEA/US	Authorized Office PCT/Internat'l Appl Processing Div (703) 305-3664 Telephone No.
---	---------------	--



# PATENT COOPERATION TREATY 09/380256

From the  
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

## PCT

### WRITTEN OPINION

(PCT Rule 66)

To: THOMAS J. PERKOWSKI  
SOUNDVIEW PLAZA  
1266 EAST MAIN STREET  
STAMFORD, CT 06902

THOMAS J. PERKOWSKI ESQ. P.C.  
RECEIVED

MAR 08 1999

Date of Mailing  
(day/month/year)

04 MAR 1999

Applicant's or agent's file reference  
105-030PCT

**REPLY DUE**

within ONE months  
from the above date of mailing

International application No.  
PCT/US98/03688

International filing date (day/month/year)  
25 FEBRUARY 1998

Priority date (day/month/year)  
26 FEBRUARY 1997

International Patent Classification (IPC) or both national classification and IPC  
IPC(6): G02F 1/1335, 1/13 and US Cl.: 349/13, 14, 15, 16, 115, 117, 176

Applicant  
REVEO, INC.

1. This written opinion is the first (first, etc.) drawn by this International Preliminary Examining Authority.

2. This opinion contains indications relating to the following items:

- I ☒ Basis of the opinion
- II ☐ Priority
- III ☐ Non-establishment of opinion with regard to novelty, inventive step or industrial applicability
- IV ☐ Lack of unity of invention
- V ☒ Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☒ Certain defects in the international application
- VIII ☐ Certain observations on the international application

3. The applicant is hereby invited to reply to this opinion.

**When?** See the time limit indicated above. ~~The applicant may, before the expiration of that time limit, request this Authority to grant an extension, see Rule 66.2(d).~~

**How?** By submitting a written reply, accompanied, where appropriate, by amendments, according to Rule 66.3. For the form and the language of the amendments, see Rules 66.8 and 66.9.

**Also** For an additional opportunity to submit amendments, see Rule 66.4.  
For the examiner's obligation to consider amendments and/or arguments, see Rule 66.4 *bis*.  
For an informal communication with the examiner, see Rule 66.6.

**If no reply is filed**, the international preliminary examination report will be established on the basis of this opinion.

4. The final date by which the international preliminary examination report must be established according to Rule 69.2 is: 26 JUNE 1999

Name and mailing address of the IPEA/US  
Commissioner of Patents and Trademarks  
Box PCT  
Washington, D.C. 20231

Facsimile No. (703) 305-3230

Authorized officer

WILLIAM SIKES

Telephone No. (703) 308-0956

WRITTEN OPINION

International application No.

PCT/US98/03688

I. Basis of the opinion

1. This opinion has been drawn on the basis of (*Substitute sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this opinion as "originally filed"*):

☒ the international application as originally filed.

☒ the description, pages 1-92, as originally filed.

pages NONE, filed with the demand.

pages NONE, filed with the letter of \_\_\_\_\_.

☒ the claims, Nos. 1-100, as originally filed.

Nos. NONE, as amended under Article 19.

Nos. NONE, filed with the demand.

Nos. NONE, filed with the letter of \_\_\_\_\_.

☒ the drawings, sheets/~~fig~~ 1-37, as originally filed.

sheets/~~fig~~ NONE, filed with the demand.

sheets/~~fig~~ NONE, filed with the letter of \_\_\_\_\_.

2. The amendments have resulted in the cancellation of:

☒ the description, pages NONE

☒ the claims, Nos. NONE

☒ the drawings, sheets/~~fig~~ NONE

3. ☐ This opinion has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed, as indicated in the ~~Supplemental Box~~ Additional observations below (Rule 70.2(c)).

4. Additional observations, if necessary:

NONE

WRITTEN OPINION

International application No.

PCT/US98/03688

**V. Reasoned statement under Rule 66.2(a)(ii) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement**

**1. STATEMENT**

Novelty (N)	Claims	<u>32-67, 81</u>	YES
	Claims	<u>1-31, 68-80, 82-100</u>	NO
Inventive Step (IS)	Claims	<u>32-67, 81</u>	YES
	Claims	<u>1-31, 68-80, 82-100</u>	NO
Industrial Applicability (IA)	Claims	<u>NONE</u>	YES
	Claims	<u>NONE</u>	NO

**2. CITATIONS AND EXPLANATIONS**

Claims 83-84, 98-99 lack novelty under PCT Article 33(2) as being anticipated by MCLAUGHLIN ET AL (PN 4,749,261.).

MCLAUGHLIN ET AL teach in col. 4, line 19 to col. 7, line 11 and col. 12, lines 61-66 a window which may be used in an automobile or a building and may maximize infrared light reflectivity, visible light transmissivity, and light scattering. The window reduces glare and heat upon passengers and also provides privacy for passengers. The window includes a frame which supports a battery, an electric circuit, and a photodetector and is formed of a polymer dispersed liquid crystal.

Claims 1, 9-10, 23, 25-26, 95, 98-99 lack novelty under PCT Article 33(2) as being anticipated by MOCKOVCIK, JR. (PN 4,475,031).

MOCKOVCIK, JR. teach a solar-powered sun sensitive window made up of liquid nematic crystals between two transparent conductors which is powered directly by a solar cell, comprising a solar power source, a voltage regulator means. This window reduces the transparency of the window, resulting in a constant intensity behind the window.

Claims 1, 7-17, 23-31, 68-69, 75-80, 82, 95-97 and 100 lack an inventive step under PCT Article 33(3) as being obvious over MCLAUGHLIN ET AL in view of DOANE ET AL (PN 5,437,811).

DOANE ET AL teach in col. 1, line 48 to col. 2, line 50, col. 3, lines 18-23, col. 4, lines 13-21 and col. 6, lines 3-7 that windows made of polymer dispersed liquid crystal have an increased haze at oblique angles. Chiral nematic liquid crystal, on the other hand, exhibits minimal haze at all angles, may reflect various colors thereby providing a greyscale or alternatively may reflect light outside the visible spectrum, and is multistable. Accordingly, it would have been obvious to substitute chiral nematic liquid crystal material for the polymer dispersed liquid crystal of MCLAUGHLIN ET AL for increased transmissivity in the clear state, for better reflection of (Continued on Supplemental Sheet.)

WRITTEN OPINION

International application No.

PCT/US98/03688

**VII. Certain defects in the international application**

The following defects in the form or contents of the international application have been noted:

Claims 76-100 are objected to under PCT Rule 66.2(a)(iii) as containing the following defect(s) in the form or contents thereof:  
There are two claims numbered 76 which have treated as separate claims. Claim 77 is seen as dependent upon the second claim 76.

**Supplemental Box**

(To be used when the space in any of the preceding boxes is not sufficient)

Continuation of: Boxes I - VIII

Sheet 10

**TIME LIMIT:**

The time limit set for response to a Written Opinion may not be extended. 37 CFR 1.484(d). Any response received after the expiration of the time limit set in the Written Opinion will not be considered in preparing the International Preliminary Examination Report.

**V. 2. REASONED STATEMENTS - CITATIONS AND EXPLANATIONS (Continued):**

infrared light as well as visible light when privacy is desired, and for stability for the various states.

Since chiral nematic liquid crystal reflects light within a specific wavelength band depending on the pitch of the material, for reflection of visible light and infrared light, it would have been obvious to include two panels, one of which reflects infrared and the other of which reflects visible light.

Claim 29 lacks an inventive step under PCT Article 33(3) as being obvious over MCLAUGHLIN ET AL in view of DOANE ET AL as applied 1, 7-17, 23-31, 68-69, 75-80, 82, 95-97 and 100 in the immediately preceding paragraph and further in view of AKINS (PN 5,399,390).

AKINS teaches in col. 5, lines 46-63 that two cholesteric liquid crystal cells of opposite intrinsic rotatory sense should be stacked, so that all light rather than just light of a particular rotatory sense may be reflected or transmitted, to improve brightness and contrast. Accordingly, to vary the window of MCLAUGHLIN ET AL, as modified by the teachings of DOANE ET AL, from highly transmissive to highly reflective, it would have been obvious to use two stacked cholesteric liquid crystal cells of opposite rotatory sense.

Claims 2-6, 18-22, 70-74, 85-94 lack an inventive step under PCT Article 33(3) as being obvious over MCLAUGHLIN ET AL in view of ADAMS, JR. ET AL (PN 3,711,181).

MCLAUGHLIN ET AL teach a liquid crystal window that reflects light including infrared light for privacy and for reducing heat transmitted through the window, as described above.

ADAMS ET AL teach in the abstract, to transmit light at substantially all wavelengths while simultaneously rejecting radiation at a single wavelength band, two optically negative liquid crystal films which are the same in intrinsic rotatory sense and a means for converting circularly polarized light of one sense to the other sense are used. ADAMS ET AL show in Figure 2, that the circular polarization converter is between the two circular polarizers and describe in col. 8, lines 49-56, that it can be an electro-optic half wave plate. Thus, for maximum transmission of visible light with complete reflection of infrared light to reduce the heat transmitted through the window, a goal of MCLAUGHLIN ET AL, it would have been obvious to use an active  $\Pi$ -phase retarder between two cholesteric liquid crystal polarizers of the same intrinsic rotatory sense in place of the polymer dispersed liquid crystal of MCLAUGHLIN ET AL in view of ADAMS, JR. ET AL.

Claims 11, 27, 78 and 100 lack an inventive step under PCT Article 33(3) as being obvious over OKAUE ET AL in view of DOANE ET AL (PN 5,437,811).

OKAUE ET AL teach in embodiment 1, a pair of electronic sunglasses with lenses formed of liquid crystal material between two polarizers. The polarizers absorb light in the light blocking mode. DOANE ET AL teach in col. 1, line 48 to col. 2, line 50, and col. 3, lines 18-23 that chiral nematic liquid crystal may reflect various colors thereby providing a greyscale or alternatively may reflect light outside the visible spectrum, does not require polarizers thereby increasing the brightness and decreasing the heat absorbed, and is multistable. Therefore, it would have been obvious to substitute chiral nematic liquid crystal material for the twisted nematic liquid crystal/polarizer combination of OKAUE ET AL to increase the transmittance of light, provide a greyscale for varying degrees of brightness, and decrease the heat absorbed by the glasses.

----- NEW CITATIONS -----

NONE

## PATENT COOPERATION TREATY

01/180250

From the  
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

09/380256

PCT

To: THOMAS J. PERKOWSKI  
SOUNDVIEW PLAZA  
1266 EAST MAIN STREET  
STAMFORD, CT 06902

THOMAS J PERKOWSKI, ESQ., P.  
RECEIVED ON

AUG 04 1999

NOTIFICATION OF TRANSMITTAL OF  
INTERNATIONAL PRELIMINARY  
EXAMINATION REPORT

(PCT Rule 71.1)

Date of Mailing  
(day/month/year)

02 AUG 1999

Applicant's or agent's file reference

105-030PCT

## IMPORTANT NOTIFICATION

International application No.

PCT/US98/03688

International filing date (day/month/year)

25 FEBRUARY 1998

Priority Date (day/month/year)

26 FEBRUARY 1997

Applicant

REVEO, INC.

1. The applicant is hereby notified that this International Preliminary Examining Authority transmits herewith the international preliminary examination report and its annexes, if any, established on the international application.
2. A copy of the report and its annexes, if any, is being transmitted to the International Bureau for communication to all the elected Offices.
3. Where required by any of the elected Offices, the International Bureau will prepare an English translation of the report (but not of any annexes) and will transmit such translation to those Offices.

## 4. REMINDER

The applicant must enter the national phase before each elected Office by performing certain acts (filing translations and paying national fees) within 30 months from the priority date (or later in some Offices)(Article 39(1))(see also the reminder sent by the International Bureau with Form PCT/IB/301).

Where a translation of the international application must be furnished to an elected Office, that translation must contain a translation of any annexes to the international preliminary examination report. It is the applicant's responsibility to prepare and furnish such translation directly to each elected Office concerned.

For further details on the applicable time limits and requirements of the elected Offices, see Volume II of the PCT Applicant's Guide.

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# PATENT COOPERATION TREATY

From the  
INTERNATIONAL PRELIMINARY EXAMINING AUTHORITY

To: THOMAS J. PERKOWSKI  
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THOMAS J. PERKOWSKI, ESQ., PC  
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AUG 04 1999

## PCT

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## PATENT COOPERATION TREATY

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## INTERNATIONAL PRELIMINARY EXAMINATION REPORT AUG 04 1999

(PCT Article 36 and Rule 70)

Applicant's or agent's file reference 105-030PCT	FOR FURTHER ACTION See Notification of Transmittal of International Preliminary Examination Report (Form PCT/IPEA/416)	
International application No. PCT/US98/03688	International filing date (day/month/year) 25 FEBRUARY 1998	Priority date (day/month/year) 26 FEBRUARY 1997
International Patent Classification (IPC) or national classification and IPC IPC(6): G02F 1/1335, 1/13 and US Cl.: 349-13, 14, 15, 16, 115, 117, 176		
Applicant REVEO, INC.		

1. This international preliminary examination report has been prepared by this International Preliminary Examining Authority and is transmitted to the applicant according to Article 36.
2. This REPORT consists of a total of 4 sheets.
- ☒ This report is also accompanied by ANNEXES, i.e., sheets of the description, claims and/or drawings which have been amended and are the basis for this report and/or sheets containing rectifications made before this Authority. (see Rule 70.16 and Section 607 of the Administrative Instructions under the PCT).
- These annexes consist of a total of 30 sheets.

## 3. This report contains indications relating to the following items:

- I ☒ Basis of the report
- II ☐ Priority
- III ☐ Non-establishment of report with regard to novelty, inventive step or industrial applicability
- IV ☐ Lack of unity of invention
- V ☒ Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement
- VI ☐ Certain documents cited
- VII ☐ Certain defects in the international application
- VIII ☐ Certain observations on the international application

Date of submission of the demand 08 JULY 1998	Date of completion of this report 12 JULY 1999
Name and mailing address of the IPPTA Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231	Authorized officer WILLIAM SIKES
Facsimile No. (703) 305-3230	Telephone No. (703) 308-0956



## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US98/03688

**I. Basis of the report**

1. This report has been drawn on the basis of *(Substitute sheets which have been furnished to the receiving Office in response to an invitation under Article 14 are referred to in this report as "originally filed" and are not annexed to the report since they do not contain amendments)*:

- ☐ the international application as originally filed.
- ☒ the description, pages (See Attached) , as originally filed.  
pages \_\_\_\_\_ , filed with the demand.  
pages \_\_\_\_\_ , filed with the letter of \_\_\_\_\_  
pages \_\_\_\_\_ , filed with the letter of \_\_\_\_\_
- ☒ the claims, Nos. (See Attached) , as originally filed.  
Nos. \_\_\_\_\_ , as amended under Article 19.  
Nos. \_\_\_\_\_ , filed with the demand.  
Nos. \_\_\_\_\_ , filed with the letter of \_\_\_\_\_  
Nos. \_\_\_\_\_ , filed with the letter of \_\_\_\_\_
- ☒ the drawings, sheets/fig (See Attached) , as originally filed.  
sheets/fig \_\_\_\_\_ , filed with the demand.  
sheets/fig \_\_\_\_\_ , filed with the letter of \_\_\_\_\_  
sheets/fig \_\_\_\_\_ , filed with the letter of \_\_\_\_\_

2. The amendments have resulted in the cancellation of:

- ☒ the description, pages NONE
- ☒ the claims, Nos. NONE
- ☒ the drawings, sheets/fig NONE

3. ☐ This report has been established as if (some of) the amendments had not been made, since they have been considered to go beyond the disclosure as filed, as indicated in the ~~Supplemental Box~~ Additional observations below (Rule 70.2(c)).

4. Additional observations, if necessary:

NONE

## INTERNATIONAL PRELIMINARY EXAMINATION REPORT

International application No.

PCT/US98/03688

**V. Reasoned statement under Article 35(2) with regard to novelty, inventive step or industrial applicability; citations and explanations supporting such statement****1. STATEMENT**

Novelty (N)	Claims <u>1-101</u>	YES
	Claims <u>NONE</u>	NO
Inventive Step (IS)	Claims <u>1-101</u>	YES
	Claims <u>NONE</u>	NO
Industrial Applicability (IA)	Claims <u>1-101</u>	YES
	Claims <u>NONE</u>	NO

**2. CITATIONS AND EXPLANATIONS**

Claims 1-101 meet the criteria set out in PCT Article 33(2)-(4), because the prior art does not teach or fairly suggest an electro-optical glazing structure having reflection and transmission mode of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, comprising various elements as claimed, more specifically, optical state switching means for switching the electro-optical glazing panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical glazing panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation.

----- NEW CITATIONS -----  
NONE

**Supplemental B x**

(To be used when the space in any of the preceding boxes is not sufficient)

Continuation of: Boxes I - VIII

Sheet 10

**I. BASIS OF REPORT:**

This report has been drawn on the basis of the description.  
pages, 1-92, as originally filed.  
pages, NONE, filed with the demand.  
and additional amendments:  
NONE

This report has been drawn on the basis of the claims,  
numbers, NONE, as originally filed.  
numbers, NONE, as amended under Article 19.  
numbers, NONE, filed with the demand.  
and additional amendments:  
Claims 1-101, filed with the letter of 05 April 1999

This report has been drawn on the basis of the drawings,  
sheets, 1-37, as originally filed.  
sheets, NONE, filed with the demand.  
and additional amendments:  
NONE

CLAIMS TO INVENTION

1. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, said electro-optical glazing structure comprising:

an electro-optical glazing panel of laminated construction, having first and second optical states of operation; and

optical state switching means for switching said electro-optical glazing panel to said first optical state of operation in order to induce said electro-optical glazing structure into said reflection mode of operation, and for switching said electro-optical glazing panel to said second optical state of operation in order to induce said electro-optical glazing structure into said transmission mode of operation.

2. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

a second electrically-passive CLC electromagnetic radiation polarizing panel;

and

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

3. The electro-optical glazing structure of claim 2, wherein said first and second electrically-passive CLC electromagnetic radiation polarizing

panels reflect electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having a second circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels reflect or transmit without absorption electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

4. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

a second electrically-active CLC electromagnetic radiation polarizing panel; and

an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

5. The electro-optical glazing structure of claim 4, wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels reflect electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel

IPEA/US 05 APR 1999

is switched to said first optical state of operation, wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having either a right hand a second circularly polarized state and/or a wavelength outside said first prespecified bandwidth when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

6. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

first and a second electrically passive single layer electromagnetic radiation polarizing panels; and

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive electromagnetic radiation polarizing panels.

7. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC electromagnetic radiation polarizing panel.

8. The electro-optical glazing structure of claim 7,

wherein said first electrically-active CLC electromagnetic radiation polarizing panel reflects electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation, and

wherein said first electrically-active CLC electromagnetic radiation polarizing panel transmits electromagnetic radiation having a second circularly polarized (RHCP) state when said electro-optical glazing panel is switched to said first optical state of operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel reflects electromagnetic radiation having said second state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits electromagnetic radiation having said first state when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit more than 50% of electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

9. The electro-optical glazing structure of claim 1, which further comprises:

a window frame for mounting said electro-optical glazing panel within a house or office building, or aboard a transportation vehicle.

10. The electro-optical glazing structure of claim 9, which further comprises:

a electromagnetic-sensor mounted on said window frame, for sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said window frame, for recharging the battery;

electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

a programmable micro-computer chip mounted within said window frame, for controlling the operation of said battery recharger and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

11. The electro-optical glazing structure of claim 1, further comprising:  
a frame for an intelligent pair of sunglasses; and

a pair of said optical glazing elements supported within said frame,

wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

12. An intelligent window system for dynamic electromagnetic radiation control which comprises:

a plurality of said electro-optical glazing structures of claim 10,



each mounted within a house or office building, or aboard a transportation vehicle; and

a central control computer for coordinating the operation of said electro-optical glazing structures.

13. A composite electro-optical glazing structure which comprises:

a plurality of said electro-optical glazing structures of claim 1, stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than two said optical states of operation which permit complex levels of electromagnetic radiation control.

14. A stereoscopic 3-D viewing device in the form of eyeglasses, comprising:

a pair of optical elements positionable before the eyes of a user of said eyeglasses, each said optical element including said electro-optical glazing structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of real world objects.

15. An electro-optical glazing structure which has high reflection, semi-transparent and greater than 50% transparent modes of operation for improved control over the flow of electromagnetic radiation within the solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

16. A reflective electro-optical glazing structure, in which the modes of

operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

17. The electro-optical glazing structure of claim 1, wherein the transmission of the visible portion of the electromagnetic spectrum is controlled and wherein the IR portion of the electromagnetic spectrum is reflected.

18. An electro-optical glazing structure, comprising an electrically-active phase retardation panel interposed between a pair of single layer electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first linear polarization state, whereby a highly reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

19. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a first and a second electrically-passive electromagnetic radiation polarizing panel, the first panel reflecting electromagnetic radiation of a first linear polarization state, the second panel reflecting electromagnetic radiation of a second linear polarization state, whereby a reflective state of operation and a semi-transparent state of operation are provided over a region of the electromagnetic spectrum.

20. The electro-optical glazing structure of claim 19, wherein the first and a second electrically-passive electromagnetic radiation polarizing panels are single layer polarizing panels.

21. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

22. An electro-optical glazing structure, comprising a pair of electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of a first circularly polarized state and the other of which is capable of reflecting electromagnetic radiation of a second circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

23. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the transmission and reflection of electromagnetic radiation, can be dynamically controlled over a broad-band region of the electromagnetic spectrum, from greater than 50% transmission to high reflection.

24. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the electromagnetic radiation over the IR region of the electromagnetic spectrum can be reflected, rather than absorbed, reducing the

temperature cycle range which the window structure is required to undergo.

25. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure of claim 1 is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within the programmed microcontroller.

26. The electro-optical glazing structure of claim 1 which is designed for integration within the heating/cooling system of a house, office building, factory or vehicle in order to control the flow of broad-band electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

27. An intelligent pair of shutter glasses, in which each optical element is realized using an electro-optical glazing structure of claim 1 fashioned to the dimensions of a shutter glass frame.

28. The electro-optic glazing structure of claim 1, further comprising:

a reflecting layer for reflecting infrared light, wherein the electro-optic glazing structure of claim 1 controls the transmission and reflection of visible light.

29. The electro-optic glazing structure of claim 1, further comprising:

a reflecting layer for reflecting UV light, wherein the electro-optic glazing structure of claim 1 controls the transmission and reflection of visible light.

30. The electro-optic glazing structure of claim 1, further comprising:

a electro-optic glazing structure which controls the transmission and reflection of IR light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of visible light.

31. The electro-optic glazing structure of claim 1, further comprising:

a electro-optic glazing structure which controls the transmission and reflection of visible light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of IR light.

32. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, the electro-optical glazing structure comprising:

an electro-optical panel of multilayer construction, having first and second optical states of operation;

optical state switching means for switching the electro-optical panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation, and

means for further controlling electromagnetic radiation incident on the electro-optical panel.

33. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a means for reflecting circularly polarized light.

34. The electro-optical glazing structure of claim 33, wherein the means for reflecting circularly polarized light comprise a cholesteric liquid crystal (CLC) reflector.

35. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a scattering layer for controllably scattering light.

36. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

37. The electro-optical glazing structure of claim 36x, wherein the anisotropically shaped objects are micron size sheets of reflecting

material.

38. The electro-optical glazing structure of claim 37, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

39. The electro-optical glazing structure of claim 37, wherein the micron size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

40. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a polymerized polymer region containing a large plurality of inclusions of liquid crystal material.

41. The electro-optical glazing structure of claim 40, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

42. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

43. The electro-optical glazing structure of claim 42, wherein the scattering layer may be made non scattering under the influence of an electric field.

44. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a

mixture of a polymer and a liquid crystal material.

45. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material is transparent to the electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

46. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material reflects a portion of the electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

47. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, the electromagnetic radiation having a first and a second linear polarization, the electro-optical glazing structure comprising:

an electro-optical panel having first and second optical states of operation; and

optical state switching means for switching the electro-optical panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation,

wherein the electro-optical panel comprises:

a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference between the



materials in each layer of the pair, the difference being in the index of refraction for electromagnetic radiation having the first linear polarization, wherein there is little difference in the index of refraction for electromagnetic radiation having the second linear polarization, the total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

48. The electro-optical glazing structure of claim 47, wherein the electro-optical panel further reflects circularly polarized electromagnetic radiation.

49. The electro-optical glazing structure of claim 48, wherein the electro-optical panel comprises a cholesteric liquid crystal (CLC) material.

50. The electro-optical glazing structure of claim 47, wherein the electro-optical panel selectively transmits and reflects electromagnetic radiation of a first bandwidth of the EM spectrum, further comprising a reflector of EM radiation which reflects radiation in a second bandwidth of the EM spectrum, the reflector of EM radiation comprising a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction between the materials in each layer of the pair.

51. The electro-optical glazing structure of claim 50, wherein the reflector of EM radiation comprises a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction between the materials in

each layer of the pair. The total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

52. The electro-optical glazing structure of claim 47, further comprising a controllable scattering layer.

53. The electro-optical glazing structure of claim 52, wherein the controllable scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

54. The electro-optical glazing structure of claim 47, wherein electrooptic panel further comprises a means for reflecting circularly polarized light.

55. The electro-optical glazing structure of claim 54, wherein the means for reflecting circularly polarized light comprise a cholesteric liquid crystal (CLC) reflector.

56. The electro-optical glazing structure of claim 47, wherein the electro-optic panel further comprises a scattering layer for controllably scattering light.

57. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

58. The electro-optical glazing structure of claim 57, wherein the anisotropically shaped objects are micron size sheets of reflecting material.

59. The electro-optical glazing structure of claim 58, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

60. The electro-optical glazing structure of claim 58, wherein the micron size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

61. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a polymerized polymer region containing a large plurality of inclusions of liquid crystal material.

62. The electro-optical glazing structure of claim 61, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

63. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

64. The electro-optical glazing structure of claim 63, wherein the scattering layer may be made non scattering under the influence of an electric field.

65. The electro-optical glazing structure of claim 47, wherein the electro-optical panel further comprises a layer of a mixture of a polymer and a liquid crystal material.

66. The electro-optical glazing structure of claim 65, wherein the mixture of polymer and liquid crystal material is transparent to the electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

67. The electro-optical glazing structure of claim 65, wherein the mixture of polymer and liquid crystal material reflects a portion of the electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

68. An electro-optical glazing structure having total-reflection and total-transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation without absorption, respectively, said electro-optical glazing comprising:

an electro-optical panel of laminated construction, having first and second optical states of operation; and

optical state switching means for switching said electro-optical panel to said first optical state of operation in order to induce said electro-optical glazing into said total-reflection mode of operation, and for switching said electro-optical panel to said second optical state of operation in order to induce said electro-optical glazing into said total-transmission mode of operation,

wherein electromagnetic radiation within a first prespecified

bandwidth falling incident upon said electro-optical panel is totally reflected from said electro-optical panel without absorption when said electro-optical panel is switched to said first optical state of operation, and

wherein electromagnetic radiation within a second prespecified bandwidth falling incident upon said electro-optical panel is totally transmitted through said electro-optical panel without absorption when said electro-optical panel is switched to said second optical state of operation.

69. The electro-optical glazing structure of claim 68, wherein said first prespecified bandwidth comprises the infrared (IR) portion and ultra-violet (UV) portions of the electromagnetic spectrum, and said second prespecified bandwidth comprises said IR portion, said UV portion and the visible portion of the electromagnetic spectrum.

70. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

a second electrically-passive CLC electromagnetic radiation polarizing panel; and an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

71. The electro-optical glazing structure of claim 70,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels totally reflect without

absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

72. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

a second electrically-active CLC electromagnetic radiation polarizing panel; and an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

73. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC

electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

74. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a right hand circularly polarized (RHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a left hand circularly polarized

(LHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

75. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC electromagnetic radiation polarizing panel.

76. The electro-optical glazing structure of claim 75,

wherein said first electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation, and

wherein said first electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when



said electro-optical panel is switched to said first optical state of operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having said RHCP state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation, and

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either said LHCP state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

77. The electro-optical glazing structure of claim 68, which further comprises:

a window frame for mounting said electro-optical panel within a house or office building, or aboard a transportation vehicle.

78. The electro-optical glazing structure of claim 77, which further comprises:

a electromagnetic-sensor mounted on said window frame, for sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said window frame, for recharging the battery;

electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

a programmable micro-computer chip mounted within said window frame, for controlling the operation of said battery recharger and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

79. An intelligent pair of sunglasses, comprising:

a frame; and

a pair of optical element supported within said frame,

wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

80. An intelligent window system for dynamic electromagnetic radiation control which comprises:

a plurality of said electro-optical glazing structures of claim 11, each mounted within a house or office building, or aboard a transportation vehicle; and

a central control computer for coordinating the operation of said electro-optical glazing structures.

81. An composite electro-optical glazing structure which comprises:

a plurality of said electro-optical glazing structures of claim 1, stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than two said optical states of operation which permit complex levels of electromagnetic radiation control.

82. A stereoscopic 3-D viewing device in the form of eyeglasses, comprising:

a pair of optical elements positionable before the eyes of a user of said eyeglasses,

each said optical element including said electro-optical glazing structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of real world objects.

83. An electro-optical glazing structure which has total-reflection, semi-transparent and totally transparent modes of operation for improved control over the flow of electromagnetic radiation within the solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

84. An electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

85. An electro-optical glazing structure having a broad band of operation, including the IR, visible and UV portions of the

electromagnetic spectrum.

86. An electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a certain polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

87. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

88. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is parallel to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

89. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of

which are capable of reflecting electromagnetic radiation of a linear polarization state, one is perpendicular to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

90. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a LHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

91. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

92. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the

RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

93. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the LHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

94. An electro-optical structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

95. An electro-optical glazing structure, comprising a pair of electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

96. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of the present invention, wherein the transmission of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, between 50% transmission to 100% reflection and between 100% transmission to 100% reflection.

97. An actively-controlled window or viewing panel constructed from an electro-optical glazing structure, wherein the transmission of electromagnetic radiation over the UV and IR regions of the electromagnetic spectrum can be totally reflected, rather than absorbed, reducing the temperature cycle range which the window structure is required to undergo.

98. An actively-controlled window or viewing panel constructed from an electro-optical glazing structures, wherein only UV and IR radiation is reflected at the window surface, while electromagnetic radiation over the visible band is transmitted to the interior environment being maintained under thermal control.

99. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure thereof is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control

voltages for driving the electrically-active elements of the electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within the programmed microcontroller.

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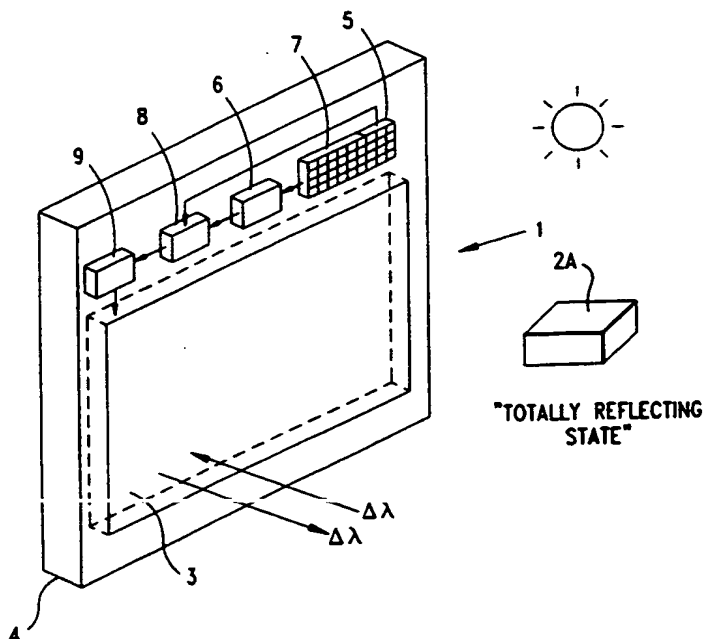
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(54) Title: ELECTRO-OPTICAL GLAZING STRUCTURES HAVING REFLECTION AND TRANSPARENT MODES OF OPERATION

(57) Abstract

Electro-optical glazing structures having total-reflection and semi-transparent and totally-transparent modes of operation which are electrically-switchable for use in dynamically controlling electromagnetic radiation flow in diverse applications.



CLAIMS TO INVENTION

1. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and

5 transmitting electromagnetic radiation, respectively, said electro-optical glazing structure comprising:

an electro-optical glazing panel of laminated construction, having first and second optical states of operation; and

10 optical state switching means for switching said electro-optical glazing panel to said first optical state of operation in order to induce said electro-optical glazing structure into said reflection mode of operation, and for switching said electro-optical glazing panel to said second optical state of operation in order to induce said electro-optical glazing structure into said transmission mode of operation.

15

2. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

20 a second electrically-passive CLC electromagnetic radiation polarizing panel;

and

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

25

3. The electro-optical glazing structure of claim 2, wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels reflect electromagnetic radiation having a first circularly

polarized state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having a second circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels reflect or transmit without absorption electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

4. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;  
a second electrically-active CLC electromagnetic radiation polarizing panel; and

an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

5. The electro-optical glazing structure of claim 4, wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels reflect electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation, wherein said first and second electrically-active CLC electromagnetic radiation polarizing

panels transmit electromagnetic radiation having either a right hand a second circularly polarized state and/or a wavelength outside said first prespecified bandwidth when said electro-optical glazing panel is switched to said first optical state of operation; and

5            wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

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6. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

first and a second electrically passive single layer electromagnetic radiation polarizing panels; and

15

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive electromagnetic radiation polarizing panels.

20

7. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC

25

electromagnetic radiation polarizing panel.

8. The electro-optical glazing structure of claim 7,

wherein said first electrically-active CLC electromagnetic radiation

polarizing panel reflects electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation, and

wherein said first electrically-active CLC electromagnetic radiation

5 polarizing panel transmits electromagnetic radiation having a second circularly polarized [(RHCP)] state when said electro-optical glazing panel is switched to said first optical state of operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel reflects electromagnetic radiation having said  
10 second state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits electromagnetic radiation having said first state when said electro-optical glazing panel is switched to  
15 said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit more than 50% of electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second  
20 optical state of operation.

9. The electro-optical glazing structure of claim 1, which further comprises:

a window frame for mounting said electro-optical glazing panel  
25 within a house or office building, or aboard a transportation vehicle.

10. The electro-optical glazing structure of claim 9, which further comprises:

a electromagnetic-sensor mounted on said window frame, for  
30 sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said window frame, for recharging the battery;

5       electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

10       a programmable micro-computer chip mounted within said window frame, for controlling the operation of said battery recharger and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

11. The electro-optical glazing structure of claim 1, further comprising:  
15   a frame for an intelligent pair of sunglasses; and  
      a pair of said optical glazing elements supported within said frame,

      wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

20

12. An intelligent window system for dynamic electromagnetic radiation control which comprises:

25       a plurality of said electro-optical glazing structures of claim 10, each mounted within a house or office building, or aboard a transportation vehicle; and

      a central control computer for coordinating the operation of said electro-optical glazing structures.

13. A composite electro-optical glazing structure which comprises:  
30       a plurality of said electro-optical glazing structures of claim 1,

stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than two said optical states of operation which permit complex levels of electromagnetic radiation control.

5

14. A stereoscopic 3-D viewing device in the form of eyeglasses, comprising:

10 a pair of optical elements positionable before the eyes of a user of said eyeglasses, each said optical element including said electro-optical glazing structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of real world objects.

15

15. An electro-optical glazing structure which has high reflection, semi-transparent and greater than 50% transparent modes of operation for improved control over the flow of electromagnetic radiation within the solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

20

16. A reflective electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

25

17. The electro-optical glazing structure of claim 1, wherein the transmission of the visible portion of the electromagnetic spectrum is controlled and wherein the IR portion of the electromagnetic spectrum is reflected.

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18. An electro-optical glazing structure, comprising an

electrically-active phase retardation panel interposed between a pair of single layer electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first linear polarization state, whereby a highly reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

19. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a first and a second electrically-passive electromagnetic radiation polarizing panel, the first panel reflecting electromagnetic radiation of a first linear polarization state, the second panel reflecting electromagnetic radiation of a second linear polarization state, whereby a reflective state of operation and a semi-transparent state of operation are provided over a region of the electromagnetic spectrum.

20. The electro-optical glazing structure of claim 19, wherein the first and a second electrically-passive electromagnetic radiation polarizing panels are single layer polarizing panels.

20

21. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

22. An electro-optical glazing structure, comprising a pair of



electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of a first circularly polarized state and the other of which is capable of reflecting electromagnetic radiation of a second circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

23. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the transmission and reflection of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, from greater than 50% transmission to high reflection.

24. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the electromagnetic radiation over the IR region of the electromagnetic spectrum can be reflected, rather than absorbed, reducing the temperature cycle range which the window structure is required to undergo.

25. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure of claim 1 is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the

electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within  
5 the programmed microcontroller.

26. The electro-optical glazing structure of claim 1 which is designed for integration within the heating/cooling system of a house, office building, factory or vehicle in order to control the flow of broad-band  
10 electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

27. An intelligent pair of shutter glasses, in which each optical element  
15 is realized using an electro-optical glazing structure of claim 1 fashioned to the dimensions of a shutter glass frame.

28. The electro-optic glazing structure of claim 1, further comprising:  
a reflecting layer for reflecting infrared light, wherein the  
20 electro-optic glazing structure of claim 1 controls the transmission and reflection of visible light.

29. The electro-optic glazing structure of claim 1, further comprising:  
a reflecting layer for reflecting UV light, wherein the electro-optic  
25 glazing structure of claim 1 controls the transmission and reflection of visible light.

30. The electro-optic glazing structure of claim 1, further comprising:  
30 a electro-optic glazing structure which controls the transmission and

reflection of IR light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of visible light.

31. The electro-optic glazing structure of claim 1, further comprising:

5       a electro-optic glazing structure which controls the transmission and reflection of visible light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of IR light.

32. An electro-optical glazing structure having reflection and  
10       transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, the electro-optical glazing structure comprising:

          an electro-optical panel of multilayer construction, having first and second optical states of operation;

15       optical state switching means for switching the electro-optical panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the  
20       transmission mode of operation, and

          means for further controlling electromagnetic radiation incident on the electro-optical panel.

33. The electro-optical glazing structure of claim 32, wherein the means  
25       for further controlling the electromagnetic radiation comprises a means for reflecting circularly polarized light.

34. The electro-optical glazing structure of claim 33, wherein the means for reflecting circularly polarized light comprise a cholesteric liquid  
30       crystal (CLC) reflector.

35. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a scattering layer for controllably scattering light.

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36. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

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37. The electro-optical glazing structure of claim 36x, wherein the anisotropically shaped objects are micron size sheets of reflecting material.

15 38. The electro-optical glazing structure of claim 37, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

39. The electro-optical glazing structure of claim 37, wherein the  
20 micron size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

40. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a polymerized polymer region containing a  
25 large plurality of inclusions of liquid crystal material.

41. The electro-optical glazing structure of claim 40, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

30

42. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

5 43. The electro-optical glazing structure of claim 42, wherein the scattering layer may be made non scattering under the influence of an electric field.

44. The electro-optical glazing structure of claim 32, wherein the means  
10 for further controlling the electromagnetic radiation comprises a mixture of a polymer and a liquid crystal material.

45. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material is transparent to the  
15 electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

46. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material reflects a portion of the  
20 electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

47. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and  
25 transmitting electromagnetic radiation, respectively, the electromagnetic radiation having a first and a second linear polarization, the electro-optical glazing structure comprising:

an electro-optical panel having first and second optical states of operation; and

30 optical state switching means for switching the electro-optical

panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation, wherein the electro-optical panel comprises:

a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference between the materials in each layer of the pair, the difference being in the index of refraction for electromagnetic radiation having the first linear polarization, wherein there is little difference in the index of refraction for electromagnetic radiation having the second linear polarization, the total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

48. The electro-optical glazing structure of claim 47, wherein the electro-optical panel further reflects circularly polarized electromagnetic radiation.

49. The electro-optical glazing structure of claim 48, wherein the electro-optical panel comprises a cholesteric liquid crystal (CLC) material.

50. The electro-optical glazing structure of claim 47, wherein the electro-optical panel selectively transmits and reflects electromagnetic radiation of a first bandwidth of the EM spectrum, further comprising a reflector of EM radiation which reflects radiation in a second bandwidth of the EM spectrum, the reflector of EM radiation comprising a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction

between the materials in each layer of the pair.

51. The electro-optical glazing structure of claim 50, wherein the reflector of EM radiation comprises a sheet having a large plurality of  
5 pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction between the materials in each layer of the pair. The total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

10 52. The electro-optical glazing structure of claim 47, further comprising a controllable scattering layer.

53. The electro-optical glazing structure of claim 52, wherein the controllable scattering layer comprises a fluid medium containing a  
15 large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

54. The electro-optical glazing structure of claim 47, wherein  
20 electrooptic panel further comprises a means for reflecting circularly polarized light.

55. The electro-optical glazing structure of claim 54, wherein the means for reflecting circularly polarized light comprise a cholesteric liquid  
25 crystal (CLC) reflector.

56. The electro-optical glazing structure of claim 47, wherein the electro-optic panel further comprises a scattering layer for controllably  
scattering light.

30

57. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

5

58. The electro-optical glazing structure of claim 57, wherein the anisotropically shaped objects are micron size sheets of reflecting material.

10 59. The electro-optical glazing structure of claim 58, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

60. The electro-optical glazing structure of claim 58, wherein the micron  
15 size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

61. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a polymerized polymer region containing a  
20 large plurality of inclusions of liquid crystal material.

62. The electro-optical glazing structure of claim 61, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

25

63. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

30 64. The electro-optical glazing structure of claim 63, wherein the



scattering layer may be made non scattering under the influence of an electric field.

65. The electro-optical glazing structure of claim 47, wherein the  
5 electro-optical panel further comprises a layer of a mixture of a polymer and a liquid crystal material.

66. The electro-optical glazing structure of claim 65, wherein the  
mixture of polymer and liquid crystal material is transparent to the  
10 electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

67. The electro-optical glazing structure of claim 65, wherein the  
mixture of polymer and liquid crystal material reflects a portion of the  
15 electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

68. An electro-optical glazing structure having total-reflection and  
transparent modes of operation for selectively reflecting and  
20 transmitting electromagnetic radiation without absorption, respectively,  
said electro-optical glazing comprising:

an electro-optical panel of laminated construction, having first and  
second optical states of operation; and

optical state switching means for switching said electro-optical  
25 panel to said first optical state of operation in order to induce said  
electro-optical glazing into said total-reflection mode of operation, and  
for switching said electro-optical panel to said second optical state of  
operation in order to induce said electro-optical glazing into said  
transmission mode of operation,

30 wherein electromagnetic radiation within a first prespecified

bandwidth falling incident upon said electro-optical panel is totally reflected from said electro-optical panel without absorption when said electro-optical panel is switched to said first optical state of operation, and

5        wherein electromagnetic radiation within a second prespecified bandwidth falling incident upon said electro-optical panel is transmitted through said electro-optical panel without absorption when said electro-optical panel is switched to said second optical state of operation.

10    69. The electro-optical glazing structure of claim 68, wherein said first prespecified bandwidth comprises the infrared (IR) portion and ultra-violet (UV) portions of the electromagnetic spectrum, and said second prespecified bandwidth comprises said IR portion, said UV portion and the visible portion of the electromagnetic spectrum.

15

70. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

        a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

20        a second electrically-passive CLC electromagnetic radiation polarizing panel; and    an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

25    71. The electro-optical glazing structure of claim 70,

        wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified

bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

15

72. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

20

a second electrically-active CLC electromagnetic radiation polarizing panel; and an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

25

73. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified

bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

15

74. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a right hand circularly polarized (RHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a left hand circularly polarized (LHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorp

30

electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

5

75. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

10 a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC electromagnetic radiation polarizing panel.

76. The electro-optical glazing structure of claim 75,

15 wherein said first electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation, and

20 wherein said first electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of  
25 operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having said RHCP state and a wavelength within said first prespecified bandwidth when said electro-optical panel  
30 is switched to said first optical state of operation, and

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either said LHCP state and/or a wavelength outside said first prespecified bandwidth when said electro-

5 optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth  
10 when said electro-optical panel is switched to said second optical state of operation.

76. The electro-optical glazing structure of claim 68, which further comprises:

15 a window frame for mounting said electro-optical panel within a house or office building, or aboard a transportation vehicle;

77. The electro-optical glazing structure of claim 76, which further comprises:

20 a electromagnetic-sensor mounted on said window frame, for sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said  
25 window frame, for recharging the battery;

electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

a programmable micro-computer chip mounted within said  
30 window frame, for controlling the operation of said battery recharger

and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

- 5 78. An intelligent pair of sunglasses, comprising:  
a frame; and  
a pair of optical element supported within said frame,  
wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

10

79. An intelligent window system for dynamic electromagnetic radiation control which comprises:

a plurality of said electro-optical glazing structures of claim 11,  
each mounted within a house or office building, or aboard a

15 transportation vehicle; and

a central control computer for coordinating the operation of said electro-optical glazing structures.

80. An composite electro-optical glazing structure which comprises:

20 a plurality of said electro-optical glazing structures of claim 1,  
stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than  
two said optical states of operation which permit complex levels of  
electromagnetic radiation control.

25

81. A stereoscopic 3-D viewing device in the form of eyeglasses,  
comprising:

a pair of optical elements positionable before the eyes of a user of  
said eyeglasses,

30 each said optical element including said electro-optical glazing

structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of  
5 real world objects.

82. An electro-optical glazing structure which has total-reflection, semi-transparent and totally transparent modes of operation for improved control over the flow of electromagnetic radiation within the  
10 solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

83. An electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.  
15

84. An electro-optical glazing structure having a broad band of operation, including the IR, visible and UV portions of the electromagnetic spectrum.

20 85. An electrically-active -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a certain polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the  
25 electromagnetic region of the electromagnetic spectrum.

86. An electro-optical glazing structure, comprising an electrically-active -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are  
30 capable of reflecting electromagnetic radiation of a linear polarization



state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

5 87. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is parallel to other, whereby a totally reflective state of  
10 operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

88. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of  
15 electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is perpendicular to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic  
20 spectrum.

89. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive cholesteric liquid crystal (CLC) electromagnetic  
25 radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a LHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

90. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

91. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

92. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the LHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

93. An electro-optical structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are

capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

5

94. An electro-optical glazing structure, comprising a pair of electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the  
10 RHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

95. An actively-controlled window or viewing panel constructed from  
15 the electro-optical glazing structure of the present invention, wherein the transmission of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, between 50% transmission to 100% reflection and between 100% transmission to 100% reflection.

20

96. An actively-controlled window or viewing panel constructed from an electro-optical glazing structure, wherein the transmission of electromagnetic radiation over the UV and IR regions of the electromagnetic spectrum can be totally reflected, rather than absorbed,  
25 reducing the temperature cycle range which the window structure is required to undergo.

97. An actively-controlled window or viewing panel constructed from an electro-optical glazing structures, wherein only UV and IR radiation  
30 is reflected at the window surface, while electromagnetic radiation over

the visible band is transmitted to the interior environment being maintained under thermal control.

98. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure thereof is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within the programmed microcontroller.

99. An electro-optical window structure which is designed for integration within the heating/cooling system of a house, office building, factory or vehicle in order to control the flow of broad-band electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

100. An intelligent pair of shutter glasses, in which each optical element is realized using an electro-optical glazing structure fashioned to the dimensions of a shutter glass frame.

## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/03688

**A. CLASSIFICATION OF SUBJECT MATTER**

IPC(6) : G02F 1/1335, 1/13  
US CL : 349/13, 14, 15, 16, 115, 117, 176  
According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 349/13, 14, 15, 16, 115, 117, 176

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X --- Y --- A	US 4,749,261 A (MCLAUGHLIN ET AL) 07 June 1988 (07/06/88), see column 4, line 19-column 7, line 11, and column 12, lines 61-66.	83, 84, 98, 99 ----- 1-10, 12, 13, 15-26, 28-31, 68, 69, 70-75, 76a, 76b, 77, 79, 80, 82, 85-97 ----- 32-46

☒ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
*A* document defining the general state of the art which is not considered to be of particular relevance	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
*E* earlier document published on or after the international filing date	--- document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
*L* document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*G* document member of the same patent family
*O* document referring to an oral disclosure, use, exhibition or other means	
*P* document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

07 JUNE 1998

Date of mailing of the international search report

08 JUL 1998

Name and mailing address of the ISA/US  
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## INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/03688

## C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y ---- A	US 5,437,811 A (DOANE ET AL) 01 August 1995 (01/08/95), see 1, line 48-column 2, line 50, column 3, lines 18-23, column 4, lines 13-21, and column 6, line 3-7.	1, 7-13, 15-17, 23-31, 68, 69, 75, 76a, 76b, 77-80, 82, 95-97, 100 ----- 32-46
Y	US 5,399,390 A (AKINS) 21 March 1995 (21/03/95), see column 5, lines 46-63.	7, 8, 13, 68, 69, 75, 76a, 80
Y	US 3,711,181 A (ADAMS, JR. ET AL) 16 January 1973 (16/01/73), see entire document, particularly the abstract.	2-6, 18-22, 70-74, 85-94
X --- Y	US 4,475,031 A (MOCKOVCIK, JR.) 02 October 1984 (02/10/1984)	1, 9, 10, 23, 25, 26, 95, 98, 99 ----- 12, 16, 79, 83, 84
Y	US 5,015,086 A (OKAUE ET AL) 14 May 1991 (14/05/91), see entire document.	11, 27, 78, 100
X,P ---- Y	US 5,686,979 A (WEBER ET AL) 11 November 1997 (11/11/97), see entire document.	1-3, 6, 9, 15-20, 23, 24, 26, 28, 30, 31, 47, 50, 51, 68, 70, 71, 76b, 82-88, 91, 95, 99 ----- 12, 29, 69, 96, 97
A	US 5,133 A (FURUTA) 16 December 1997 (16/12/97), see entire document.	14, 81
A	US 4,922 A (JACOB) 10 February 1987 (10/02/87), see entire document.	47-67

# INTERNATIONAL SEARCH REPORT

International application No.  
PCT/US98/03688

## Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This international report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

- ☐ Claims Nos.:  
because they relate to subject matter not required to be searched by this Authority, namely:
  
2. ☒ Claims Nos.: 95  
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:  
  
Claim 95 includes a glazing structure "of the present invention". Since the claims define the invention, a recitation of "the present invention" in the claim renders the scope of claim 95 completely undefined.
  
3. ☐ Claims Nos.:  
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

## Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.
2. ☐ As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:
  
4. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

Remark on Protest

- ☐ The additional search fees were accompanied by the applicant's protest.  
☐ No protest accompanied the payment of additional search fees.

ELECTRO-OPTICAL GLAZING STRUCTURES  
HAVING REFLECTION AND TRANSPARENT MODES OF OPERATION

5

BACKGROUND OF THE INVENTION

Technical Field

10       The present invention relates generally to an electro-optical glazing structure having total-reflection and semi-transparent and totally-transparent modes of operation which are electrically-switchable for use in dynamically controlling electromagnetic radiation flow in diverse applications.

Background Art

15       The use of windows in homes, commercial buildings, and automotive vehicles alike is very well known. The reasons for providing windows in such structures and systems are directly related to the functions they perform. For example, window structures provide for ventilation, lighting, a sense of spaciousness, as  
20       well as a way of making contact with the outdoors. Windows made of glazing (e.g. glass material) also permit selective transmission of electromagnetic radiation between the outdoors and the interior space of homes, commercial buildings, and automotive vehicles. While conventional forms of glazing serves many useful functions,  
25       such forms are not without problems.

      An appreciation of the problems presented by the use of conventional glazing in windows, can be most easily attained by recognizing the nature and composition of electromagnetic radiation with which windows universally come in contact.



On a clear day at sea level, electromagnetic radiation is composed of 3% ultraviolet light (i.e. electromagnetic radiation in the UV band), 44% visible light (i.e. electromagnetic radiation in the visible band); and 53% infrared light (i.e. electromagnetic radiation in the IR band). In accordance with the laws of physics, 50% of all electromagnetic radiation produced is left hand circularly polarized (LHCP) while the other 50% thereof is right hand circularly polarized (RHCP). The total electromagnetic radiation striking a window surface is a combination of direct radiation from the Sun and diffuse radiation from the ambient environment. While electromagnetic radiation is broad-band in nature, it is the ultraviolet light component thereof which causes molecular decomposition in various types of plastic material and inorganic dyes, which results in color fading.

When electromagnetic radiation strikes a glass window, three different physical processes occur. Some of the radiant energy is transmitted through the glass; some of the radiant energy is reflected off the glass; and a small portion of the radiant energy is absorbed by the glass. The energy transmitted through the glass window is typically absorbed by furnishings or structures within the interior environment, and often becomes trapped therewithin causing an increase in interior temperature.

Depending on the season, electromagnetic radiation transmitted through glass windows can be either mitigate or worsen the thermal loading imposed upon the heating and cooling systems associated with the glass windows. Consequently, during the hot weather season, it is highly desired to shield windows and sliding glass doors from electromagnetic radiation in order to lessen thermal loading

upon cooling systems. During cold weather season, it is highly desired to expose windows and sliding glass doors to electromagnetic radiation in order to lessen thermal loading on heating systems.

In short, it is highly desired to selectively control the transmission of electromagnetic radiation through window structures at different times of the day and year so that thermal loading upon the heating and cooling systems of residential, commercial and industrial building environments can be minimized. By minimizing such thermal loading, power can be used in an economical manner to control the internal temperature of residential, commercial and industrial building environments. Achievement of this goal would impact the natural environment in a positive manner, while improving the quality of life.

With such objectives in mind, great effort has been expended in recent times to improve the ways and means of selectively controlling the transmission of electromagnetic radiation through window structures.

One approach to electromagnetic radiation control involves using a window shade to reduce the transmission of electromagnetic radiation through windows. The most popular type of shade is the window blind. However, as window blind is mounted within the interior of the building or transportation environment, electromagnetic radiation is allowed transmit through the window, raise the temperature within the internal environment, and thus increase thermal loading on cooling systems during the hot weather season. Also, the operation of window blinds requires mechanical or electro-mechanical controls which tend to be bulky and expensive to manufacture, install and maintain.

Another approach to electromagnetic radiation control involves the use of sun control films which are physically applied to the surface of glass windows in building and automotive vehicles alike. Presently a variety of different types of sun control film are  
5 marketed by various firms. Such electromagnetic control films can be categorized into one of the three basic categories, namely: high reflectivity film; heat saving or winter film; and fade protection film.

High reflectivity electromagnetic films are most effective at blocking summer heat. The higher the reflectivity of electromagnetic  
10 film, the more effective it will be at blocking electromagnetic radiation. Electromagnetic reflectivity film having a silver, mirror-like surface is more effective in blocking electromagnetic radiation than the colored, more transparent films. Electromagnetic reflectivity films can lower the U-value of glass by more than 10%.  
15 Notably, in climates having long heating seasons, the use of high reflectivity film prevents using the winter sun to warm the interior of buildings during the cold weather season, and thus lessen thermal loading on building heating systems.

Heat-saving or winter films are designed to reduce winter heat  
20 losses through glazing. These films can lower the U-value of glass windows by more than 20%.

Fade-protection films are designed to filter out ultraviolet rays. Ultraviolet rays cause about 60-65% of color fading in most home furnishing fabrics and automobile dash boards.

25 While electromagnetic radiation control films of the types described above can be used to control heat and glare, eliminate sun damage, and to a lesser extent, reduce visibility into buildings during the daytime. The major disadvantages thereof are reduction in

interior light, loss of visibility, and extra care required in cleaning. Moreover, prior art electromagnetic window films are incapable of changing from transmissive during winter months to reflective during summer months in order to effectively use electromagnetic radiation for dynamic temperature control of biological environments (e.g. human habitats, greenhouses and the like).

An alternative approach to electromagnetic radiation control involves using special glass panels having radiation transmission characteristics which effectively absorb (i.e. block) the infrared and ultra violet wavelengths, while transmitting the visible wavelengths thereby allowing window viewing and day light to enter the interior spaces of buildings using such window technology. While the light transmission characteristics of such glass provides a measure of electromagnetic radiation control during cooling seasons, where outdoor temperatures tend to be above 72 degrees Fahrenheit, its IR absorption characteristics prevents, during heating season, IR wavelengths of Sun light to warm the interior spaces of building structures in which such glass panels are installed. Consequently, during heating seasons, such glass fails to lessen the thermal loading on the heating systems of such buildings, as would be desired in an effort to conserve energy and heating resources during the winter months.

In recent times, there has been great interest in using variable light transmission glass or glazing, referred to as "*smart windows*", to achieve electromagnetic radiation (i.e. energy) control in buildings and vehicles alike. The reason for using smart window structures, rather than conventional glass window panels, is quite clear. Smart window structures have light transmission characteristics that can be

electrically controlled during the course of the day (or year) in order to meet lighting needs, minimize thermal load on heating and/or cooling systems, and provide privacy within the interior spaces of buildings and vehicles alike.

5           The use of chromogenic switchable glazing or smart windows for controlling the flow of light and heat into and out of a glazing according to occupant comfort, is discussed in great detail in the following papers: "Chromogenic Switchable Glazing: Towards the Development of the Smart Window" by Carl Lempert published in the  
10       June 1995 Proceedings of the Window Innovation Conference, Toronto, Canada; and "Optical Switching Technology for Glazings" by Carl Lempert published in Thin Solid Films, Volume 236, 1993, pages 6-13, both incorporated herein by reference.

15           In general, there are several different types chromogenic switchable glazing or smart windows, namely: non-electrically activated switchable glazings; and electrically-activated switchable glazings. The non-electrically activated types of chromogenic switchable glazing are based on: photochromics, thermochromics and thermotropics. The most common electrically-activated types of  
20       chromogenic switchable glazing are based on polymer dispersed liquid crystals (PDLC), dispersed particle systems (DPS), and electrochromics.

25           Prior art smart window structures based upon conventional twisted nematic (TN) or super twist nematic (STN) liquid crystal technology require the use of a pair of polarizers. This, however, results in high optical loss, as up to 60% of the incident light is absorbed by the polarizers, in the desired non-blocking mode of operation.

While a smart window structure based on polymer dispersed liquid crystal (PDLC) technology offers better performance than TN or STN based window structures, such smart window structures suffer from several significant shortcomings. In particular, conventional PDLC panels have a translucent state which can be used only to provide privacy, but lack a totally opaque state and a totally reflective state required for electromagnetic radiation control functions. In addition, the viewing haze limitation provided by the PDLC panels prevents clear viewing through this prior art window structure at larger viewing angles.

A primary drawback associated with Dispersed Particle Systems is that such systems simply do not have a reflection mode of operation, and thus created heat build-up within interior spaces which is sought to be avoided in thermal radiation control applications.

Thus it is clear that there is a great need in the art for an improved form of variable light transmission glazing structure which avoids the shortcomings and drawbacks of prior art technologies.

#### DISCLOSURE OF THE INVENTION

Accordingly, a primary object of the present invention is to provide an electro-optical glazing structure which avoids the shortcomings and drawbacks of prior art technologies.

Another object of the present invention is to provide an electro-optical glazing structure which has total-reflection, semi-transparent and totally transparent modes of operation for improved control over the flow of electromagnetic radiation within

the solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

A further object of the present invention is to provide such an electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

A further object of the present invention is to provide such an electro-optical glazing structure having a broad band of operation, including the IR, visible and UV portions of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a certain polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -

phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is parallel to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is perpendicular to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a LHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, both of



which are capable of reflecting electromagnetic radiation of a RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

5 A further object of the present invention is to provide an electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state  
10 and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

A further object of the present invention is to provide an  
15 electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the LHCP state, whereby a totally reflective state of operation and a totally  
20 transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC  
25 electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-

transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

A further object of the present invention is to provide an electro-optical glazing structure, comprising a pair of electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

Another object of the present invention is to provide an actively-controlled window or viewing panel constructed from the electro-optical glazing structure of the present invention, wherein the transmission of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, between 50% transmission to 100% reflection and between 100% transmission to 100% reflection.

Another object of the present invention is to provide an actively-controlled window or viewing panel constructed from the electro-optical glazing structure of the present invention, wherein the transmission of electromagnetic radiation over the UV and IR regions of the electromagnetic spectrum can be totally reflected, rather than absorbed, reducing the temperature cycle range which the window structure is required to undergo.

Another object of the present invention is to combine the electro-optical glazing panel of the present invention with a controllable scattering layer or structure in order to scatter light transmitted therethrough or reflected therefrom.

Another object of the present invention is to provide an actively-controlled window or viewing panel constructed from the electro-optical glazing structures of the present invention, wherein only UV and IR radiation is reflected at the window surface, while  
5 electromagnetic radiation over the visible band is transmitted to the interior environment being maintained under thermal control.

Another object of the present invention is to provide an intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or  
10 automobile, wherein the electro-optical glazing structure thereof is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for  
15 recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing  
20 control voltages as required by a radiation flow control program stored within the programmed microcontroller.

A further object of the present invention is to provide such an electro-optical window structure which is designed for integration within the heating/cooling system of a house, office building, factory  
25 or vehicle in order to control the flow of broad-band electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

Another object of the present invention is to provide a

thermal/viewing shield or panel made from electro-optical glazing structure of the present invention.

Another object of the present invention is to provide of an intelligent pair of sunglasses, in which each optical element is realized using an electro-optical glazing structure of the present invention, fashioned to the dimensions of a sunglass frame.

Another object of the present invention is to provide of an intelligent pair of shutter glasses, in which each optical element is realized using an electro-optical glazing structure of the present invention, fashioned to the dimensions of a shutter glass frame.

Another object of the present invention is to provide an intelligent windshield or viewing screen, which is realized from an electro-optical glazing structure of the present invention.

These and other objects of the present invention will become apparent hereinafter and in the Claims to Invention.

### BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the Object of the Present Invention, the following Detailed Description of the Illustrative Embodiments of the Present Invention should be read in conjunction with the accompanying Drawings, wherein:

Fig. 1A is a perspective view of a generalized embodiment of the intelligent electro-optical window system of the present invention, wherein the electro-optical glazing structure thereof is electrically switched under microcomputer-control to its totally-reflecting state of operation upon detecting a first set of

preprogrammed electromagnetic conditions, whereby broad-band electromagnetic radiation is completely reflected off the electro-optical glazing structure thereof;

Fig. 1B is a perspective view of the generalized embodiment of the intelligent electro-optical window system shown in Fig. 1A, wherein the electro-optical glazing structure thereof is electrically switched under microcomputer-control to its transmission state of operation upon detecting a second set of preprogrammed electromagnetic conditions, where broad-band electromagnetic radiation is transmitted through the electro-optical glazing structure thereof;

Fig. 2 is an exploded perspective view of a first illustrative embodiment of the electro-optical glazing structure of the present invention, showing an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive RHCP electromagnetic radiation reflecting panels, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 2A is a schematic diagram of the RHCP electromagnetic radiation reflecting panel shown in Fig. 2, and its response to both RHCP and LHCP electromagnetic radiation incident thereto;

Fig. 2B is a schematic representation of the electromagnetic radiation reflection characteristics of the RHCP electromagnetic radiation reflecting panels of the glazing structure of Fig. 2, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$ ;

Fig. 2C is a schematic representation of a first embodiment of the  $\pi$ -phase retardation panel used in the construction of the glazing

structure of Fig. 2, illustrating its operating characteristics in response to different glazing control voltages;

Fig. 2D is a schematic representation of a second embodiment of the  $\pi$ -phase retardation panel used in the construction of the glazing structure of Fig. 2, illustrating its operating characteristics in response to different glazing control voltages;

Fig. 2E1 is a schematic diagram of a super broad-band  $\pi$ -phase retardation panel construction formed by interposing a twisted nematic, super-twisted nematic or cholesteric liquid crystal cell between a pair of electrically-passive broad-band  $\pi/2$  phase retardation panels;

Fig. 2E2 is a schematic diagram of a broad-band  $\pi$ -phase retardation panel employed in the electrically-switchable super-broad band phase-retardation panel shown in Fig. 2E1, made by laminating a plurality of narrow-band or broad-band  $\pi/2$  layers, each realized using a material having a different birefringence and its  $\pi/2$  phase-retardation characteristics centered about a different wavelength;

Fig. 2E3 is a graphical representation of the resulting  $\pi/2$  phase retardation characteristics provided by the cooperation of the phase retardation characteristics of the individual narrow-band or broad-band  $\pi/2$  layers used to construct the electrically-passive super-broad band  $\pi/2$  phase-retardation panel shown in Fig. 2E2;

Fig. 3A is a schematic diagram illustrating the operation of the glazing structure of Fig. 2, wherein the  $\pi$ -phase retardation panel of Fig. 2C is used and the control voltage provided thereto is selected

(i.e.,  $V=0$ ,  $\phi=\pi$ ) so that the window panel is switched into its optically opaque or reflection state of operation;

Fig. 3B is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 2, where the  $\pi$ -phase retardation panel of Fig. 2C is used and the control voltage provided thereto is selected (i.e.,  $V=1$ ,  $0$ ) so that the window panel is switched into its the optically transparent (i.e. semi-clear) state of operation;

Fig. 4 is an exploded perspective view of a second illustrative embodiment of the intelligent electro-optical window of the present invention, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive LHCP electromagnetic radiation reflecting panels, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 4A is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 4, and its response to both RHCP and LHCP electromagnetic radiation incident thereto;

Fig. 4B is a schematic representation of the electromagnetic radiation reflection characteristics of the LHCP electromagnetic radiation reflecting panels of the window of Fig. 4, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$ ;

Fig. 5A is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 4, where the  $\pi$ -phase retardation panel of Fig. 2D is used and the control voltage provided thereto is selected (i.e.,  $v=1$ ,  $\phi=\pi$ ) so that the window panel is switched into its the opaque or reflection state of operation;

Fig. 5B is a schematic diagram illustrating the operation of the

intelligent electro-optical window of Fig. 5, where the  $\pi$ -phase retardation panel of Fig. 5D is used and the control voltage provided thereto is selected (I.e.,  $V=0$ ,  $\phi=0$ ) so that the window panel is switched into its optically semi-transparent (i.e., semi-clear) state of operation;

Fig. 6 is an exploded perspective view of a third illustrative embodiment of the intelligent electro-optical window of the present invention, comprising an electrically-active  $\pi$ -phase retardation panel interposed between an electrically-passive RHCP electromagnetic radiation reflecting panel and an electrically-passive LHCP electromagnetic radiation reflecting panel, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 6A is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 6, and its response to both RHCP and LHCP electromagnetic radiation incident thereto;

Fig. 6B is a schematic representation of the electromagnetic radiation reflection characteristics of the LHCP electromagnetic radiation reflecting panel of the window of Fig. 6, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$ ;

Fig. 6C is a schematic diagram of the RHCP electromagnetic radiation reflecting panel shown in Fig. 6, and its response to both RHCP and LHCP electromagnetic radiation incident thereto;

Fig. 6D is a schematic representation of the electromagnetic radiation reflection characteristics of the RHCP electromagnetic radiation reflecting panel of the window of Fig. 6, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$ ;



Fig. 7A is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 6, where the  $\pi$ -phase retardation panel of Fig. 2C is used and the control voltage provided thereto is selected (i.e.,  $v=0$ ,  $\phi=\pi$ ) so that the window panel is  
5 switched into its the optically semi-transparent (i.e. semi-clear) state of operation;

Fig. 7B is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 6, where the  $\pi$ -phase retardation panel of Fig. 2C is used and the control voltage provided  
10 thereto is selected (i.e.,  $v=0$ ,  $\phi=0$ ) so that the window panel is switched into its optically opaque or reflection state of operation;

Fig. 8 is an exploded perspective view of a fourth illustrative embodiment of the intelligent electro-optical window of the present invention, comprising an electrically-active polarization rotation  
15 panel interposed between an electrically-passive linear polarizing (LP1) electromagnetic radiation reflecting panel and an electrically-passive LP1 electromagnetic radiation reflecting panel, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic  
20 spectrum;

Fig. 8A is a schematic diagram of the LP1 electromagnetic radiation reflecting panel shown in Fig. 8, and its response to both LP1 and LP2 electromagnetic radiation incident thereto;

Fig. 8B is a schematic representation of the electromagnetic radiation reflection characteristics of the LP1 electromagnetic radiation reflecting panel of the window of Fig. 8, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{LP1}}$ ;

25

Fig. 8C is a schematic diagram of the LP2 electromagnetic radiation reflecting panel shown in Fig. 8, and its response to both LP1 and LP2 electromagnetic radiation incident thereto;

Fig. 8D is a schematic representation of the electromagnetic radiation reflection characteristics of the LP2 electromagnetic radiation reflecting panel of the window of Fig. 8, over its broadband range of operation,  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$ ;

Fig. 8E is a schematic representation of an illustrative embodiment of the electro-optical glazing structure of Fig. 8, in which an electrically-switchable linear polarization direction rotating panel, realized using an electrically-controlled birefringence (ECB) cell, surface stabilized ferroelectric liquid crystal (SSFLC) cell, twisted nematic cell, super-twisted nematic cell, or cholesteric liquid crystal cell, is interposed between a pair of electrically-passive linear broadband polarizing reflective panels realized using (1) broad-band CLC films with  $\pi/2$  phase-retardation surfaces integrally formed therein and/or other types of reflective linear polarizers such as multi-layer interference linear polarizers;

Fig. 9A is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 8, where the linear polarization direction rotating panel of Fig. 8 is used and the control voltage provided thereto is selected (i.e.,  $v=0$ , 90 degrees rotation) so that the window panel is switched into its transmission or semi-clear state of operation;

Fig. 9B is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 9, where the linear polarization direction rotating panel of Fig. 8 is used and the control

voltage provided thereto is selected (i.e.,  $v=1$ , zero degrees rotation) so that the window panel is switched into its optically opaque state of operation;

Fig. 10 is an exploded perspective view of a fifth illustrative embodiment of the intelligent electro-optical window of the present invention, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a first electrically-active LHCP electromagnetic radiation reflecting panel and a second electrically-active LHCP electromagnetic radiation reflecting panel, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 10A is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 10, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in the LHCP radiation reflecting state thereof;

Fig. 10B is a schematic representation of the electromagnetic radiation reflection characteristics of the LHCP electromagnetic radiation reflecting panels of Fig. 10, over the broadband range of operation thereof  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$ , when operated in the LHCP radiation reflecting state thereof;

Fig. 10C is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 10, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in the radiation transmission state thereof;

Fig. 10D is a schematic representation of the electromagnetic transmission characteristics of the LHCP electromagnetic radiation

reflecting panels of Fig. 10, over the broadband range of operation thereof  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$ , when operated in the radiation transmission state thereof;

Fig. 10E is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 10, where the control voltages provided to both LHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically opaque state of operation;

Fig. 10F is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 10, where the control voltages provided to both LHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically transparent (i.e. clear) state of operation;

Fig. 11 is schematic cross-sectional diagram illustrating the construction of the first illustrative embodiment of the electrically-switchable, circularly polarizing CLC panels used in the electro-optical glazing structures of Figs. 10, 12 and 14;

Fig. 11A1 is a graphical representation of the reflection characteristics of the first embodiment of the electrically-switchable broad-band CLC panel of Fig. 10, measured prior to UV polymerization of the CLC material contained within the ITO coated substrate plates of the panel, using un-polarized light;

Fig. 11A2 is a graphical representation of the reflection characteristics of the first embodiment of the electrically-switchable broad-band CLC panel of Fig. 10, measured subsequent to UV polymerization of the CLC material contained within the ITO coated substrate plates of the panel, using right-handed and left-handed circularly polarized light;

Fig. 11A3 is a graphical representation of the reflection characteristics of the first embodiment of the electrically-switchable broad-band CLC panel of Fig. 10, measured during electrically inactive (no voltage applied) and electrically-active (voltage applied) states of operation using right-handed circularly polarized light;

Fig. 12 is an exploded perspective view of a sixth illustrative embodiment of the intelligent electro-optical window of the present invention, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a first electrically-active RHCP electromagnetic radiation reflecting panel and a second electrically-active RHCP electromagnetic radiation reflecting panel, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 12A is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 12, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in the RHCP radiation reflecting state thereof;

Fig. 12B is a schematic representation of the electromagnetic radiation reflection characteristics of the RHCP electromagnetic radiation reflecting panels of Fig. 12, over the broadband range of operation thereof  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$ , when operated in the RHCP radiation reflecting state thereof;

Fig. 12C is a schematic diagram of the RHCP electromagnetic radiation reflecting panel shown in Fig. 12, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in the radiation transmission state thereof;

Fig. 12D is a schematic representation of the electromagnetic transmission characteristics of the RHCP electromagnetic radiation reflecting panels of Fig. 12, over the broadband range of operation thereof  $\Delta\lambda_{\text{transmission}}^{\text{RHCP}}$ , when operated in the radiation transmission state thereof;

Fig. 13A is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 12, where the control voltages provided to both RHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically opaque state of operation;

Fig. 13B is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 12, where the control voltages provided to both RHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically transparent (i.e. clear) state of operation;

Fig. 14 is an exploded perspective view of a seventh illustrative embodiment of the intelligent electro-optical window of the present invention, showing an electrically-active LHCP electromagnetic radiation reflecting panel laminated to an electrically-active RHCP electromagnetic radiation reflecting panel, each made from CLC material having polarization-selective reflection characteristics over a broad-band region of the electromagnetic spectrum;

Fig. 14A is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 14, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in its LHCP radiation reflecting state;

Fig. 14B is a schematic representation of the electromagnetic radiation reflection characteristics of the LHCP electromagnetic

radiation reflecting panel of Fig. 14, over its broadband range of operation  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$ , when operated in its LHCP radiation reflecting state;

Fig. 14C is a schematic diagram of the LHCP electromagnetic radiation reflecting panel shown in Fig. 14, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when  
5 operated in its radiation transmission state;

Fig. 14D is a schematic representation of the electromagnetic radiation transmission characteristics of the LHCP electromagnetic radiation reflecting panel of Fig. 14, over its broadband range of  
10 operation  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$ , when operated in its radiation transmission state;

Fig. 14E is a schematic diagram of the RHCP electromagnetic radiation reflecting panel shown in Fig. 14, and its response to both RHCP and LHCP electromagnetic radiation incident thereto when operated in its RHCP radiation reflecting state;

Fig. 14F is a schematic representation of the electromagnetic radiation reflection characteristics of the RHCP electromagnetic radiation reflecting panel of Fig. 14, over its broadband range of  
15 operation  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$ , when operated in its RHCP radiation reflecting state;

Fig. 14G is a schematic diagram of the RHCP electromagnetic radiation reflecting panel shown in Fig. 14, and its response to both  
20 RHCP and LHCP electromagnetic radiation incident thereto when operated in its radiation transmission state;

Fig. 14H is a schematic representation of the electromagnetic radiation transmission characteristics of the RHCP electromagnetic radiation reflecting panel of Fig. 14, over its broadband range of  
25 operation  $\Delta\lambda_{\text{transmission}}^{\text{RHCP}}$ , when operated in its radiation transmission state;

Fig. 15A is a schematic diagram illustrating the operation of the

intelligent electro-optical window of Fig. 14, where the control voltages provided to both LHCP and RHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically opaque state of operation;

5           Fig. 15B is a schematic diagram illustrating the operation of the intelligent electro-optical window of Fig. 14, where the control voltages provided to both RHCP electromagnetic radiation reflecting panels are selected so that the window panel is switched into its the optically transparent (i.e. clear) state of operation;

10           Fig. 16A is a schematic diagram of a second, alternative embodiment of the electrically-switchable broad-band CLC panel of Fig. 14, showing a portion of un-polarized light being polarized in a first polarization state and reflected off CLC microflakes (i.e. CLC pigments) that are oriented in a parallel manner within electrically-  
15           active host nematic liquid crystal molecules homogeneously aligned between a pair of ITO coated plates, across which no control voltage is applied, while a second portion of the un-polarized light is polarized in a second polarization state and transmitted through the oriented CLC microflakes;

20           Fig. 16B is a schematic diagram of the second embodiment of the electrically-switchable broad-band CLC panel of Fig. 14, showing the un-polarized light being transmitted between CLC microflakes that are oriented in a vertical manner within electrically-active host  
25           nematic liquid crystal molecules homotropically aligned between a pair of ITO coated plates, across which a control voltage is applied;

          Figs. 17A and 17B show a first illustrative embodiment of an electrically-controllable light scattering structure mountable to any embodiment of the electro-optical glazing structure of the invention



disclosed or taught herein in order to scatter that portion of incident light which is not reflected during its reflection-mode of operation, thereby improving the privacy function of the glazing structure in the reflection mode;

5           Figs. 18A and 18B show a second illustrative embodiment of an electrically-controllable light scattering structure mountable to any embodiment of the electro-optical glazing structure of the invention disclosed or taught herein in order to reflect that portion of incident light which is not reflected during its reflection-mode of operation,  
10           thereby improving the privacy function of the glazing structure in the reflection mode;

          Fig. 18C shows a third illustrative embodiment of an electrically-controllable light scattering structure mountable to any embodiment of the electro-optical glazing structure of the invention  
15           disclosed or taught herein in order to scatter that portion of incident light which is not reflected during its reflection-mode of operation, thereby improving the privacy function of the glazing structure in the reflection mode;

          Fig. 19 shows a fourth illustrative embodiment of an electrically-controllable light scattering structure mountable to any  
20           embodiment of the electro-optical glazing structure of the invention disclosed or taught herein in order to scatter that portion of incident light which is not reflected during its reflection-mode of operation, thereby improving the privacy function of the glazing structure in  
25           the reflection mode;

          Fig. 19A shows the electro-optical light scattering structure of Fig. 19 operated in its transmission mode, wherein no external voltage is applied (i.e.  $V=V_{\text{off}}$ );

Figs. 19B and 19C show transmission and reflection characteristics for the mode of operation indicated in Fig. 19A;

Fig. 19D shows the electro-optical light scattering structure of Fig. 19 operated in its light scattering mode, wherein an external voltage  $V$  is applied across the ITO surfaces (i.e.  $V=V_{on}$ );

Figs. 19E and 19F show transmission and reflection characteristics for the mode of operation indicated in Fig. 19D;

Fig. 20 shows a fifth illustrative embodiment of an electrically-controllable light scattering structure mountable to any embodiment of the electro-optical glazing structure of the invention disclosed or taught herein in order to scatter that portion of incident light which is not reflected during its reflection-mode of operation, thereby improving the privacy function of the glazing structure in the reflection mode;

Fig. 20A shows the electro-optical light scattering structure of Fig. 20 operated in its light scattering mode, wherein no external voltage is applied (i.e.  $V=V_{off}$ );

Figs. 20B and 20C show transmission and reflection characteristics for the mode of operation indicated in Fig. 20A;

Fig. 20D shows the electro-optical light scattering structure of Fig. 20 operated in its light transmission mode, wherein an external voltage  $V$  is applied across the ITO surfaces (i.e.  $V=V_{on}$ );

Figs. 20E and 20F show transmission and reflection characteristics for the mode of operation indicated in Fig. 20D;

Figs. 21 through 21F provide a generalized description of the illustrative embodiment disclosed in Figs. 6 and 8, wherein the electrically-passive broad-band polarizing layers have different

handedness in both the circularly polarizing (RHCP/LHCP) and linearly polarizing (LP1/LP2) system configurations;

5 Figs. 22 through 22F provide a generalized description of the illustrative embodiments disclosed in Figs. 2 and 4, wherein the electrically-passive broad-band polarizing layers have the same handedness in both the circularly polarizing (LHCP/LHCP or RHCP/RHCP) and linearly polarizing (LP1/LP1 or LP2/LP2) system configurations.

10 Figs. 23 through 23F provide a generalized description of the illustrative embodiment disclosed in Figs. 14 through 15B, wherein the electrically-active broad-band polarizing layers have a different handedness in the circularly polarizing (LHCP/LHCP or RHCP/RHCP) system configurations, and there is no optically active element disposed between the electrically-active polarizing layers;

15 Fig. 24 shows an illustrative embodiment of the electro-optical glazing structure of the present invention comprising (1) a pair of electrically-passive broadband IR reflective polarizing panels for reflecting incident LHCP and RHCP light within the broad IR band and transmitting all other components of light, and (2) an electrically-  
20 controlled light scattering panel for selectively scattering light over the visible band (when no external voltage is applied) so as to render the resulting glazing structure opaque to provide privacy behind the window structure into which is installed;

25 Fig. 24A shows the electro-optical glazing structure of Fig. 24 operated in scattering mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the electrically-controlled scattering panel;

Figs. 24B and 24C show transmission and reflection characteristics for the mode of operation shown in Fig. 24A;

Fig. 24D shows the electro-optical light glazing structure of Fig. 24 operated in its total-transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{on}$ ) is applied to electrically-controlled light scattering panel;

5 Figs. 24E and 24F show the transmission and reflection characteristics for the mode of operation shown in Fig. 24D;

Fig. 25 shows an other illustrative embodiment of the electro-optical glazing structure of the present invention which is the reverse mode of the electro-optical glazing structure shown in Fig. 24;

10 Fig. 25A shows the electro-optical glazing structure of Fig. 25 operated in its light transmission mode, wherein no external voltage (i.e.  $V=V_{off}$ ) is applied to the electrically-controlled scattering panel;

Figs. 25B and 25C show transmission and reflection characteristics for the mode of operation shown in Fig. 25A;

15 Fig. 25D shows the electro-optical light glazing structure of Fig. 24 operated in its light scattering mode, wherein an external voltage  $V$  (i.e.  $V=V_{on}$ ) is applied to electrically-controlled light scattering panel;

20 Figs. 25E and 25F show transmission and reflection characteristics for the mode of operation shown in Fig. 25D;

Fig. 26 shows another embodiment of the electro-optical glazing structure of the present invention constructed by adding the broadband IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 22, wherein the broadband polarizing panels are each of the same handedness (e.g. RHCP/RHCP or LP1/LP1);

Fig. 26A shows the electro-optical glazing structure of Fig. 26

operated in its total-transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof;

Figs. 26B and 26C show transmission and reflection characteristics for the mode of operation shown in Fig. 26A;

Fig. 26D shows the electro-optical light glazing structure of Fig. 26 operated in its partial-reflection/transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof;

Figs. 26E and 26F show the transmission and reflection characteristics for the mode of operation shown in Fig. 26D;

Fig. 27 shows another embodiment of the electro-optical glazing structure of the present invention which operates in the "reverse" mode of the glazing structure of Fig. 26, and is constructed by adding the broad-band IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 21, wherein the broadband polarizing panels are each of different handedness (e.g. RHCP/LHCP or LP1/LP2);

Fig. 27A shows the electro-optical glazing structure of Fig. 27 operated in its partial-reflection/transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof;

Figs. 27B and 27C show transmission and reflection characteristics for the mode of operation shown in Fig. 27A;

Fig. 27D shows the electro-optical light glazing structure of Fig.

27 operated in its total-reflection mode, wherein an external voltage  $V$  (i.e.  $V=V_{on}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof;

Figs. 27E and 27F show transmission and reflection characteristics for the mode of operation shown in Fig. 27D;

Fig. 28 shows another embodiment of the electro-optical glazing structure of the present invention constructed by adding the broadband IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 23, wherein the electrically-active broadband polarizing panels thereof are each of different handedness (i.e. RHCP/LHCP);

Fig. 28A shows the electro-optical glazing structure of Fig. 28 operated in its total-reflection mode, wherein no external voltage (i.e.  $V=V_{off}$ ) is applied to the electrically-active circularly-polarizing reflective panels thereof;

Figs. 28B and 28C show transmission and reflection characteristics for the mode of operation shown in Fig. 28A;

Fig. 28D shows the electro-optical light glazing structure of Fig. 26 operated in its total-transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{on}$ ) is applied to the electrically-active circularly-polarizing reflective panels thereof;

Figs. 28E and 28F shows transmission and reflection characteristics for the mode of operation shown in Fig. 28D;

Figs. 29A through 29C show a broad-band reflector for use in constructing broad-band circularly (and linearly) polarizing reflective panels employed in any one of embodiments of the electro-optical glazing panel hereof.

### BEST MODE EMBODIMENTS OF THE PRESENT INVENTION

5 Referring now to the accompanying Drawings, illustrative embodiments of the intelligent electro-optical window of the present invention will be described in great detail. In each of the figures, like structures and elements shall be indicated by like reference numerals.

10 In Figs. 1A and 1B, a generalized embodiment of the intelligent electro-optical glazing structure (i.e. window structure) of the present invention is shown installed within an environment (e.g. building or vehicle) having an interior space or volume adjacent the window structure. Typically, the interior space or volume functions as a  
15 form of human habitat, although there may be applications in which this is not the case. Preferably, the intelligent electro-optical window structure 1 cooperates with the heating/cooling system 2A of a house, office building, factory or vehicle indicated by reference numeral 2. In such preferred applications, the function of the  
20 electro-optical window structure will be to selectively control the flow of electromagnetic radiation through its electro-optical glazing structure and into the interior space, in order to minimize or reduce thermal loading upon the heating/cooling system of the environment.

As shown in Figs. 1A and 1B, the electro-optical glazing  
25 structure 1 comprises an electro-optical glazing panel 3 securely supported within a prefabricated window frame 4 which can be realized using virtually any suitable material such as, for example, plastic, metal, rubber, wood or composite material. Within the

window frame, a number of system subcomponents are securely mounted, namely: a electromagnetic-radiation sensor 5 for sensing electromagnetic conditions in the outside environment; a rechargeable-type battery 6 for producing electrical power within the window frame; a electromagnetic-powered battery recharger 7 for recharging the rechargeable battery 6; a micro-controller (e.g. RISC-type micro-computer chip with onboard ROM, EPROM and RAM) 8 for controlling the battery recharger and glazing control signals as required by a radiation flow control program stored within the micro-computer chip; and electrical circuitry 9, response to glazing control signals, for producing control voltages that are applied to the electrically-active elements of the electro-optical glazing structure 3 to electrically switch the same from one optical state to another optical state under microcontroller control.

As shown in Fig. 1, when a first set of preprogrammed electromagnetic conditions (e.g. a first prespecified band of electromagnetic radiation having power above a first prespecified power threshold) is detected by electromagnetic-radiation sensor, the electro-optical glazing structure 3 is electrically switched to its totally-reflecting state of operation under the control of preprogrammed microcontroller 8. In this totally-reflecting state of operation, visible and electromagnetic radiation is completely reflected off the glazing structure over a broad band of spectral wavelengths (e.g. 400 to 750 nanometers).

As shown in Fig. 1B, when a second set of preprogrammed electromagnetic conditions (e.g. a second prespecified band of electromagnetic radiation having power above a second prespecified power threshold) is detected by electromagnetic-radiation sensor, the



electro-optical glazing structure 3 is electrically switched to its transmission state of operation under the control of preprogrammed microcontroller 8. In this transmission state, visible and electromagnetic radiation is transmitted through the electro-optical glazing structure over a broad band of spectral wavelengths (e.g. 300 to 1000 nanometers).

While only two particular reflection/transmission states are illustrated in the above generalized embodiment, it is understood that virtually any set of reflection/transmission characteristics can be realized by the window structure of the present invention. In each such alternative embodiment, a particular set of conditions can be predefined to trigger a change in the optical state of the electro-optical glazing structure of the present invention. Then microcontroller is programmed to switch the optical state of the glazing structure upon detecting the corresponding condition. In alternative embodiments, the environmental condition or conditions which cause a switching operation, need not be related to electromagnetic radiation, but may be related to moisture, barometric pressure, temperature, or any other parameter prespecified within the programmed microcontroller 8.

While in theory there exists an infinite number of embodiments of the electro-optical glazing structure of the present invention, six different embodiments of the electro-optical glazing structure will be described in detail below in order to illustrate the inventive features thereof. Notably, each electro-optical glazing structure of the present invention is realized using CLC material having polarization-selective reflection characteristics over a broad-band of operation (i.e. selectively reflecting and/or transmitting RHCP

and LHCP wavelengths over the IR, visible and UV portions of the electromagnetic spectrum). An excellent tutorial and overview on the polarization-reflective properties of CLC materials and principles of polarization state conversion (i.e. linear-to-circular, circular-to-linear, linear-to-linear, circular-to-circular, unpolarized-to-linear, and unpolarized-to-circular) can be found in Applicant's US Patent No. 5,221,982, incorporated herein by reference in its entirety.

By virtue of such ultra broad-band operating characteristics of the electro-optical glazing material hereof, and the novel panel configurations disclosed herein, it is now possible to provide a level of electromagnetic radiation control hitherto unattainable by prior art smart window systems and methodologies.

#### First Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The first illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 2 through 3B. As shown in Fig. 2, the electro-optical glazing structure of the first illustrative embodiment 10 comprises: an electrically-active  $\pi$ -phase retardation panel 11 interposed between a pair of electrically-passive right-hand circularly polarized (RHCP) electromagnetic radiation reflecting panels 12A and 12B, respectively, for imparting a  $\pi$ -phase retardation to electromagnetic radiation transmitted therethrough in response to optical-state control voltages applied across the electrically-active  $\pi$ -phase retardation panel 11; and electrically conductive means 13 for applying optical-state control voltages to the electrically-active  $\pi$ -phase retardation panel 11.

Preferably, the electro-optical glazing structure of Fig 2 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

As illustrated in Figs. 2A and 2B, electromagnetic radiation having a RHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP

electromagnetic radiation reflecting panels 12A (12B) is 100% reflected directly therefrom without absorption, while electromagnetic radiation having either a LHCP polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panels 12A (12B) is transmitted 100% directly therethrough without absorption.

Such electrically-passive, broad-band RHCP electromagnetic radiation reflecting panels can be made using the fabrication methods disclosed in International Publication No. WO 97/16762 entitled "Super Broad-Band Polarizing Reflective Material" incorporated herein by reference in its entirety. Alternatively, narrow-band RHCP electromagnetic radiation reflecting panels 12A (12B) can be made using the fabrication methods disclosed in US Patent No. 5,221,982 to Faris, or using the techniques disclosed in US Patent No. 5,506,704 to Broer, et al. each being incorporated herein by reference in its entirety.

There are a number of different ways in which to fabricate broad-band electromagnetic radiation reflecting panels 12A (12B) using the super broad-band, broad-band, narrow-band and

spectrally-tunable CLC films taught in the above-cited references.

For example, broad-band circularly polarizing reflective panels 12A (12B) can be fabricated by producing sheets of such CLC film and then laminating the CLC film sheets onto a surface of glass or like substrate material physically associated with the electrically-switchable  $\pi$ -retardation panel 11 interposed between the circularly polarizing CLC panels, as shown in Figs. 2, 4, and 6, in particular. Notably, using the spectral-tuning techniques disclosed in detail in International Publication No. WO 97/16762, the CLC film hereof can be fabricated to have virtually any desired set of polarization reflection characteristics that would required by any particular application over a super broad-band of operation (e.g. from the UV region to the IR region of the electromagnetic spectrum).

Alternatively, sheets of super-broad-band, broad-band, narrow-band and/or spectrally-tuned CLC film can be produced as taught in the above references, and thereafter fragmented into microscopic sized CLC microflakes using film fragmentation techniques taught in US Patent No. 5,364,557. Then the CLC microflakes can be added to an optically transparent carrier fluid to produce a CLC ink or paint that can then be applied to the exterior surfaces of the glass substrates used to construct the electrically-switchable  $\pi$  retardation panel component of electro-optical glazing structures, of the type shown in Figs. 2, 4 and 6, for example. The concentration of the CLC microflakes and the viscosity of the carrier medium (e.g. lacquer, polymer, etc.) should be selected to ensure that when the coating of the CLC ink or paint is applied to a substrate, the CLC microflakes will be distributed within the carrier medium so that

incident light reflects from the resulting CLC coating in a non-specular manner. This will ensure that the resulting coating produces a "super-white" appearance in the eyes of on-viewers, providing a high measure of privacy, as well as aesthetic value, highly desired in window applications.

In the illustrative embodiment of the glazing structure of Fig. 2, the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 12A is designed to be substantially the same as characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel 12B. It is understood, however, that in alternative embodiments of the present invention, such reflection bandwidth characteristics may be specifically designed to partially overlap, or be separated from each other on the wavelength (i.e. frequency) domain in to provide desired reflection/transmission performance characteristics.

In general, a  $\pi$ -cell (i.e.  $\pi$ -retardation panel) or an electrically-controlled birefringence (ECB) panel can be used to realize the electrically-switchable  $\pi$ -phase retardation panel 11 employed in the circularly polarizing reflective glazing structures of Figs. 2, 4 and 6 hereof. Preferably, the techniques disclosed in US Patent No. 4,566,758 to Bos, incorporated herein by reference, are used to fabricate such electrically-switchable  $\pi$ -phase retardation panels 11. For most applications, the bandwidth of prior art  $\pi$ -cells should be sufficient to provide glazing structures having operating characteristics over the visible portion of the electromagnetic spectrum. However, in some instances, it will be desirable to provide electro-optical glazing structures having super broad-band operation

(i.e. from the IR region into the UV region of the spectrum). In such applications, it will be necessary to extend the  $\pi$ -phase retardation characteristics of the electrically-switchable  $\pi$ -phase retardation panel beyond the visible band. The following technique may be used to construct electrically-active (switchable)  $\pi$ -retardation panels capable of super broad-band operation.

As shown in Fig. 2E1, an electrically-switchable super broadband  $\pi$ -retardation panel can be constructed by interposing an electrically-active structure linear polarization direction rotating panel such as TN, or STN, or CLC cell, between a pair of electrically-passive super broad-band  $\pi/2$  retardation panels (shifters). As shown in Fig. 2E2, each super broad-band  $\pi/2$ -retardation panel is made by laminating, or depositing two or more broad-band or narrow-band  $\pi/2$  retardation layers, each made from different material and having  $\pi/2$  phase retardation characteristics centered about at different wavelength, as schematically shown in Fig. 2E3. These subcomponent broad-band or narrow-band  $\pi/2$  retardation layers can be made from liquid crystal material, birefringent polymer, and crystals.

The function of each electrically-passive super-broad-band  $\pi/2$  retardation panel is to convert circularly polarized light into linearly polarized light which can be polarization direction rotated by the electrically switchable TN, or STN, or CLC cell sandwiched between the pair of super broad-band  $\pi/2$  retardation layers. The function of the TN (twist nematic), or STN (super twist nematic), or CLC cell is to operate as an electrically-switchable optical rotator which rotates a linear polarization light by  $90^\circ$  when there is no electric field is

applied across its ITO surfaces. If an electric field is applied, the optical rotation power of the elements disappears. This control over the electric field allows the glazing structure to be switched from its total reflection state to its half reflection state, or vice versa. When the electrically-switchable polarization direction rotator is made from low-molecular weight (LMW) liquid crystal material having a chiral phase when no voltage is applied, then its selective wavelength of the should be located outside the window operating spectrum region. By controlling the helix of the CLC molecules in the chiral phase, as well as the total thickness thereof, a 90° rotation of a linear polarization can be achieved.

In general, there are two different ways to configure electrically-switchable  $\pi$  retardation panel 11 in terms of external control voltages. In Figs. 2C and 2D, these configurations are specified.

In Fig. 2C, the first embodiment of the  $\pi$ -phase retardation panel 11 is shown along with a specification of its various states of operation. As shown, when a non-zero voltage (e.g. 20 Volts) is applied across the phase retardation panel, 0-phase retardation is imparted to electromagnetic radiation transmitted therethrough. When a control voltage of zero volts is applied across the phase retardation panel, it imparts a  $\pi$ -phase retardation to electromagnetic radiation transmitted therethrough having a wavelength within its operating band  $\Delta\lambda_\pi$  which is typically 300-1000 nanometers.

In Fig. 2D, a second embodiment of the  $\pi$ -phase retardation panel is shown along with a specification of its states of operation. As shown, when a control voltage of zero volts is applied across this retardation panel, it imparts a 0-phase shift to electromagnetic

radiation having a wavelength within its operating band which is typically 350 nanometers, whereas  $\pi$ -phase retardation is imparted to such electromagnetic radiation when a non-zero voltage (e.g. 5-50 Volts) is applied thereacross. For wavelengths outside of the operating band, a phase shift other than  $\pi$ -radians is imparted to incident electromagnetic radiation when a non-zero voltage is applied.

Physically interfacing the subcomponent panels of the electro-optical glazing structure of Fig. 2 can be achieved using conventional lamination techniques well known in the glazing art.

The operation of the glazing structure of Fig. 2 will now be described with reference to Figs. 3A and 3B, where the  $\pi$ -phase retardation panel of Fig. 2C is used in the construction of the glazing structure.

As shown in Fig. 3A, the electro-optical glazing structure of Fig. 2 is switched to its optically opaque state of operation by applying the appropriate control voltage thereacross (e.g.  $V = 0$  Volts). In this optical state, the electro-optical glazing structure reflects both LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident the window panel independent of the direction of propagation. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 3A. Inasmuch as 100% of incident electromagnetic radiation is reflected from the surface of the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

As shown in Fig. 3B, the electro-optical glazing structure of Fig. 2 is switched to its optically semi-transparent (i.e. semi-clear state) of operation by applying the appropriate control voltage thereacross



(e.g.  $V=20$  Volts). In this optical state, the electro-optical glazing structure reflects RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident the window panel independent of the direction of propagation, while transmitting LHCP electromagnetic radiation falling incident the window panel independent of the direction of electromagnetic radiation propagation. The physical mechanisms associated with such reflection and transmission processes are schematically illustrated in Fig. 3A. Inasmuch as 50% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, while 50% of such electromagnetic radiation is reflected therefrom, this glazing structure can be said to "partially transmissive" in this state of operation.

#### Second Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The second illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 4 through 5B. As shown in Fig. 4, the electro-optical glazing structure of the second illustrative embodiment 14 comprises: an electrically-active (i.e. switchable)  $\pi$ -phase retardation panel 11 interposed between a pair of electrically-passive left-hand circularly polarizing (LHCP) electromagnetic radiation reflecting panels 15A and 15B, respectively; and electrically conductive means 16 for applying optical-state control voltages to the electrically-active  $\pi$ -phase retardation panel 11. Preferably, the electro-optical glazing structure of Fig 4 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

As illustrated in Figs. 4A and 4B, electromagnetic radiation having a LHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panels 15A, 15B is reflected directly therefrom without absorption, while electromagnetic radiation having either a RHCP polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the LHCP electromagnetic radiation reflecting panels is transmitted directly therethrough without absorption. Such electrically-passive, broad-band LHCP electromagnetic radiation reflecting panels can be made using the fabrication methods disclosed in International Publication No. WO 97/16762, supra. In the preferred embodiment, the broad-band RHCP electromagnetic radiation reflecting panels 12A (12B) are fabricating by applying a coating of CLC-based ink (with suspended CLC flakes therein) onto a conventional glass panel, as taught in International Publication No. WO 97/16762, supra. Alternatively, narrow-band RHCP electromagnetic radiation reflecting panels can be made using the fabrication methods disclosed in US Patent No. 5,506,704 to Broer, et al, or the methods disclosed in US Patent No. 5,221,982 to Faris.

Physically interfacing panels 11, 15A and 15B of the electro-optical glazing structure of Fig. 4 can be achieved using conventional lamination techniques well known in the glazing art.

In the illustrative embodiment of the glazing structure of Fig. 4, characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel 15A is designed to be substantially the same as characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel 15B. It is understood, however, that in alternative embodiments of the present

invention, such reflection characteristics may be specifically designed to partially overlap, or be separated from each other on the wavelength (i.e. frequency) domain in to provide desired reflection/transmission performance characteristics.

5           The electrically-active  $\pi$ -retardation panel 11 can be constructed using any of the techniques described in detail above.

The operation of the glazing structure of Fig. 4 will now be described with reference to Figs. 5A and 5B, where the  $\pi$ -phase retardation panel 11 of Fig. 2C is used in the construction of the  
10           glazing structure.

As shown in Fig. 5A, the electro-optical glazing structure of Fig. 4 is switched to its optically opaque state of operation by applying the appropriate control voltage thereacross (i.e.  $V = 0$  Volts). In this optical state, the electro-optical glazing structure 14 reflects both  
15           LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident the window panel, independent of its direction of propagation. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 5A.

20           Inasmuch as 100% of incident electromagnetic radiation is reflected from the surface of the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

As shown in Fig. 5B, the electro-optical glazing structure of Fig. 4 is switched to its optically semi-transparent (i.e. semi-clear state)  
25           of operation by applying the appropriate control voltage thereacross (i.e.  $V = 20$  Volts). In this optical state, the electro-optical glazing structure 14 reflects LHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident the window panel, independent of its direction of propagation, while transmitting RHCP electromagnetic radiation

within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident the window panel, independent of the direction of electromagnetic radiation propagation. As such, the operation of this particular electro-optical glazing structure is “symmetrical”. The physical mechanisms associated with such reflection and transmission processes are schematically illustrated in Fig. 5A. Inasmuch as 50% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, while 50% of such electromagnetic radiation is reflected therefrom, this glazing structure is “partially transmissive” in this state of operation.

### Third Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The third illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 6 through 7B. As shown in Fig. 6, the electro-optical glazing structure of the third illustrative embodiment 17 comprises: an electrically-active  $\pi$ -phase retardation panel 11 interposed between an electrically-passive LHCP electromagnetic radiation reflecting panel 18A and an electrically-passive RHCP electromagnetic radiation reflecting panel 18B; and electrically conductive means 19 for applying optical-state control voltages to the electrically-active  $\pi$ -phase retardation panel 11. Preferably, the electro-optical glazing structure of Fig 6 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

As illustrated in Figs. 6A and 6B, electromagnetic radiation having a LHCP polarization state and a wavelength inside the

characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel 18A is reflected directly therefrom without absorption, while electromagnetic radiation having either a RHCP polarization state and/or a wavelength outside the characteristic reflection band  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption. In the preferred embodiment, the broad-band RHCP electromagnetic radiation reflecting panels 18A are fabricating by applying a coating of CLC-based ink (with suspended CLC flakes therein) onto a conventional glass panel, as taught in International Publication No. WO 97/16762, and described hereinabove.

Alternatively, narrow-band RHCP electromagnetic radiation reflecting panels 18A can be made using the fabrication methods disclosed in US Patent No. 5,221,982 to Faris, and while less preferred, using the methods disclosed in US Patent No. 5,506,704 to Broer, et al.

As illustrated in Figs. 6C and 6D, electromagnetic radiation having a RHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 18B is reflected directly therefrom without absorption, while electromagnetic radiation having either a LHCP polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption. In the preferred embodiment, the broad-band RHCP electromagnetic radiation reflecting panels 18B are fabricating by applying a coating of CLC-based ink (with suspended CLC flakes therein) onto a conventional glass panel, as taught in International Publication No. WO 97/16762, and described hereinabove. Alternatively, narrow-band RHCP electromagnetic

radiation reflecting panels 18B can be made using the fabrication methods disclosed in US Patent No. 5,221,982 to Faris, and using the less preferred techniques disclosed in US Patent No. 5,506,704 to Broer, et al.

5 In the illustrative embodiment of the glazing structure of Fig. 6, characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 18B is designed to be substantially the same as characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel 18A. It is understood, however, that in alternative embodiments of the present invention, such reflection bandwidth characteristics may be specifically designed to partially overlap, or be separated from each other on the wavelength (i.e. frequency) domain in to provide desired reflection/transmission performance characteristics.

15 Electrically-active  $\pi$  retardation panel 11 can be realized using any of the construction techniques described in detail above. Physically interfacing panels 11, 18A and 18B of the electro-optical glazing structure of Fig. 6 can be achieved using conventional lamination techniques well known in the glazing art.

20 The operation of the glazing structure of Fig. 6 will now be described with reference to Figs. 7A and 7B, where the  $\pi$ -phase retardation panel 11 of Fig. 2C is used in the construction of the glazing structure.

25 As shown in Fig. 7A, the electro-optical glazing structure of Fig. 6 is switched to its semi-optically transparent (i.e. clear) state of operation by applying the appropriate control voltage thereacross (i.e.  $V = 0$  Volts). In this optical state, the electro-optical glazing structure reflects LHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$

incident on the LHCP electromagnetic radiation reflecting panel 18A of the window panel, while transmitting RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident thereto and converting the same into LHCP electromagnetic radiation by the  $\pi$ -phase shifter as it emanates from the RHCP electromagnetic radiation reflecting panel 18B. In this optical state, the electro-optical glazing structure reflects RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident on the RHCP electromagnetic radiation reflecting panel 18B of the window panel, while transmitting LHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident thereto and converting the same into RHCP electromagnetic radiation as it emanates from the LHCP electromagnetic radiation reflecting panel 18A. As such, the operation of this particular electro-optical glazing structure is "assymmetrical". The physical mechanisms associated with such reflection and transmission-reflection processes are schematically illustrated in Fig. 7A in great detail. Inasmuch as 50% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, while 50% of such electromagnetic radiation is reflected therefrom, this glazing structure is "partially transmissive" in this state of operation.

As shown in Fig. 7B, the electro-optical glazing structure of Fig. 6 is switched to its optically opaque state of operation by applying the appropriate control voltage thereacross (i.e.  $V = 20$  Volts). In this optical state, the electro-optical glazing structure reflects LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident on the LHCP electromagnetic radiation reflecting panel of the window panel. In this optical state, the electro-optical glazing structure 17 also reflects RHCP and LHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident on the RHCP electromagnetic radiation reflecting panel 18B of the

window panel. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection and transmission-reflection processes are schematically illustrated in Fig. 7B in great detail. Inasmuch as 100% of incident electromagnetic radiation is reflected from the surface of the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

#### Fourth Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The fourth illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 8 through 9B. As shown in Fig. 8, the electro-optical glazing structure of the fourth illustrative embodiment 19 comprises: an electrically-passive linear polarization direction rotating panel 19C interposed between a first electrically-active linearly polarizing electromagnetic radiation reflecting panel 19A having linearly polarization state LP1, and a second electrically-active LHCP electromagnetic radiation reflecting panel 19C having linearly polarization state LP2, orthogonal to LP1 or parallel; and electrically conductive means 19D for applying optical-state control voltages to the electrically-active LHCP electromagnetic radiation reflecting panels 19B and 19C. Preferably, the electro-optical glazing structure of Fig. 8 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

In Figs. 8A and 8B, the reflection characteristics of electrically-passive LP1 electromagnetic radiation reflecting panel 19B are



illustrated. As shown, electromagnetic radiation having a LP1 polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LP1}}$  of the LP1 electromagnetic radiation reflecting panel is reflected directly therefrom without absorption, while electromagnetic radiation having either a LP2 polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$  of the LP2 electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption.

In Figs. 8C and 8D, the reflection characteristics of electrically-active LP2 electromagnetic radiation reflecting panel 19C are illustrated. As shown in Figs. 8C and 8D, electromagnetic radiation having a LP1 polarization state and any wavelength within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{LP2}}$  is transmitted directly through the glazing panel without absorption, while electromagnetic radiation having either a LP2 polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$  of the LP2 electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption.

Electrically-passive LP1 and LP2 polarization reflective panels 19A and 19B can be made from super broad-band CLC film taught in International Publication No. WO 97/16762 by Reveo, Inc., and while less preferred, using the fabrication methods disclosed in US Patent No. 5,221,982 to Faris, and in US Patent No. 5,506,704 to Broer, et al, each of these references incorporated herein by reference in its entirety. These applications disclose how to make circularly polarizing reflective CLC films. Such films can be converted into linearly polarizing CLC films using the novel phase-retardation imparting techniques taught in great detail in International Application Serial No. PCT/US97/20091 entitled "Liquid Crystal Film

Structures With Phase-Retardation Surface Regions Formed Therein” by Reveo, Inc., incorporated herein by reference in its entirety. The methods taught therein allows one to make an electrically-passive, broad-band linear polarizing panel from a single layer of CLC film material, without laminating a  $\pi/2$  phase-retardation panel to a layer of circularly polarizing CLC film.

An alternative method of making broad-band linearly polarizing reflective panels 19A and 19B is disclosed in US Patent No. 5,506,704 to Broer, et al. However, the fabrication techniques disclosed therein are less preferred than those taught in International Application Serial No. PCT/US97/20091, as the technique disclosed in US Patent No. 5,506,704 requires laminating a  $\pi/2$  phase retardation panel to a circularly polarizing CLC film layer, which complicates manufacture and increases manufacturing costs.

The electronically-switchable linear polarization direction rotating panel 19C employed in the electro-optical glazing structure of Fig. 8 can be realized as an electrically-controlled birefringence (ECB) cell, surface stabilized ferroelectric liquid crystal (SSFLC) cell, twisted nematic (TN) liquid crystal cell, super-twisted nematic (STN) liquid crystal cell, or CLC cell, whose operation is controlled by a control voltage well known in the art. To construct the linear polarization rotating cell 19C, a layer of liquid crystal material is contained between a spaced apart pair of glass panels bearing layers of ITO on the interior surfaces thereof, and rubbed polyimide to provide liquid crystal alignment in a manner well known in the art. The ITO layers are used to create the necessary voltage across the layer of liquid crystal material and align the liquid crystal molecules, thereby preventing rotation of the polarization direction of linearly polarized light being transmitted therethrough during operation of

the electro-optical glazing structure.

Physically interfacing panels 19A, 19B and 19C of the electro-optical glazing structure of Fig. 8 can be achieved using conventional lamination techniques well known in the glazing art.

5 The operation of the glazing structure of Fig. 8 will now be described with reference to Figs. 9A and 9B.

As shown in Fig. 9A, the electro-optical glazing structure of Fig. 8 is switched to its optically opaque state of operation by not applying a control voltage thereacross (i.e.  $V=0$ ). In this optical state, the electro-optical glazing structure 19 reflects LP1  
10 electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LP1}}$  incident on the LP1 electromagnetic radiation reflecting panel without adsorption, while transmitting LP2 electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LP1}}$  incident thereto without adsorption. Also in this optical state, the electro-optical glazing structure 19 reflects LP2 electromagnetic radiation  
15 within  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$  incident on the LP2 electromagnetic radiation reflecting panel without adsorption, while transmitting LP1 electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$  incident thereto without adsorption. As such, the operation of this particular electro-optical glazing structure is "asymmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 9A in great detail. Inasmuch as 50% of incident  
20 electromagnetic radiation is reflected from the electro-optical glazing structure and 50% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is "partially reflective" in this state of operation.  
25

As shown in Fig. 9B, the electro-optical glazing structure of Fig. 8 is switched to its optically transparent (i.e. clear) state of operation by applying the appropriate control voltage thereacross (i.e.  $V=1$ ). In

this optical state, the electro-optical glazing structure 19 reflects both LP1 and LP2 electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LP1}}$  and  $\Delta\lambda_{\text{reflection}}^{\text{LP2}}$  incident on either electromagnetic radiation reflecting panel of the window panel without adsorption, independent of the direction of propagation of the incident electromagnetic radiation. As such, the operation of this particular electro-optical glazing structure is “symmetrical”. The physical mechanisms associated with such transmission processes are schematically illustrated in Fig. 9B in great detail. Inasmuch as 100% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is “totally opaque” in this state of operation.

The electro-optical glazing structure of Fig. 8 can be readily adapted to exhibit “asymmetrical” reflection/transmission characteristics over its broad-band of operation by tuning the spectral transmission characteristics of both the CLC-based LP1 and LP2 electromagnetic radiation reflecting panels 19A and 19B of the illustrative embodiment so that the spectral reflection (and transmission) bandwidth characteristics thereof are either completely or partially overlapping or are separated on the wavelength (i.e. frequency) domain. Using such CLC-tuning techniques, it is possible to create an electro-optical glazing structure having the construction of Fig. 8 which, when switched to its first optical state, is capable of totally reflecting electromagnetic radiation within a desired reflection band (e.g. within the ultraviolet and infrared bands) in a first direction defined with respect to the panel, and when switched to its second optical state, totally transmitting electromagnetic radiation within such reflection band.

Fifth Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The fifth illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 10 through 11C2.

As shown in Fig. 10, the electro-optical glazing structure of the fifth illustrative embodiment 20 comprises: an electrically-passive  $\pi$ -phase retardation panel 21 interposed between a first electrically-active LHCP electromagnetic radiation reflecting panel 22A and a second electrically-active LHCP electromagnetic radiation reflecting panel 22B; and electrically conductive means 23 for applying optical-state control voltages to the electrically-active LHCP electromagnetic radiation reflecting panels 22A and 22B. Preferably, the electro-optical glazing structure of Fig 10 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

In Fig. 10A, electrically-active LHCP electromagnetic radiation reflecting panel 22A is shown operated in its electrically inactive state (i.e. when  $V=0$ ). As shown in Fig. 10C, electromagnetic radiation having a LHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel is reflected directly therefrom without absorption, while electromagnetic radiation having either a RHCP polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of the LHCP electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption.

In Fig. 10B, the electrically-active LHCP electromagnetic radiation reflecting panel 22B is shown operated in its electrically active state (i.e. when  $V=1$ ). As shown in Fig. 10D, electromagnetic radiation having a LHCP or RHCP polarization state and any wavelength within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$  is transmitted directly through the glazing panel without absorption.

The electrically-passive  $\pi$ -phase retardation panel 21 employed in the electro-optical glazing structure of Fig. 10 can be made from any material having a permanent birefringence which imparts to a  $\pi$ -phase retardation to electromagnetic radiation (within the operational band of the device). This panel can be fabricated from PVA, nematic liquid crystal, mica, etc. in a manner well known in the art. Methods for making such optical devices are disclosed in US Patent No. 5,113,285 to Franklin, et al., incorporated herein by reference.

Electrically-switchable circularly polarizing reflective panels 22A and 22B can be fabricated using the construction techniques illustrated in Figs. 11 through 11A3. As shown in Fig. 11, each such panel generally comprises a pair of optically transparent plates 22A1 and 22A2 (e.g. made of glass, acrylic, etc.) spaced apart by a spacers 22A3 in a manner known in the art. In the illustrative embodiment, the spacing between the plates is about 20 microns, however, it is understood that such dimensions may vary from embodiment to embodiment of the invention. The internal surfaces of the plates are coated with a layer of ITO material 22A4 and 22A to form optically transparent electrode surfaces. A polyimide coating is applied over the ITO layers, which is then rubbed to create director (i.e. alignment) surfaces for liquid crystal molecules to spontaneously order in accordance with the chiral phase, in a manner well known in

the art. Electrical leads are attached to the ITO layers.

Having formed a cell between the spaced apart plates 22A1 and 22A2, a cholesteric liquid crystal (CLC) mixture 22A6 is prepared and then poured into the interior volume of the "cell" formed  
5 between the plates and spacers. In the illustrative embodiment set forth in Fig. 10, a "left-hand CLC formula" must be used to make the CLC mixture for the electrically switchable LCHP panels 22A and 22B. In the illustrative embodiment set forth in Fig. 12, a "right-hand CLC formula" must be used to make the CLC mixture for the electrically  
10 switchable RCHP panels 25A and 25B. In the illustrative embodiment set forth in Fig. 14, a "left-hand CLC formula" must be used to make the CLC mixture for the electrically switchable LHCP panel 28A, and a "right-hand CLC formula" must be used to make the CLC mixture for the electrically switchable RHCP panel 28B. These  
15 CLC formulas will be described in detail below.

According to the left-handed CLC formula, the following material components are measured and mixed together in a vessel, in the hereinafter specified "by weight" proportions, namely: 1 weight unit of liquid crystal polymerizable material having a left-handed  
20 cholesteric order (phase) (e.g. CC4039L from Wacker Chemical, Germany); 49.4 weight units of low-molecular weight nematic liquid crystal material (e.g. E7 from EMI, Inc. of Hawthorne, New York); 0.026 weight units of UV photoinitiator (e.g. IG184 from Ciba Gigy); 0.30 weight units of a first left-handed chiral additive (e.g. R1011  
25 from EMI, Inc.); and 0.42 weight units of a second left-handed chiral additive (e.g. CB15 from EMI, Inc.).

According to the right-handed CLC formula, the following material components are measured and mixed together in a vessel, in the hereinafter specified "by weight" proportions, namely: 1 weight  
30 unit of liquid crystal polymerizable material having a right-handed

cholesteric order (phase) (e.g. CC4039R from Wacker Chemical, Germany); 49.4 weight units of low-molecular weight nematic liquid crystal material (e.g. E7 from EMI, Inc. Of Hawthorne, New York); 0.026 weight units of UV photoinitiator (e.g. IG184 from Ciba-Gigy); 0.30 weight units of a first right-handed chiral additive (e.g. R1011 from EMI, Inc.); and 0.42 weight units of a second right-handed chiral additive (e.g. CB15 from EMI, Inc.). The spectral reflection characteristics for this particular right-handed CLC material (prior to UV polymerization) are shown in Fig. 11A1.

After the appropriate CLC mixture has been made and poured into the cell region between the glass plates 22A1 and 22A2, the panel structure is placed in a temperature-controlled curing cabinet containing a UV light source of controlled light intensity. The CLC panel structure is then cured within the cabinet. For the case of the above-described embodiment, using the above-described CLC mixture formulas, the CLC structure is cured for 12 hours while being maintained at 25°C and exposed to UV light of 365nm and power density 0.72mW/cm<sup>2</sup>.

In Fig. 11A1, the reflection characteristics of the RHCP CLC panel prior to UV polymerization are shown. In Fig. 11A2, the reflection characteristics for the RHCP CLC panel after UV polymerization are shown when no voltage has been applied across the ITO coated plates. Notably, after UV polymerization, the reflection bandwidth of the CLC material has doubled. In Fig. 11A3, the reflection characteristics for the RHCP CLC panel are shown when a voltage has been applied. Notably, the big reflection peak shown in Fig. 11A2 disappears due to the unwinding of the CLC helix of the CLC panel in the presence of the electric field created by the applied voltage. However, a weak peak is still observed in the reflection



characteristics of this example due to the fact that the applied voltage had not been high sufficiently high enough intensity.

Having constructed the various subcomponents of the electro-optical glazing structure of Fig. 10, panels 21, 22A and 22B can then be physically interfaced as an integral unit using conventional lamination techniques well known in the glazing art.

The operation of the glazing structure shown in Fig. 10 will now be described with reference to Figs. 10E and 10F.

As shown in Fig. 10E, the electro-optical glazing structure of Fig. 10 is switched to its optically opaque state of operation by not applying a control voltage thereacross (i.e.  $V=0$ ). In this optical state, the electro-optical glazing structure 20 reflects LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident on either LHCP electromagnetic radiation reflecting panel without adsorption, independent of the direction of propagation thereof, as shown in Fig. 10E. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 10E in great detail. Inasmuch as 100% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

As shown in Fig. 10F, the electro-optical glazing structure of Fig. 10 is switched to its optically transparent (i.e. clear) state of operation by applying the appropriate control voltage thereacross (i.e.  $V=1$ ). In this optical state, the electro-optical glazing structure 20 transmits both LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  incident on either LHCP electromagnetic radiation reflecting panel of the window panel without adsorption, independent of the direction of propagation of the incident electromagnetic radiation. As

such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such transmission processes are schematically illustrated in Fig. 10F in great detail. Inasmuch as 100% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is "totally transmissive" in this state of operation.

The electro-optical glazing structure of Fig. 10 can be readily adapted to exhibit "asymmetrical" reflection/transmission characteristics over its broad-band of operation by tuning the spectral transmission characteristics of both the CLC-based LHCP electromagnetic radiation reflecting panels 22A and 22B so that the spectral reflection (and transmission) bandwidth characteristics thereof are either completely or partially overlapping or are separated on the wavelength (i.e. frequency) domain. Using such CLC-tuning techniques, it is possible to create an electro-optical glazing structure having the construction of Fig. 10 which, when switched to its first optical state, is capable of totally reflecting electromagnetic radiation within a desired reflection band (e.g. within the ultraviolet and infrared bands) in a first direction defined with respect to the panel, and when switched to its second optical state, totally transmitting electromagnetic radiation within such reflection band.

#### Sixth Illustrative Embodiment Of The Electro-Optical Glazing Structure Of The Present Invention

The sixth illustrative embodiment of the electro-optical glazing structure hereof will be described with reference to Figs. 12 through 13B.

As shown in Fig. 12, the electro-optical glazing structure of the

sixth illustrative embodiment 24 comprises: an electrically-passive  $\pi$ -phase retardation panel 21 interposed between a first electrically-active RHCP electromagnetic radiation reflecting panel 25A and a second electrically-active RHCP electromagnetic radiation reflecting panel 25B; and electrically conductive means 26 for applying optical-state control voltages to the electrically-active RHCP electromagnetic radiation reflecting panels 25A and 25B. Preferably, the electro-optical glazing structure of Fig 12 is mounted within a frame structure as described in connection with the generalized embodiment shown in Figs. 1A and 1B, and incorporates all of the power generation, electromagnetic radiation detection and micro-control mechanisms thereof.

In Fig. 12A, the electrically-active RHCP electromagnetic radiation reflecting panel 25A (25B) is shown being operated in its electrically inactive state (i.e. when  $V=0$ ). As shown in Fig. 12B, electromagnetic radiation having a RHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 25A (25B) is reflected directly therefrom without absorption, while electromagnetic radiation having either a LHCP polarization state and/or a wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel is transmitted directly therethrough without absorption.

In Fig. 12C, the electrically-active RHCP electromagnetic radiation reflecting panel 25A (25B) is shown being operated in its electrically active state (i.e. when  $V=1$ ). As shown in Fig. 12D, electromagnetic radiation having a LHCP or RHCP polarization state and any wavelength within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{RHCP}}$  is transmitted directly through the electro-optical panel without

absorption.

The electrically-passive  $\pi$ -phase retardation panel 21 employed in the electro-optical glazing structure of Fig. 12 can be realized in the manner described above in connection with the embodiment shown in Fig. 12 above. The electrically-active, broad-band LHCP electromagnetic radiation reflecting panels 25A and 25B used in the glazing structure of Fig. 10 can be made using the fabrication methods described above in connection with the embodiment shown in Fig. 10. Physically interfacing panels 21, 25A and 25B of the electro-optical glazing structure of Fig. 12 can be achieved using conventional lamination techniques well known in the glazing art.

The operation of the glazing structure of Fig. 12 will now be described with reference to Figs. 13A and 13B.

As shown in Fig. 13A, the electro-optical glazing structure of Fig. 12 is switched to its optically opaque state of operation by not applying a control voltage thereacross (e.g.  $V=0$  Volts). In this optical state, the electro-optical glazing structure 24 reflects LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident on the RHCP electromagnetic radiation reflecting panel 25A (25B) of the window panel without adsorption, independent of the direction of propagation of the incident electromagnetic radiation. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 13A in great detail. Inasmuch as 100% of incident electromagnetic radiation is reflected from the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

As shown in Fig. 13B, the electro-optical glazing structure of

Fig. 12 is switched to its optically transparent (i.e. clear) state of operation by applying the appropriate control voltage thereacross (e.g.  $V=1$  Volts). In this optical state, the electro-optical glazing structure 24 transmits both LHCP and RHCP electromagnetic radiation within  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident on either RHCP electromagnetic radiation reflecting panel 25A (or 25B) without adsorption, independent of the direction of propagation of the incident electromagnetic radiation. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such transmission processes are schematically illustrated in Fig. 13B in great detail. Inasmuch as 100% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is "totally transmissive" in this state of operation.

The electro-optical glazing structure of Fig. 12 can be readily adapted to exhibit "asymmetrical" reflection/transmission characteristics over its broad-band of operation by tuning the spectral transmission characteristics of both the CLC-based RHCP electromagnetic radiation reflecting panels 25A and 25B so that the spectral reflection (and transmission) bandwidth characteristics thereof are either completely or partially overlapping or are separated on the wavelength (i.e. frequency) domain. Using CLC-tuning techniques, it is possible to create an electro-optical glazing structure having the construction of Fig. 12 which, when switched to its first optical state, is capable of totally reflecting electromagnetic radiation within a desired reflection bandwidth (e.g. within the ultraviolet and infrared bands) in a direction defined with respect to the panel, and when switched to its second optical state, totally transmitting electromagnetic radiation within such reflection band.

Seventh Illustrative Embodiment Of The Electro-Optical Glazing  
Structure Of The Present Invention

The seventh illustrative embodiment of the electro-optical  
5 glazing structure hereof will be described with reference to Figs. 14  
through 15B.

As shown in Fig. 14, the electro-optical glazing structure of the  
seventh illustrative embodiment 27 comprises: an electrically-active  
10 LHCP electromagnetic radiation reflecting panel 28A; an electrically-  
active RHCP electromagnetic radiation reflecting panel 28B laminated  
to panel 28A; and electrically conductive means 29 for applying  
optical-state control voltages to the electrically-active LHCP and RHCP  
electromagnetic radiation reflecting panels 28A and 28B. Preferably,  
15 the electro-optical glazing structure of Fig 14 is mounted within a  
frame structure as described in connection with the generalized  
embodiment shown in Figs. 1A and 1B, and incorporates all of the  
power generation, electromagnetic radiation detection and micro-  
control mechanisms thereof.

In Fig. 14A, the electrically-active LHCP electromagnetic  
20 radiation reflecting panel 28A is shown being operated in its  
electrically inactive state (i.e. when  $V=0$ ). As shown in Fig. 14B,  
electromagnetic radiation having a LHCP polarization state and a  
wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of  
the LHCP electromagnetic radiation reflecting panel 28A is reflected  
25 directly therefrom without absorption, while electromagnetic  
radiation having either a RHCP polarization state and/or a  
wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$  of  
the LHCP electromagnetic radiation reflecting panel 28A is  
transmitted directly therethrough without absorption.

30 In Fig. 14C, the electrically-active LHCP electromagnetic

radiation reflecting panel 28B is shown being operated in its electrically active state (i.e. when  $V=1$ ). As shown in Fig. 14D, electromagnetic radiation having a LHCP or RHCP polarization state and any wavelength within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$  is  
 5 transmitted directly through the electro-optical panel 28A without absorption.

In Fig. 14E, the electrically-active RHCP electromagnetic radiation reflecting panel 28B is shown being operated in its electrically inactive state (i.e. when  $V=0$ ). As shown in Fig. 14F,  
 10 electromagnetic radiation having a RHCP polarization state and a wavelength inside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 28B is reflected directly therefrom without absorption, while electromagnetic radiation having either a LHCP polarization state and/or a  
 15 wavelength outside the characteristic reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  of the RHCP electromagnetic radiation reflecting panel 28B is transmitted directly therethrough without absorption.

In Fig. 14G, the electrically-active RHCP electromagnetic radiation reflecting panel 28B is shown being operated in its electrically active state (i.e. when  $V=1$ ). As shown in Fig. 14H,  
 20 electromagnetic radiation having a LHCP or RHCP polarization state and any wavelength within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{RHCP}}$  is transmitted directly through the electro-optical panel 28B without absorption.

25 The electrically-active, broad-band LHCP and RHCP electromagnetic radiation reflecting panels 28A and 28B used in the glazing structure of Fig. 14 can be made using the fabrication methods described above in connection with the embodiment shown in Fig. 10. In the preferred embodiment, the liquid crystal polymer

material contained within panel 28A can be made using the following formula: CLC polymer (BASF 171): 12%; CB15: 25%; E44: 64%; IG184: 1%. The sample is made by filling the mixture into a pair of buffed polyimide ITO glass substitutes. UV curing intensity is  $10^5 \text{ w/cm}^2$ .  
5 A similar formula is used to make the liquid crystal polymer material contained within panel 28B.

Physically interfacing panels 28A and 28B of the electro-optical glazing structure of Fig. 14 can be achieved using conventional lamination techniques well known in the glazing art.

10 The operation of the glazing structure of Fig. 14 will now be described with reference to Figs. 15A and 15B.

As shown in Fig. 15A, the electro-optical glazing structure of Fig. 14 is switched to its optically opaque state of operation by not applying a control voltage thereacross (i.e.  $V=0$ ). In this optical  
15 state, the electro-optical glazing structure 27 reflects LHCP and RHCP electromagnetic radiation within reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{LHCP}}$

incident on the LHCP electromagnetic radiation reflecting panel 28A without adsorption, while reflecting LHCP and RHCP electromagnetic radiation within reflection bandwidth  $\Delta\lambda_{\text{reflection}}^{\text{RHCP}}$  incident on the RHCP

20 electromagnetic radiation reflecting panel 28B without adsorption. As such, the operation of this particular electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such reflection processes are schematically illustrated in Fig. 15A in great detail. Inasmuch as 100% of incident electromagnetic radiation  
25 is reflected from the electro-optical glazing structure, this glazing structure is "totally reflective" in this state of operation.

As shown in Fig. 15B, the electro-optical glazing structure of Fig. 14 is switched to its optically transparent (i.e. clear) state of operation by applying the appropriate control voltage thereacross



(i.e.  $V=1$ ). Assuming that the LHCP electromagnetic radiation reflecting panel 28A and RHCP electromagnetic radiation reflecting panel 28B each have the same characteristic transmission bandwidth (i.e.  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$  is the same as  $\Delta\lambda_{\text{transmission}}^{\text{RHCP}}$ ), then when switched in this optical state, the electro-optical glazing structure of Fig. 14 transmits without adsorption, both LHCP and RHCP wavelengths within transmission bandwidth  $\Delta\lambda_{\text{transmission}}^{\text{LHCP}}$  independent of whether such wavelengths fall incident on either the LHCP or RHCP electromagnetic radiation reflecting panel of the electro-optical glazing structure. As such, the operation of this particular embodiment of the electro-optical glazing structure is "symmetrical". The physical mechanisms associated with such transmission processes are schematically illustrated in Fig. 15B in great detail. Inasmuch as 100% of incident electromagnetic radiation is transmitted through the electro-optical glazing structure, this glazing structure is "totally transmissive" in this state of operation.

Notably, the electro-optical glazing structure of Fig. 14 can be readily adapted to exhibit "asymmetrical" reflection/transmission characteristics over its broad-band of operation. Such characteristics can be imparted by tuning the spectral transmission characteristics of both the CLC-based RHCP and LHCP electromagnetic radiation reflecting panels 28A and 28B of the present invention so that the spectral characteristics thereof are either completely or partially overlapping or are separated on the wavelength (or frequency) domain. Using CLC-tuning techniques disclosed in International Publication No. WO 97/16762, it is possible to create an electro-optical glazing structure which, when switched to its first optical state, is capable of totally reflecting electromagnetic radiation within a desired reflection bandwidth (e.g. within the UV and IR bands) in a

direction defined with respect to the panel, and when switched to its second optical state, totally transmitting electromagnetic radiation within the reflection band.

Alternatively, the electrically-active LHCP and RHCP reflecting panels 28A and 28B panels in the glazing structure of Fig. 14 can be realized using the novel electro-optical construction schematically illustrated in Figs. 16A and 16B.

As shown in Figs. 16A and 16B, the physical construction of this alternative embodiment of the electrically-switchable broad-band CLC panels 28A (28B) is very similar to that of the panels described above in connection with Figs. 11 through 11A3. However, in this alternative embodiment shown in Figs. 16A and 16B, the broad-band (or super broad-band) CLC material contained between glass plates thereof is radically different from that contained with the panel illustrated in Figs. 11 through 11A3, as will be explained below.

The novel material contained between the plates of this novel electrically-switchable super-broadband CLC (BBCLC) polarizer is made from polymerizable liquid crystal blends in cholesteric order. According to this aspect of the present invention, "functional pigment suspended liquid crystal" (FPSLC) material is created by mixing (i) broad-band CLC pigments (e.g. CLC microflakes taught in International Publication No. WO 97/16762) into (ii) an electrically-active (i.e. electrically-responsive) carrier fluid such as a low-molecular weight (LMW) nematic liquid crystal fluid (e.g. E7 and E44) which is commercially available from EMI of Hawthorne, New York. As will be explained in greater detail hereinafter, the micro-sized functional pigments of this particular embodiment have unique optical properties that can be exploited in various applications including electro-optical glazing structures. In the illustrative embodiment, the functional pigments are realized using BBCLC

microflakes having a size in the range of about 20-100 microns.

When making the LHCP panel 28A, left-handed BBCLC microflakes should be used, whereas when making the RHCP panel 28B, right-handed BBCLC microflakes should be used. The mass density of the CLC microflakes should be substantially equal to the mass density of the LMW carrier liquid fluid. Also the refractive index of the CLC microflakes should be matched closely to the refractive index of the carrier fluid.

Once prepared, the FPSLC mixture is poured into a cell constructed from a pair of spaced apart ITO-coated glass or plastic plates. To achieve the required liquid crystal alignment, the ITO layers are coated with rubbed polyimide in a manner well known in the art. The ITO layers are also provided with electrical leads so that an external field can be impressed across the ITO coated glass plates. As will be illustrated greater detail below, this makes the FPSLC material between the plates electrically-active or switchable between its electro-optical states of operation. Notably, when making such electrically-switchable plates, there is no UV polymerization step, as in the above-described fabrication methods.

After the filling operation, the CLC pigments are uniformly distributed inside the cell in order to cover the entire cell area. The cell thickness is designed to be larger than the pigment dimension. It is assumed that the liquid crystal molecules are spontaneously aligned in homogeneous state due to the surface coating. The homogeneous alignment of the host LC molecules forces the CLC pigments to align parallel to the cell surface, as shown in Fig. 16A. The switching or reorientation of the host liquid crystal molecules by an applied electric field forces the suspended CLC pigments to be reoriented accordingly, as shown in Fig. 16B. For purposes of convention, it will be helpful to designate state "A" of the host liquid

crystal as the state when there is no electrical field is applied, as illustrated in Fig. 16A. Accordingly, the CLC pigments are assigned to be in state " $A_{clc}$ ". Once a strong enough field, e.g., an electric field, is applied, the host liquid crystal molecules are reoriented to state "B" as shown in Fig. 16B. Accordingly, the CLC pigments are reoriented from state " $A_{clc}$ " to state " $B_{clc}$ ". Since the BBCLC pigments in the host liquid crystal preserve the same polarization property, then its parallel orientation should exhibit a polarizing state for an incoming light onto the cell surface. If the CLC microflakes are vertically aligned due to the reorientation of the host liquid crystal molecules under an applied field, then the cell loses the capability to polarize light and becomes transparent or quasi-transparent, i.e. provided that the thickness of the CLC microflakes is much smaller than the aerial dimension of the electro-optical cell.

The electrically-switchable circularly polarizing panels of the type shown in Figs. 16A and 16B can be realized in a variety of configurations. These alternative configurations will be described below.

#### Parallel-To-Vertical Configuration (Case I)

In this configuration, the cell is constructed so that the host *nematic* liquid crystal adopts a spontaneous alignment in *homogeneous* state. The ITO substrate is coated with a polyimide favorable for such an alignment followed by a mechanical rubbing. If the host liquid crystal has a *positive* dielectric anisotropy, it can be vertically reoriented into a *homeotropic* state by an electric field (E-field). In this case, state "A" of the host LC refers to *homogeneous*, and state "B" to *homeotropic*; while state " $A_{clc}$ " and " $B_{clc}$ " of the CLC pigments refers to *parallel* and *perpendicular* to the cell surface,

respectively, as schematically shown in Fig.16A. In this way, the panel can be switched from *polarizing reflection* to *transparent* or *quasi-transparent* state. Varying the strength of the E-field can change the final reflectivity of the panel. It should be pointed out that rubbed polyimide is not the only choice for surface treatment. Other techniques are also applicable, such as oblique deposition of SiO<sub>x</sub>, UV alignable layers, etc.

#### Parallel-To-Vertical Configuration (Case II)

In this configuration, the cell is constructed so that the host *low molecular weight (LMW) cholesteric* liquid crystal adopts a spontaneous alignment in the *planar* state. The pitch of the LMW CLC can be tuned either inside or outside of the CLC pigment reflection spectral region. The ITO substrate is coated with a rubbed polyimide favorable for planar alignment. If the host liquid crystal in cholesteric order has a *positive* dielectric anisotropy, it can be reoriented vertically into a *homeotropic* state by an electric field (E-field). In this case, state "A" of the host LC refers to *planar*, and state "B" to *homeotropic*; while state "A<sub>clc</sub>" and "B<sub>clc</sub>" of the CLC pigments refers to *parallel* and *perpendicular* to the cell surface, respectively. Thus the panel can be switched from *polarizing reflection* to *transparent* state. Varying the strength of the E-field can change the final reflectivity of the panel. It should be pointed out that rubbed polyimide is not the only choice for surface treatment. Other techniques are applicable, such as oblique deposition of SiO<sub>x</sub>, UV alignable layers, etc. In some cases, no alignment layer is required.

### Vertical-To-Parallel Configuration (Case I)

In this configuration, the cell is constructed so that the host *nematic* liquid crystal adopts a spontaneous alignment in *homeotropic* state. The ITO substrate is coated with an alignment agent favorable for such an alignment. No mechanical rubbing is necessary. If the host liquid crystal has a *negative* dielectric anisotropy, it can be reoriented into a *homogeneous* state by an electric field (E-field). In this case, state "A" of the host LC refers to *homeotropic*, and state "B" to *homogeneous*; while state " $A_{clc}$ " and " $B_{clc}$ " of the CLC pigments refer to *perpendicular* and *parallel* to the cell surface, respectively. Thus the panel can be switched from *transparent* to *polarizing reflection* state. Varying the strength of the E-field can change the final reflectivity of the panel.

### Vertical-To-Parallel Configuration (Case II)

In this configuration, the cell is constructed so that the host *low molecular weight (LMW) cholesteric* liquid crystal adopts a spontaneous alignment in *homeotropic* state. The pitch of the LMW CLC can be tuned either inside or outside of the CLC pigment reflection spectral region. The ITO substrate is coated with an alignment agent favorable for homeotropic alignment. If the host liquid crystal in cholesteric order has a *negative* dielectric anisotropy, it can be reoriented into a *planar* state by an electric field (E-field). In this case, state "A" of the host LC refers to *homeotropic*, and state "B" to *planar*; while state " $A_{clc}$ " and " $B_{clc}$ " of the CLC pigments refers to *perpendicular* and *parallel* to the cell surface, respectively. Thus the panel can be switched from *transparent* to *polarizing reflection* state. Varying the strength of the E-field can change the final reflectivity of the panel.

### FPSLC With Polymer Network

In this preferred configuration, the cell is constructed so that the host *low molecular weight (LMW)* liquid crystal in cholesteric order contains a small amount of polymer network which is formed by UV polymerizing a polymer material mixed inside the LMW LC in absence of any field. The purpose of introducing the polymer network is to realize a bistable state, i.e., weak scattering state and high reflection state of the panel and, possibly, improving the reflectivity. The polymer network helps to better confine CLC flakes in a preferred orientation, for example, a parallel orientation. The host liquid crystal can adopt either an ECB or TN or STN or cholesteric order. The ITO substrate is coated with a polyimide favorable for a homogeneous alignment. If the host liquid crystal in cholesteric order has a *positive* dielectric anisotropy, it can be reoriented from planar to homeotropic state by an electric field (E-field). In this case, state "A" of the host LC refers to homogeneous, and state "B" to *homeotropic*; while state " $A_{clc}$ " and " $B_{clc}$ " of the CLC pigments refers to *parallel* and *perpendicular* to the cell surface, respectively. Thus the panel can be switched from *polarizing reflection* to *semi-or total transparent* state. Varying the strength of the E-field can change the final reflectivity of the panel. Another important feature of this polymer stabilized FPSLC configuration is that a reflection and scattering mixed mode can be realized by properly controlling polymer density and applied voltage, similar to the conventional polymer stabilized cholesteric texture (PSCT).

### FPSLC With Surface Stabilization Function

In this preferred configuration, the cell is constructed so that the

host *low molecular weight (LMW)* liquid crystal in cholesteric order is surface stabilized which exhibits also a bistable state, i.e., weak scattering state and relatively high reflective state. This texture helps to better confine CLC flakes in a preferred orientation, for example, a parallel orientation. The ITO substrate is coated with a polyimide favorable for a homogeneous alignment. If the host liquid crystal in cholesteric order has a *positive* dielectric anisotropy, it can be reoriented from planar to homeotropic state by an electric field (E-field). In this case, state "A" of the host LC refers to homogeneous, and state "B" to *homeotropic*; while state " $A_{clc}$ " and " $B_{clc}$ " of the CLC pigments refers to *parallel* and *perpendicular* to the cell surface, respectively. Thus the panel can be switched from *polarizing reflection* to *semi-or total transparent* state. Varying the strength of the E-field can change the final reflectivity of the panel. Another important feature of this surface-stabilized FPSLC configuration is that a reflection and scattering mixed mode can be realized by properly controlling polymer density and applied voltage, similar to the conventional polymer stabilized cholesteric texture (PSCT).

Each of the cell configurations described above can be used to build a switchable (super) broadband FPSLC panel which is electrically switchable from *reflection* state to *transparent* state, or vice versa. The reflected light is polarized and can cover a broad spectral bandpass, such as the entire visible region. Ideally, in a perfect reflection state, 50% of the incident light is reflected into one polarization state and another 50% is transmitted in other polarization state. However, when switched into the total transmission mode, the panel passes 100% of the incident light. Varying the strength of the E-field can change the final reflectivity between 0% and 50% (equivalently, the transmittance can be varied



between 50% to 100%).

The electrically-switchable FPSLC-based structures described above can be used to realize the electrically-switchable circularly polarizing panels employed in the systems shown in Figs. 10 and 12 hereof. In such electro-optical glazing structures, the particular compositions used to create the FPSLC material will vary in order to provide the required polarization reflective functions. For example, when making broad-band LHCP panels 22A and 22B, left-handed BBCLC microflakes should be added to the LMW liquid crystal carrier fluid of the FPSLC mixture thereof. When making broad-band RHCP panels 25A and 25B, right-handed BBCLC microflakes should be added to the LMW liquid crystal carrier fluid of the FPSLC mixture thereof. When making RHCP panels 25A and 25B having spectrally-tuned reflection characteristics, right-handed BBCLC microflakes with narrow-band reflection characteristics should be added to the LMW liquid crystal carrier fluid of the FPSLC mixture thereof. For example, five color CLC microflakes (i.e. pigments) can be added into the LMW liquid crystal carrier fluid in order to cover the visible band. It is understood, various combinations of left and right handed CLC microflakes (having super broad-band, broad-band and/or narrow-band polarization reflection characteristics) can be added to the LMW liquid crystal carrier fluid in order to produce electrically-switchable circularly polarizing glazing structures having diverse polarization reflection characteristics adapted to meet any application imaginable.

Additional Embodiments Of The Electro-Optical Glazing Structure Of  
The Present Invention

Many more embodiments of the electro-optical glazing structure  
of the present invention can be provided by combining the above-  
described embodiments so provide systems and devices having  
transmission and reflection modes of operation.

In particular, the illustrative embodiments of the invention  
disclosed in Figs. 2 through 9B and Figs. 14 through 15B, in  
particular, can be readily combined with other structures to provide  
additional embodiments of the present invention. For simplicity of  
explanation, the embodiments described hereinabove are generalized  
in Figs. 21 through 23F.

In particular, Figs. 21 through 21F provide a generalized  
description of the illustrative embodiments disclosed in Figs. 6 and 8,  
wherein the electrically-passive broad-band polarizing layers have  
different handedness in both the circularly polarizing (RHCP/LHCP)  
and linearly polarizing (LP1/LP2) system configurations. Figs. 22  
through 22F provide a generalized description of the illustrative  
embodiments disclosed in Figs. 2 and 4, wherein the electrically-  
passive broad-band polarizing layers have the same handedness in  
both the circularly polarizing (LHCP/LHCP or RHCP/RHCP) and  
linearly polarizing (LP1/LP1 or LP2/LP2) system configurations.  
Before describing these additional embodiments of the electro-optical  
glazing structure hereof, the operation of these two generalized  
embodiments of the present invention will be briefly summarized.  
Likewise, Figs. 23 through 23F provide a generalized description of  
the illustrative embodiment disclosed in Figs. 14 through 15B,  
wherein the electrically-active broad-band polarizing layers have a  
different handedness in the circularly polarizing (LHCP/LHCP or

RHCP/RHCP) system configurations, and there is no optically active element disposed between the electrically-active polarizing layers.

Before describing additional embodiments of the electro-optical glazing structure hereof which can be based on the above-identified  
5       embodiments, it will be helpful to briefly summarize the structure and function of these embodiments hereinbelow in a more generalized manner to more clearly appreciate the various aspects of the present invention.

In Fig. 21A, the electro-optical glazing structure of Fig. 21 is  
10       shown operated in its partial-reflection/transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 21B and 21C, transmission and reflection characteristics for this mode of operation are shown, respectively. In Fig. 21D, the electro-optical light glazing structure of Fig. 21 is shown operated in its total-  
15       reflection mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 21E and 21F, transmission and reflection characteristics for this mode of operation are shown, respectively.

In Fig. 22A, the electro-optical glazing structure of Fig. 22 is  
20       shown operated in its total-reflection mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 22B and 22C, transmission and reflection characteristics for this mode of operation are shown, respectively. In Fig. 22D, the electro-optical light glazing structure of Fig. 22 is shown operated in its partial-  
25       reflection/transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 22E and 22F, transmission and reflection characteristics for this mode of operation are shown, respectively.

In Fig. 23A, the electro-optical glazing structure of Fig. 23 is

shown operated in its total-reflection mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 23B and 23C, transmission and reflection characteristics for this mode of operation are shown, respectively. In Fig. 23D, the electro-optical light glazing structure of Fig. 23 is shown operated in its total-transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the  $\pi$  phase shifter. In Figs. 23E and 23F, transmission and reflection characteristics for this mode of operation are shown, respectively.

In Fig. 24, an other illustrative embodiment of the electro-optical glazing structure of the present invention is shown comprising: a first electrically-passive broadband IR reflective polarizing panel for reflecting incident LHCP light within the broad IR band, and transmitting all other components of light; a second electrically-passive broadband IR reflective polarizing panel, laminated or mounted to the first IR reflective polarizing panel, for reflecting incident RHCP light within the broad IR band, and transmitting all other components of light. The resulting IR filter structure is mounted or affixed to an electrically-controlled light scattering panel, for selectively scattering light over the visible band (when no external voltage is applied) so as to render the resulting glazing structure opaque to provide privacy behind the window structure into which is installed. While circularly polarizing reflectors of the type taught in International Publication No WO/97/16762 by Reveo, Inc., incorporated herein by reference, can be used to realize the broad-band IR circularly-polarizing panels of this structure, it is understood that broad-band IR polarizers which reflect linearly polarized light, as taught in International Application No. PCT/US97/20091 by Reveo, Inc., incorporated herein by reference,

may also well be used to realize such linearly polarizing IR panels. Alternatively, such broadband IR reflecting panels may be made from multilayer polymer layers as disclosed in US Patent No. 5,686,979, incorporated herein by reference, and as taught elsewhere in the prior art. The electrically-controlled light scattering panel employed in the glazing structure of Fig. 24 can be realized by any one of the electrically-controlled light scattering panels disclosed in Figs. 17A through 20F, described in detail hereinbelow.

In Fig. 24A, the electro-optical glazing structure of Fig. 24 is shown operated in scattering mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the electrically-controlled scattering panel. In Figs. 24B and 24C, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electrically-controlled scattering panel renders the glazing structure optically opaque over the visible-band of the spectrum. In Fig. 24D, the electro-optical light glazing structure of Fig. 24 is shown operated in its total-transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to electrically-controlled light scattering panel. In Figs. 24E and 24F, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electrically-controlled scattering panel renders the glazing structure optically transparent over the visible-band of the spectrum enabling viewing through the glazing structure in bi-directional manner.

In Fig. 25, an other illustrative embodiment of the electro-optical

glazing structure of the present invention is shown. This is the reverse mode of the electro-optical glazing structure shown in Fig. 24. As shown, this glazing structure comprises: a first electrically-passive broadband IR reflective polarizing panel for reflecting incident LHCP light within the broad IR band, and transmitting all other components of light; a second electrically-passive broadband IR reflective polarizing panel, laminated or mounted to the first IR reflective polarizing panel, for reflecting incident RHCP light within the broad IR band, and transmitting all other components of light. As shown, the resulting IR filter structure is mounted or affixed to an electrically-controlled light scattering panel, for selectively scattering light over the visible band (when an external voltage is applied) so as to render the resulting glazing structure opaque to provide privacy behind the window structure into which is installed. While circularly polarizing reflectors of the type taught in International Publication No WO/97/16762 by Reveo, Inc., incorporated herein by reference, can be used to realize the broad-band IR circularly-polarizing panels of this structure, it is understood that broad-band IR polarizers which reflect linearly polarized light, as taught in PCT Application No. PCT/US97/20091 by Reveo, Inc., incorporated herein by reference, may also well be used to realize such linearly polarizing IR panels. Alternatively, such broadband IR reflecting panels may be made from multilayer polymer layers as are known in the art. Alternatively, such broadband IR reflecting panels may be made from multilayer polymer layers as disclosed in US Patent No. 5,686,979, incorporated herein by reference, and as taught elsewhere in the prior art. The electrically-controlled light scattering panel employed in the glazing structure of Fig. 24 can be realized by any one of the electrically-controlled light scattering panels disclosed in Figs. 17A through 20F, described in detail hereinbelow.

In Fig. 25A, the electro-optical glazing structure of Fig. 25 is shown operated in its light transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the electrically-controlled scattering panel. In Figs. 25B and 25C, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electrically-controlled scattering panel renders the glazing structure substantially transparent over the visible-band of the spectrum. In Fig. 25D, the electro-optical light glazing structure of Fig. 24 is shown operated in its light scattering mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to electrically-controlled light scattering panel. In Figs. 25E and 25F, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electrically-controlled scattering panel renders the glazing structure optically opaque over the visible-band of the spectrum preventing viewing through the glazing structure.

In Fig. 26, another embodiment of the electro-optical glazing structure of the present invention is disclosed. As shown, this electro-optical structure is constructed by adding the broad-band IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 22 wherein the broadband polarizing panels are each of the same handedness (e.g. RHCP/RHCP or LP1/LP1).

In Fig. 26A, the electro-optical glazing structure of Fig. 26 is shown operated in its total-transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifting panel disposed

between the pair of broadband polarizing reflective panels thereof. In Figs. 26B and 26C, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broadband IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 22) totally-reflects over the visible band in order to render the glazing structure substantially transparent over the visible-band of the spectrum. In Fig. 26D, the electro-optical light glazing structure of Fig. 26 is shown operated in its partial-reflection/transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{on}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof. In Figs. 26E and 26F, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 22) renders the glazing structure optically opaque over the visible-band of the spectrum preventing viewing through the glazing structure.

In Fig. 27, another embodiment of the electro-optical glazing structure of the present invention is disclosed which is operates in the "reverse" mode of the glazing structure of Fig. 26, described above. As shown in Fig. 27, this electro-optical structure is constructed by adding the broad-band IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 21 wherein the broadband polarizing panels are each of different handedness (e.g. RHCP/LHCP or LP1/LP2).



In Fig. 27A, the electro-optical glazing structure of Fig. 27 is shown operated in its partial-reflection/transmission mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof. In Figs. 27B and 27C, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broadband IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 21) partially-reflects and partially-transmits over the visible band in order to render the glazing structure semi-opaque over the visible-band of the spectrum. In Fig. 27D, the electro-optical light glazing structure of Fig. 27 is shown operated in its total-reflection mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the  $\pi$  phase shifting panel disposed between the pair of broadband polarizing reflective panels thereof. In Figs. 27E and 27F, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 21) renders the glazing structure optically opaque over the visible-band of the spectrum preventing viewing through the glazing structure.

In Fig. 28, another embodiment of the electro-optical glazing structure of the present invention is disclosed. As shown, this electro-optical structure is constructed by adding the broad-band IR filter panel shown in Figs. 24 and 25, to the electro-optical glazing structure shown in Fig. 23, wherein the electrically-active broadband

polarizing panels thereof are each of different handedness (i.e. RHCP/LHCP).

In Fig. 28A, the electro-optical glazing structure of Fig. 28 is shown operated in its total-reflection mode, wherein no external voltage (i.e.  $V=V_{\text{off}}$ ) is applied to the electrically-active circularly-polarizing reflective panels thereof. In Figs. 28B and 28C, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broadband IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 21) totally-reflects over the visible band in order to render the glazing structure optically opaque over the visible-band of the spectrum. In Fig. 28D, the electro-optical light glazing structure of Fig. 26 is shown operated in its total-transmission mode, wherein an external voltage  $V$  (i.e.  $V=V_{\text{on}}$ ) is applied to the electrically-active circularly-polarizing reflective panels thereof. In Figs. 28E and 28F, transmission and reflection characteristics for this mode of operation are shown, respectively. During this state operation, the composite broad-band IR filter structure totally reflects incident IR radiation providing excellent thermal insulation to the glazing structure, while the electro-optical glazing substructure (shown individually in Fig. 22) renders the glazing structure optically transparent over the visible-band of the spectrum.

Figs. 29A through 29C show a broad-band reflector for use in constructing broad-band circularly (and linearly) polarizing reflective panels employed in any one of embodiments of the electro-optical glazing panel hereof.

Fig. 29A shows a multilayer extruded polymer layer comprising a

number of pairs of layers. Each layer of a pair has a different index of refraction from the other layer of the pair. The various layers are of the order of a quarter wavelength of light, so that the electric field of the light reflecting from the layer boundaries adds in phase with light reflecting from other boundaries to increase reflection in a well known manner.

Fig. 29B shows the prior art distribution of the layer thicknesses. The thickness of the layers does not change with depth, changes in stepwise fashion, or changes in a linear fashion. Fig. 29C shows a non-linear change in the thickness of the layers with depth. As taught in International Publication No. WO/97/16762 by Reveo, Inc., a non linearly varying pitch is necessary for efficient broad band reflection from cholesteric liquid crystal material. The non-linearly varying pitch shown in Fig. 29C allows much broader range of reflectivity than the prior art pitch variations of Fig. 29B for the multilayer reflectors. In the case that the two polymer layers shown in Fig. 29A are layers of at least one birefringent material where the index of refraction for a first linear polarization is changed from one material to the next, but where the index of refraction for a second linear polarization perpendicular to the first is the same from one material to the next, the structure shown in Fig. 29A will reflect light of the first polarization, and transmit light of the second polarization. The non-linearly varying pitch shown by Fig. 29C ensures broad band operation of the device without interference effects at shorter wavelengths which plague the step function distribution attempt at broadband operation of the prior art.

Broad band IR reflectors made from the multilayer extruded polymer material shown in Fig. 29A may be added to the panels of the invention to add IR reflectivity to the control of visible light. Multilayer linear polarizers may be used in the panels of the

invention instead of CLC materials for controlling the light.

Additional Embodiments Of The Electro-Optical Glazing Structure of  
The Present Invention

Each of illustrative embodiments of electro-optical glazing panel hereof described hereinabove can be combined in various ways in order to provide intelligent glazing structures capable of controlling light transmission therethrough in any number of radiation bands.

For example, transmission in the IR band may be allowed in the winter in the daylight, and at night the IR light may be reflected to save heating energy. In summer, however, IR light may be allowed to escape from the window structure, while visible radiation is reflected to insure privacy.

While the intelligent glazing structures of the invention taught hereinabove allow a very large part of the visible spectrum to be substantially totally reflected, some of these embodiments may, in practice, transmit some radiation, especially at large angles measured with respect to a projection axis normal to the glazing structure, or allow a very small amount of light to leak from a brightly lit room at night, to the dark outside. Consequently, such undesired light transmission in such instances may compromise the level of privacy demanded by particular users in diverse lighting environments. Therefore, there is a great need for a way to further improve the above-described electro-optical glazing structures of the present invention in a simple yet effective manner.

In accordance with another aspect of the present invention, this problem of undesired, partial light transmission can be solved, in instances where it arises, by embodying each electro-optical glazing structure of the present invention with an additional structure that is

capable of controlling (e.g. reflecting or scattering) light incident thereon so as to either block the transmission of such light by reflection, or obscure it by scattering. In principle, such objectives can be achieved using a variety of different types of electro-optical structures well known in the art for different purposes, unrelated to the above-described problem at hand. The improved electro-optical glazing structures can be formed by mounting or incorporating such electrically-controllable structures to any of the above-described electro-optical glazing structures. In principle, such alternative embodiments of the present invention should solve the problems associated with partial light transmission during reflection modes of operation of the panel, thereby ensuring the desired level of privacy demanded by its user in diverse environments. Several different embodiments of the light controlling (reflecting or scattering) structure are described hereinbelow.

In Figs. 17A and 17B, a first illustrative embodiment of the electrically-controllable light scattering structure is shown in the form of an ultra-thin panel comprising a polymer dispersed liquid crystal (PDLC) material 173 contained between a pair of spaced-apart transparent electrically conducting layers 174 and 175 (e.g. ITO). The PDLC material comprises a polymer material with regions 176 of liquid crystal material formed into small spheres of micron or submicron dimension. As illustrated in Fig. 17A, the molecules of the liquid crystal material (depicted as short lines) are correlated by the internal forces in the liquid crystal to have internal order, which may random in a predetermined state of the panel.

In Fig. 17A, PDLC panel 172 is shown operated in its scattering state, wherein light rays 171 incident on a layer 172 are scattered by the liquid crystal molecules ordered therein. During this state, light propagating through the polymer material 173 strikes the sphere of

liquid crystal material 176, and will in general refract at the polymer liquid crystal interface because there will generally be a change in the index of refraction of the (randomly ordered) liquid crystal material and the polymer material. The layer 172 will then scatter light passing through. The light rays traced in Fig. 17A are shown transmitted through the layer 172, which would be the case for very light loading of liquid crystal material in the polymer. In the more general case, light incident on the panel would be as likely scattered backward as forward, and would likely be scattered isotropically in all directions.

In Fig. 17B, the PDLC panel 172 is shown operated in its transmission state, wherein an electric field is applied across the layer 172 by applying voltage across the conducting layers 174 and 175. In this state of operation, the electric field forces the liquid crystal molecules in each sphere to line up parallel with the field, causing the index of refraction of the liquid crystal material to match the index of the polymer material, thereby enabling the light rays pass through the layer 172 without deviation or scattering.

In Figs. 18A and 18C, a second illustrative embodiment of the electrically-controllable light scattering structure 182 is shown in the form of a thin panel comprising a liquid crystal polymer material 183 contained between a pair of spaced-apart transparent electrically conducting layers 174 and 175 (e.g. ITO) having surfaces that have been either rubbed or coated with a molecular aligning layer such as polyamide, well known in the CLC art. In this embodiment, the liquid crystal material 183 is admixed with a polymer material, but unlike the embodiment shown in Figs. 17A and 17B, the resultant material does not phase segregate. Instead, the linear liquid crystal molecules remain entangled in the polymer material.

In Fig 18A, the electro-optical light scattering structure 182 is

shown operated in its reflection mode, wherein the crystal molecules (depicted as short lines) are lined up parallel with the conducting plates 174 and 175 because, for example, the surfaces of the plates have been rubbed, causing the molecules to become internally ordered (e.g. aligned) such that incident light on the layer 183 is reflected as shown. This molecular ordering can be thought of as a "relaxed ordering" when no external electrical force field is applied thereto.

In Fig. 18B, the electro-optical light scattering structure 182 is shown operated in its reflection mode, wherein an electric field is impressed across the layer 183 by applying a voltage across layers 174 and 175. In this state of operation, the molecules rotate to line up parallel to the field and light, propagating parallel to the field, is transmitted through the layer 183 without scattering, reflection, or absorption. When the electric field is removed by disruption the applied voltage source, the polymer acts as restoring force to rotate the molecules back to their starting relaxed ordering as shown in Fig. 18A.

In Fig. 18C, a third illustrative embodiment of the electrically-controllable light scattering structure 182 is shown comprising liquid crystal polymer material 183 contained between a pair of spaced-apart transparent electrically conducting layers 174 and 175 (e.g. ITO) having surfaces that have not been rubbed or coated with a molecular aligning layer such as polyamide, as in the embodiment of Figs. 18A and 18B. Thus there is no internal order imposed on the liquid crystal material by rubbed bounding surfaces or layers, as in the structure of Figs. 18A and 18B. In Fig. 18C, the electro-optical light scattering structure 182 is shown operated in its scattering mode, wherein there is no internal ordering created by rubbed surfaces or polyamide layers, or an electric field created by an

externally applied voltage. In this mode of operation, the liquid crystal material naturally tends towards lowering its internal energy by having near neighbor molecules align with one another, but there is no long range order. Thus the regions of material now scatter light randomly and, without the application an electric field, the light incident on the layer 184 is scattered. When an electric field is impressed across the panel of Fig. 18C, the molecules therebetween swing around to line up with the applied electric field, enabling incident light to be transmitted through the panel 182 without scattering in a manner similar to that shown in Fig. 18B. This is the transmission mode of operation of the electrically-controllable light scattering device.

In Fig. 19, fourth illustrative embodiment for an electro-optical light scattering structure (i.e. panel) is shown comprising an isotropic scattering material, such as a liquid crystal polymer, contained between a pair of transparent glass panels. Each of these plates has an ITO coating upon the glass plate surface, electrical terminals connected thereto, and a polyamide layer applied upon the ITO layer. Alternatively, the ITO surfaces can be rubbed for initiating molecular alignment in lieu of the ITO layers.

In Fig. 19A, the electro-optical light scattering structure of Fig. 19 is shown operated in its transmission mode, wherein no external voltage is applied (i.e.  $V=V_{\text{off}}$ ). In Figs. 19B and 19C, transmission and reflection characteristics for this mode of operation are shown, respectively. In Fig. 19D, the electro-optical light scattering structure of Fig. 19 is shown operated in its light scattering mode, wherein an external voltage  $V$  is applied across the ITO surfaces (i.e.  $V=V_{\text{on}}$ ). In Figs. 19E and 19F, transmission and reflection characteristics for this mode of operation are shown, respectively. As light is transmitted



when no external voltage is applied, and scatters when a voltage is applied, this structure is said to operate in the "reverse mode".

In Fig. 20, a fifth illustrative embodiment for an electrically-controllable light scattering structure is shown comprising an isotropic scattering material, such as a liquid crystal polymer (made using a different polymer mixing ratio than used in Fig. 19), contained between a pair of transparent glass panels. Each of the plates has an ITO coating upon the glass plate surface and an electrical terminal connected thereto, but is not rubbed or coated with a polyamide or like layer to ensure that there is no high order molecular alignment when no external field is applied.

In Fig. 20A, the electro-optical light scattering structure of Fig. 20 is shown operated in its scattering mode, wherein no external voltage is applied (i.e.  $V=V_{\text{off}}$ ). In Figs. 20B and 20C, transmission and reflection characteristics for this mode of operation are shown, respectively. In Fig. 20D, the electro-optical light scattering structure of Fig. 20 is shown operated in its light transmission mode, wherein an external voltage  $V$  is applied across the ITO surfaces (i.e.  $V=V_{\text{on}}$ ). In Figs. 20E and 20F, transmission and reflection characteristics for this mode of operation are shown, respectively. As light is transmitted when an external voltage is applied, and scatters when a voltage is no applied, this structure is said to operate in the "normal mode".

Such alternative embodiments of the present invention will be particularly useful when a room is brightly lit at night, and a very small amount of light leaking from the inside to the dark outside may compromise privacy.

Having described such alternative embodiments of the present invention, further modifications thereto readily come to mind.

For example, the electro-optical glazing structures described above can be stacked and laminated together, in virtually any number or ordering, so as form composite electro-optical glazing structures having more than two optical states (e.g. four or more).  
5 Such electro-optical glazing structures can be used to construct sophisticated window systems capable of providing complex levels of solar and/or visible radiation control.

Electrically controlled CLC-based smart windows of the present invention can be used in homes, schools, offices, factories, as well as  
10 in automobiles and airplanes to provide privacy, brightness control, and reduce thermal loading on heating and cooling systems employed therein.

The electro-optical glazings of the present invention can be used to make intelligent sunglasses and sun visors for use in a  
15 variety of applications. In such embodiments of the present invention, the electro-optical glazing of the present invention is realized in the form of a pair of lenses which are mounted within a frame supportable upon the head of its user, as in conventional eyeglasses or sun-visors. The programmed microcontroller, battery,  
20 electromagnetic detector, battery recharging circuitry and optical state switching circuitry embodied within the window frame shown in Figs. 1A and 12B can be reduced in size and embodied within the ultra-compact sunglasses frame of this illustrative embodiment of the present invention.

25 In yet another alternative embodiment of the present invention, the electro-optical glazing structures of the present invention can be mounted before each LCD viewing panel within the shutter-type stereoscopic 3-D viewing glasses taught in International Publication No. WO 97/43681 by VRex, Inc., a wholly owned  
30 subsidiary of Reveo, Inc., which is incorporated herein by reference in

its entirety. Advantageously, the application of the present invention thereto would provide stereoscopic 3-D viewing glasses having several additional modes of operation, wherein the user could simply control electromagnetic radiation in either a manual or automatic manner during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or stereoscopic viewing of real world objects while walking, bicycling, jogging, sailing, or just lounging about in the rays of the Sun.

The electro-optical glazings of the present invention can be used in automotive vehicles, maritime vessels, aircrafts and spacecrafts.

The modifications described above are merely exemplary. It is understood that other modifications to the illustrative embodiments will readily occur to persons with ordinary skill in the art. All such modifications and variations are deemed to be within the scope and spirit of the present invention as defined by the accompanying Claims to Invention.

CLAIMS TO INVENTION

1. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, said electro-optical glazing structure comprising:

an electro-optical glazing panel of laminated construction, having first and second optical states of operation; and

optical state switching means for switching said electro-optical glazing panel to said first optical state of operation in order to induce said electro-optical glazing structure into said reflection mode of operation, and for switching said electro-optical glazing panel to said second optical state of operation in order to induce said electro-optical glazing structure into said transmission mode of operation.

2. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

a second electrically-passive CLC electromagnetic radiation polarizing panel;

and

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

3. The electro-optical glazing structure of claim 2, wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels reflect electromagnetic radiation having a first circularly

polarized state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having a second circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels reflect or transmit without absorption electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

4. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;  
a second electrically-active CLC electromagnetic radiation polarizing panel; and

an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

5. The electro-optical glazing structure of claim 4, wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels reflect electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation, wherein said first and second electrically-active CLC electromagnetic radiation polarizing

panels transmit electromagnetic radiation having either a right hand a second circularly polarized state and/or a wavelength outside said first prespecified bandwidth when said electro-optical glazing panel is switched to said first optical state of operation; and

5 wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

10

6. The electro-optical glazing structure of claim 1, wherein said electro-optical glazing panel comprises:

first and a second electrically passive single layer electromagnetic radiation polarizing panels; and

15

an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive electromagnetic radiation polarizing panels.

7. The electro-optical glazing structure of claim 1, wherein said  
20 electro-optical glazing panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC

25

electromagnetic radiation polarizing panel.

8. The electro-optical glazing structure of claim 7,

wherein said first electrically-active CLC electromagnetic radiation

polarizing panel reflects electromagnetic radiation having a first circularly polarized state when said electro-optical glazing panel is switched to said first optical state of operation, and

wherein said first electrically-active CLC electromagnetic radiation polarizing panel transmits electromagnetic radiation having a second circularly polarized [(RHCP)] state when said electro-optical glazing panel is switched to said first optical state of operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel reflects electromagnetic radiation having said second state when said electro-optical glazing panel is switched to said first optical state of operation,

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits electromagnetic radiation having said first state when said electro-optical glazing panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit more than 50% of electromagnetic radiation having either said first state or said second state when said electro-optical glazing panel is switched to said second optical state of operation.

9. The electro-optical glazing structure of claim 1, which further comprises:

a window frame for mounting said electro-optical glazing panel within a house or office building, or aboard a transportation vehicle.

10. The electro-optical glazing structure of claim 9, which further comprises:

a electromagnetic-sensor mounted on said window frame, for sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said window frame, for recharging the battery;

5           electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

10           a programmable micro-computer chip mounted within said window frame, for controlling the operation of said battery recharger and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

11. The electro-optical glazing structure of claim 1, further comprising:  
15   a frame for an intelligent pair of sunglasses; and  
          a pair of said optical glazing elements supported within said frame,

          wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

20

12. An intelligent window system for dynamic electromagnetic radiation control which comprises:

25           a plurality of said electro-optical glazing structures of claim 10, each mounted within a house or office building, or aboard a transportation vehicle; and

          a central control computer for coordinating the operation of said electro-optical glazing structures.

13. A composite electro-optical glazing structure which comprises:  
30           a plurality of said electro-optical glazing structures of claim 1,



stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than two said optical states of operation which permit complex levels of electromagnetic radiation control.

5

14. A stereoscopic 3-D viewing device in the form of eyeglasses, comprising:

a pair of optical elements positionable before the eyes of a user of said eyeglasses, each said optical element including said electro-optical  
10 glazing structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of real world objects.

15

15. An electro-optical glazing structure which has high reflection, semi-transparent and greater than 50% transparent modes of operation for improved control over the flow of electromagnetic radiation within the solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

20

16. A reflective electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

25

17. The electro-optical glazing structure of claim 1, wherein the transmission of the visible portion of the electromagnetic spectrum is controlled and wherein the IR portion of the electromagnetic spectrum is reflected.

30 18. An electro-optical glazing structure, comprising an

electrically-active phase retardation panel interposed between a pair of single layer electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first linear polarization state, whereby a highly reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

19. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a first and a second electrically-passive electromagnetic radiation polarizing panel, the first panel reflecting electromagnetic radiation of a first linear polarization state, the second panel reflecting electromagnetic radiation of a second linear polarization state, whereby a reflective state of operation and a semi-transparent state of operation are provided over a region of the electromagnetic spectrum.

20. The electro-optical glazing structure of claim 19, wherein the first and a second electrically-passive electromagnetic radiation polarizing panels are single layer polarizing panels.

21. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a first circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

22. An electro-optical glazing structure, comprising a pair of

electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of a first circularly polarized state and the other of which is capable of reflecting electromagnetic radiation of a second circularly polarized state, whereby a highly reflective state of operation and a highly transparent state of operation are provided over a region of the electromagnetic spectrum.

23. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the transmission and reflection of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, from greater than 50% transmission to high reflection.

24. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of claim 1, wherein the electromagnetic radiation over the IR region of the electromagnetic spectrum can be reflected, rather than absorbed, reducing the temperature cycle range which the window structure is required to undergo.

25. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure of claim 1 is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the

electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within  
5 the programmed microcontroller.

26. The electro-optical glazing structure of claim 1 which is designed for integration within the heating/cooling system of a house, office building, factory or vehicle in order to control the flow of broad-band  
10 electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

27. An intelligent pair of shutter glasses, in which each optical element  
15 is realized using an electro-optical glazing structure of claim 1 fashioned to the dimensions of a shutter glass frame.

28. The electro-optic glazing structure of claim 1, further comprising:  
a reflecting layer for reflecting infrared light, wherein the  
20 electro-optic glazing structure of claim 1 controls the transmission and reflection of visible light.

29. The electro-optic glazing structure of claim 1, further comprising:  
a reflecting layer for reflecting UV light, wherein the electro-optic  
25 glazing structure of claim 1 controls the transmission and reflection of visible light.

30. The electro-optic glazing structure of claim 1, further comprising:  
30 a electro-optic glazing structure which controls the transmission and

reflection of IR light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of visible light.

31. The electro-optic glazing structure of claim 1, further comprising:

5 a electro-optic glazing structure which controls the transmission and reflection of visible light, wherein the electro-optic glazing structure of claim 1 separately controls the transmission and reflection of IR light.

32. An electro-optical glazing structure having reflection and  
10 transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, the electro-optical glazing structure comprising:

an electro-optical panel of multilayer construction, having first and second optical states of operation;

15 optical state switching means for switching the electro-optical panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the  
20 transmission mode of operation, and

means for further controlling electromagnetic radiation incident on the electro-optical panel.

33. The electro-optical glazing structure of claim 32, wherein the means  
25 for further controlling the electromagnetic radiation comprises a means for reflecting circularly polarized light.

34. The electro-optical glazing structure of claim 33, wherein the means  
30 for reflecting circularly polarized light comprise a cholesteric liquid crystal (CLC) reflector.

35. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a scattering layer for controllably scattering light.

5

36. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

10

37. The electro-optical glazing structure of claim 36x, wherein the anisotropically shaped objects are micron size sheets of reflecting material.

15 38. The electro-optical glazing structure of claim 37, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

20 39. The electro-optical glazing structure of claim 37, wherein the micron size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

25 40. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a polymerized polymer region containing a large plurality of inclusions of liquid crystal material.

41. The electro-optical glazing structure of claim 40, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

30

42. The electro-optical glazing structure of claim 35, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

5 43. The electro-optical glazing structure of claim 42, wherein the scattering layer may be made non scattering under the influence of an electric field.

10 44. The electro-optical glazing structure of claim 32, wherein the means for further controlling the electromagnetic radiation comprises a mixture of a polymer and a liquid crystal material.

15 45. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material is transparent to the electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

20 46. The electro-optical glazing structure of claim 44, wherein the mixture of polymer and liquid crystal material reflects a portion of the electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

25 47. An electro-optical glazing structure having reflection and transmission modes of operation for selectively reflecting and transmitting electromagnetic radiation, respectively, the electromagnetic radiation having a first and a second linear polarization, the electro-optical glazing structure comprising:

an electro-optical panel having first and second optical states of operation; and

30 optical state switching means for switching the electro-optical

panel to the first optical state of operation in order to induce the electro-optical glazing structure into the reflection mode of operation, and for switching the electro-optical panel to the second optical state of operation in order to induce the electro-optical glazing structure into the transmission mode of operation,

wherein the electro-optical panel comprises:

a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference between the materials in each layer of the pair, the difference being in the index of refraction for electromagnetic radiation having the first linear polarization, wherein there is little difference in the index of refraction for electromagnetic radiation having the second linear polarization, the total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

48. The electro-optical glazing structure of claim 47, wherein the electro-optical panel further reflects circularly polarized electromagnetic radiation.

49. The electro-optical glazing structure of claim 48, wherein the electro-optical panel comprises a cholesteric liquid crystal (CLC) material.

50. The electro-optical glazing structure of claim 47, wherein the electro-optical panel selectively transmits and reflects electromagnetic radiation of a first bandwidth of the EM spectrum, further comprising a reflector of EM radiation which reflects radiation in a second bandwidth of the EM spectrum, the reflector of EM radiation comprising a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction



between the materials in each layer of the pair.

51. The electro-optical glazing structure of claim 50, wherein the reflector of EM radiation comprises a sheet having a large plurality of pairs of layers parallel to a surface of the sheet, each pair of layers having a difference in the index of refraction between the materials in each layer of the pair. The total thickness of each pair of layers in the large plurality of layers varying non linearly across the sheet.

52. The electro-optical glazing structure of claim 47, further comprising a controllable scattering layer.

53. The electro-optical glazing structure of claim 52, wherein the controllable scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

54. The electro-optical glazing structure of claim 47, wherein electrooptic panel further comprises a means for reflecting circularly polarized light.

55. The electro-optical glazing structure of claim 54, wherein the means for reflecting circularly polarized light comprise a cholesteric liquid crystal (CLC) reflector.

56. The electro-optical glazing structure of claim 47, wherein the electro-optic panel further comprises a scattering layer for controllably scattering light.

57. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a fluid medium containing a large plurality of anisotropically shaped objects for controllably scattering light, the orientation of anisotropically shaped objects controllable by a field.

5

58. The electro-optical glazing structure of claim 57, wherein the anisotropically shaped objects are micron size sheets of reflecting material.

10 59. The electro-optical glazing structure of claim 58, wherein the micron size sheets of reflecting material are multilayer polymer reflectors.

15 60. The electro-optical glazing structure of claim 58, wherein the micron size sheets of reflecting material are cholesteric liquid crystal (CLC) reflectors.

20 61. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a polymerized polymer region containing a large plurality of inclusions of liquid crystal material.

62. The electro-optical glazing structure of claim 61, wherein the scattering layer comprises a polymer dispersed liquid crystal (PDLC) layer.

25

63. The electro-optical glazing structure of claim 56, wherein the scattering layer comprises a mixture of a polymer and a liquid crystal material.

30 64. The electro-optical glazing structure of claim 63, wherein the

scattering layer may be made non scattering under the influence of an electric field.

65. The electro-optical glazing structure of claim 47, wherein the  
5 electro-optical panel further comprises a layer of a mixture of a polymer and a liquid crystal material.

66. The electro-optical glazing structure of claim 65, wherein the  
10 mixture of polymer and liquid crystal material is transparent to the electromagnetic radiation incident on the electro-optical panel when an electric field is induced in the mixture.

67. The electro-optical glazing structure of claim 65, wherein the  
15 mixture of polymer and liquid crystal material reflects a portion of the electromagnetic radiation incident on the electro-optical panel when no electric field is induced in the mixture.

68. An electro-optical glazing structure having total-reflection and  
20 transparent modes of operation for selectively reflecting and transmitting electromagnetic radiation without absorption, respectively, said electro-optical glazing comprising:

an electro-optical panel of laminated construction, having first and second optical states of operation; and

optical state switching means for switching said electro-optical  
25 panel to said first optical state of operation in order to induce said electro-optical glazing into said total-reflection mode of operation, and for switching said electro-optical panel to said second optical state of operation in order to induce said electro-optical glazing into said transmission mode of operation,

30 wherein electromagnetic radiation within a first prespecified

bandwidth falling incident upon said electro-optical panel is totally reflected from said electro-optical panel without absorption when said electro-optical panel is switched to said first optical state of operation, and

5            wherein electromagnetic radiation within a second prespecified bandwidth falling incident upon said electro-optical panel is transmitted through said electro-optical panel without absorption when said electro-optical panel is switched to said second optical state of operation.

10    69. The electro-optical glazing structure of claim 68, wherein said first prespecified bandwidth comprises the infrared (IR) portion and ultra-violet (UV) portions of the electromagnetic spectrum, and said second prespecified bandwidth comprises said IR portion, said UV portion and the visible portion of the electromagnetic spectrum.

15    70. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

          a first electrically-passive cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

20            a second electrically-passive CLC electromagnetic radiation polarizing panel; and    an electrically-active  $\pi$ -phase retardation panel interposed between said first and second electrically-passive CLC electromagnetic radiation polarizing panels.

25    71. The electro-optical glazing structure of claim 70,

          wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified

bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-passive CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

15

72. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel;

20

a second electrically-active CLC electromagnetic radiation polarizing panel; and an electrically-passive  $\pi$ -phase retardation panel interposed between said first and second electrically-active CLC electromagnetic radiation polarizing panels.

25

73. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified

bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

74. The electro-optical glazing structure of claim 72,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels totally reflect without absorption electromagnetic radiation having a right hand circularly polarized (RHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation,

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either a left hand circularly polarized (LHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption

electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth when said electro-optical panel is switched to said second optical state of operation.

5

75. The electro-optical glazing structure of claim 68, wherein said electro-optical panel comprises:

a first electrically-active cholesteric liquid crystal (CLC) electromagnetic radiation polarizing panel; and

10

a second electrically-active CLC electromagnetic radiation polarizing panel adjacent said first electrically-active CLC electromagnetic radiation polarizing panel.

76. The electro-optical glazing structure of claim 75,

15

wherein said first electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having a left hand circularly polarized (LHCP) state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation, and

20

wherein said first electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either a right hand circularly polarized (RHCP) state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of

25

operation;

wherein said second electrically-active CLC electromagnetic radiation polarizing panel totally reflects without absorption electromagnetic radiation having said RHCP state and a wavelength within said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation, and

30

wherein said second electrically-active CLC electromagnetic radiation polarizing panels transmits without absorption electromagnetic radiation having either said LHCP state and/or a wavelength outside said first prespecified bandwidth when said electro-optical panel is switched to said first optical state of operation; and

5 wherein said first and second electrically-active CLC electromagnetic radiation polarizing panels transmit without absorption electromagnetic radiation having either said LHCP state or said RHCP state and a wavelength within said second prespecified bandwidth  
10 when said electro-optical panel is switched to said second optical state of operation.

76. The electro-optical glazing structure of claim 68, which further comprises:

15 a window frame for mounting said electro-optical panel within a house or office building, or aboard a transportation vehicle;

77. The electro-optical glazing structure of claim 76, which further comprises:

20 a electromagnetic-sensor mounted on said window frame, for sensing electromagnetic conditions;

a battery supply mounted within said window frame, for providing electrical power;

a electromagnetic-powered battery recharger mounted within said  
25 window frame, for recharging the battery;

electrical circuitry mounted within said window frame, for producing glazing control voltages for switching said first and second optical states of operation; and

a programmable micro-computer chip mounted within said  
30 window frame, for controlling the operation of said battery recharger



and said electrical circuitry, and the production of said glazing control voltages as required by a radiation flow control program stored within said programmable microcontroller.

5 78. An intelligent pair of sunglasses, comprising:

a frame; and

a pair of optical element supported within said frame,

wherein each said optical element is realized using said electro-optical glazing structure of claim 1.

10

79. An intelligent window system for dynamic electromagnetic radiation control which comprises:

a plurality of said electro-optical glazing structures of claim 11, each mounted within a house or office building, or aboard a

15 transportation vehicle; and

a central control computer for coordinating the operation of said electro-optical glazing structures.

80. An composite electro-optical glazing structure which comprises:

20 a plurality of said electro-optical glazing structures of claim 1, stacked together as a composite electro-optical structure,

wherein said composite electro-optical structure has more than two said optical states of operation which permit complex levels of electromagnetic radiation control.

25

81. A stereoscopic 3-D viewing device in the form of eyeglasses, comprising:

a pair of optical elements positionable before the eyes of a user of said eyeglasses,

30 each said optical element including said electro-optical glazing

structure of claim 1,

whereby said eyeglasses can control electromagnetic radiation during stereoscopic 3-D viewing or monoscopic 2-D viewing of displayed images (i.e. virtual world viewing), or during stereoscopic viewing of  
5 real world objects.

82. An electro-optical glazing structure which has total-reflection, semi-transparent and totally transparent modes of operation for improved control over the flow of electromagnetic radiation within the  
10 solar region of the electromagnetic spectrum (i.e. Solar Spectrum).

83. An electro-optical glazing structure, in which the modes of operation can be electrically-activated or switched, while avoiding the use of energy absorbing mechanisms.

15

84. An electro-optical glazing structure having a broad band of operation, including the IR, visible and UV portions of the electromagnetic spectrum.

20 85. An electrically-active -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a certain polarization state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the  
25 electromagnetic region of the electromagnetic spectrum.

86. An electro-optical glazing structure, comprising an electrically-active -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are  
30 capable of reflecting electromagnetic radiation of a linear polarization

state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

5 87. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is parallel to other, whereby a totally reflective state of  
10 operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

88. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of  
15 electrically-passive electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a linear polarization state, one is perpendicular to other, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic  
20 spectrum.

89. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive cholesteric liquid crystal (CLC) electromagnetic  
25 radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a LHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over the electromagnetic region of the electromagnetic spectrum.

90. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of a RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

91. An electro-optical glazing structure, comprising an electrically-active  $\pi$ -phase retardation panel interposed between a pair of electrically-passive CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

92. An electro-optical glazing structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are capable of reflecting electromagnetic radiation of the LHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

93. An electro-optical structure, comprising an electrically-passive  $\pi$ -phase retardation panel interposed between a pair of electrically-active CLC electromagnetic radiation polarizing panels, both of which are

capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a semi-transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

5

94. An electro-optical glazing structure, comprising a pair of electrically-active CLC electromagnetic radiation polarizing panels, one of which is capable of reflecting electromagnetic radiation of the LHCP state and the other of which is capable of reflecting electromagnetic radiation of the RHCP state, whereby a totally reflective state of operation and a totally transparent state of operation are provided over a broad-band region of the electromagnetic spectrum.

95. An actively-controlled window or viewing panel constructed from the electro-optical glazing structure of the present invention, wherein the transmission of electromagnetic radiation can be dynamically controlled over a broad-band region of the electromagnetic spectrum, between 50% transmission to 100% reflection and between 100% transmission to 100% reflection.

20

96. An actively-controlled window or viewing panel constructed from an electro-optical glazing structure, wherein the transmission of electromagnetic radiation over the UV and IR regions of the electromagnetic spectrum can be totally reflected, rather than absorbed, reducing the temperature cycle range which the window structure is required to undergo.

25

97. An actively-controlled window or viewing panel constructed from an electro-optical glazing structures, wherein only UV and IR radiation is reflected at the window surface, while electromagnetic radiation over

30

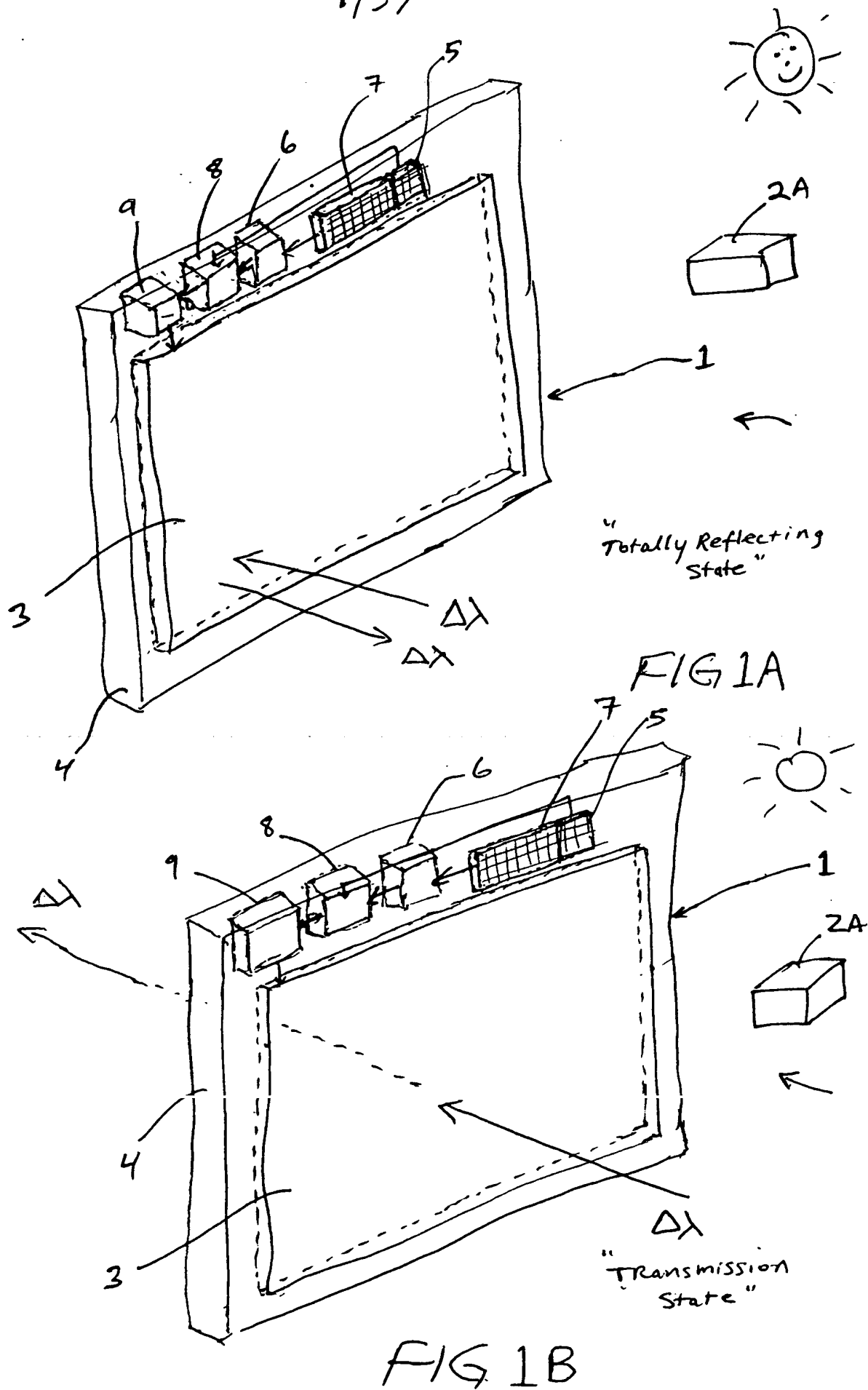
the visible band is transmitted to the interior environment being maintained under thermal control.

98. An intelligent window system for installation within a house or office building, or aboard a transportation vehicle such as an airplane or automobile, wherein an electro-optical glazing structure thereof is supported within a prefabricated window frame, within which are mounted: a electromagnetic-sensor for sensing electromagnetic conditions in the outside environment; a battery supply for providing electrical power; a electromagnetic-powered battery recharger for recharging the battery; electrical circuitry for producing glazing control voltages for driving the electrically-active elements of the electro-optical glazing supported within the window frame; and a micro-computer chip for controlling the operation of the battery recharger and electrical circuitry and the production of glazing control voltages as required by a radiation flow control program stored within the programmed microcontroller.

99. An electro-optical window structure which is designed for integration within the heating/cooling system of a house, office building, factory or vehicle in order to control the flow of broad-band electromagnetic radiation through the electro-optical window structure, while minimizing thermal loading upon the heating/cooling system thereof.

100. An intelligent pair of shutter glasses, in which each optical element is realized using an electro-optical glazing structure fashioned to the dimensions of a shutter glass frame.

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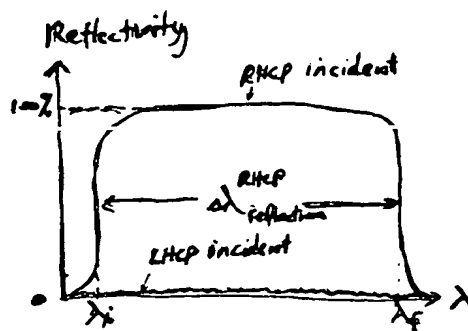
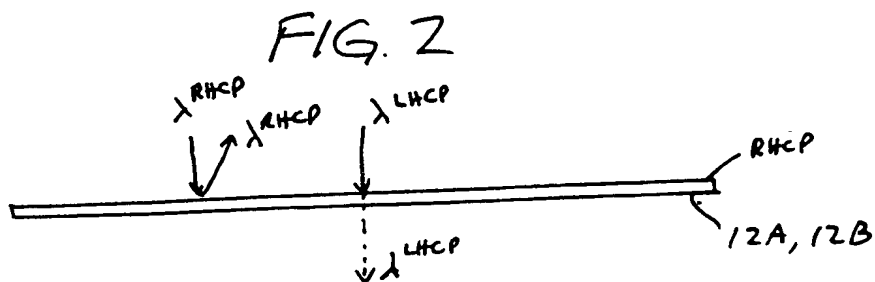
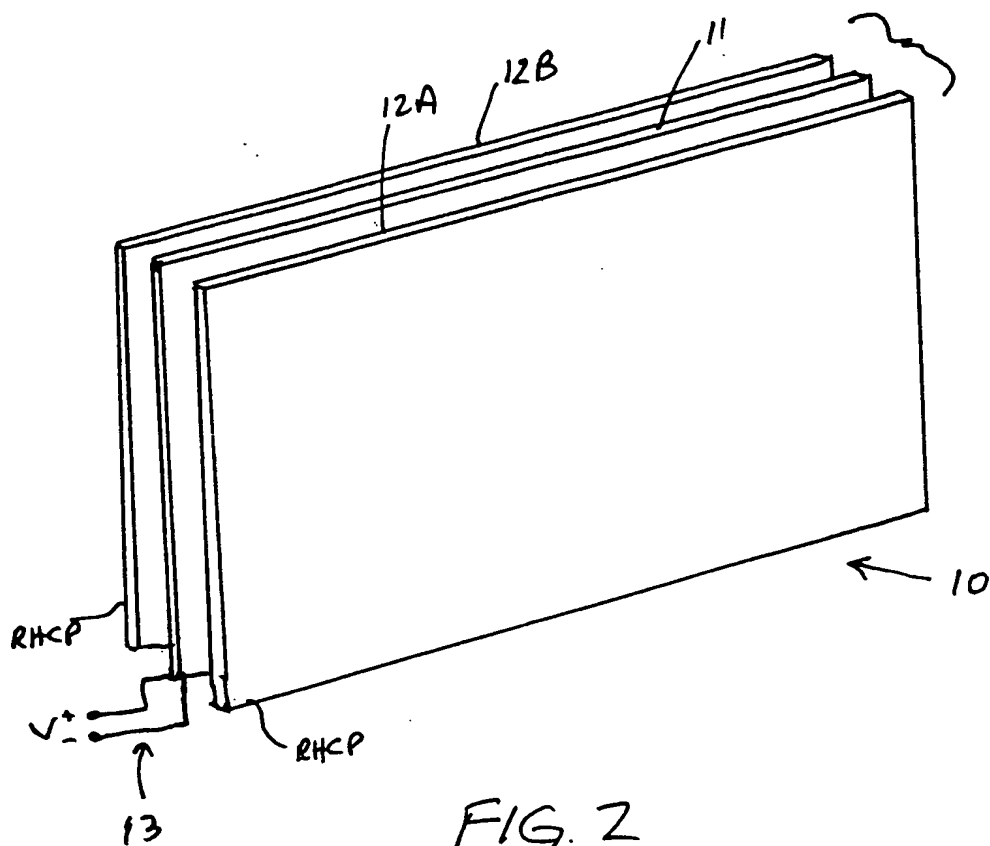


FIG. 2B



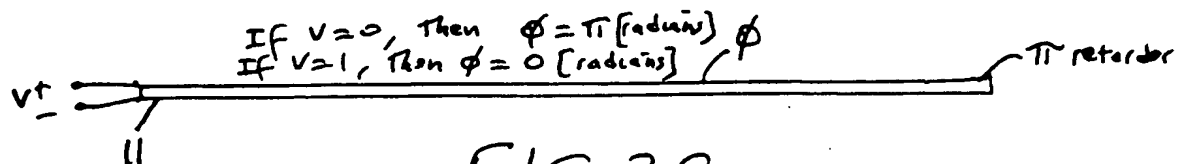


FIG. 2C

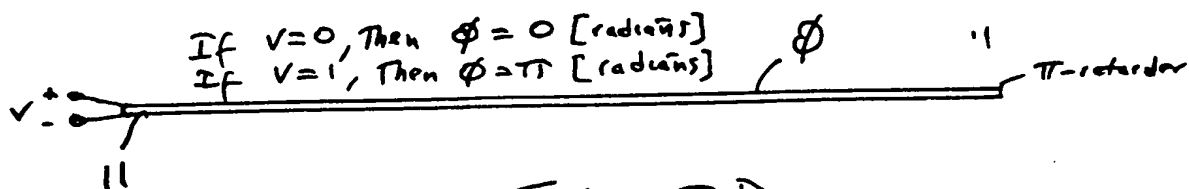


FIG. 2D

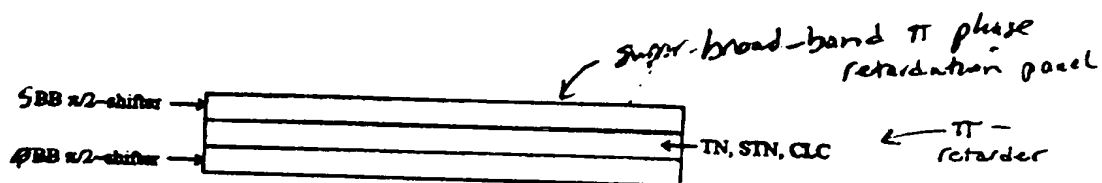


FIG. 2E1

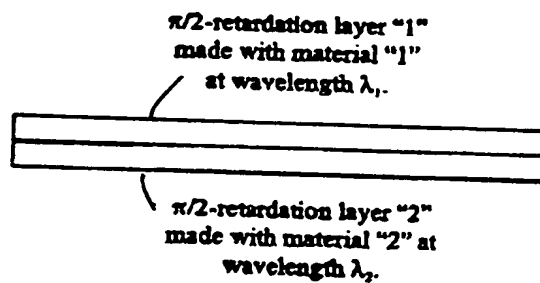


FIG. 2E2

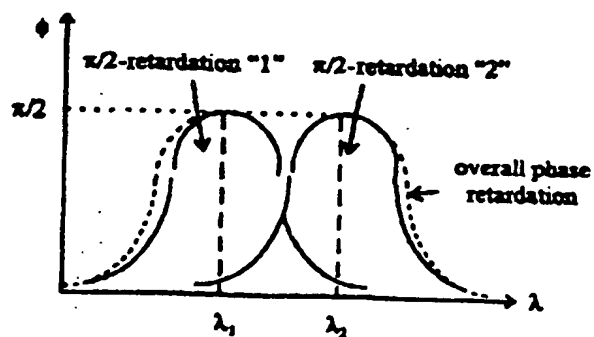


FIG. 2E3

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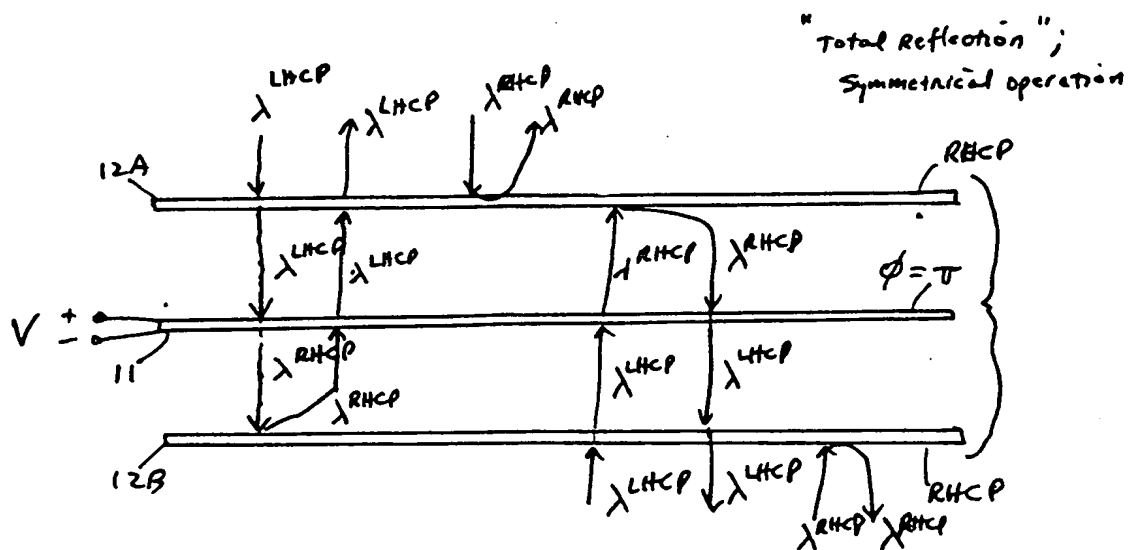


FIG. 3A

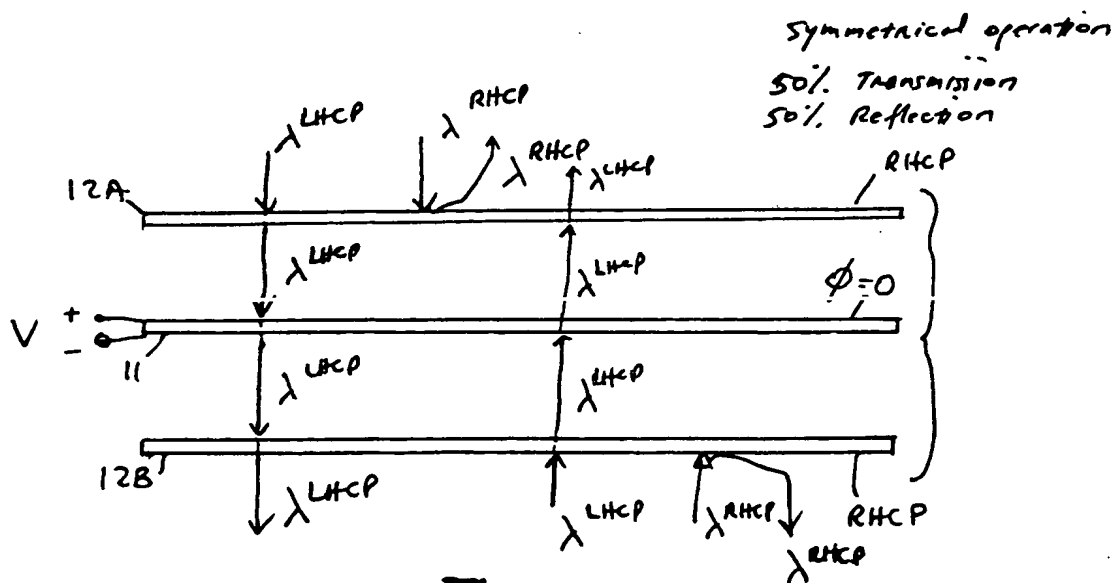


FIG. 3B

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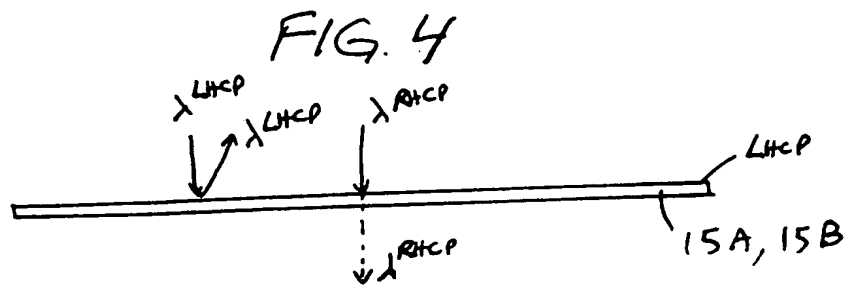
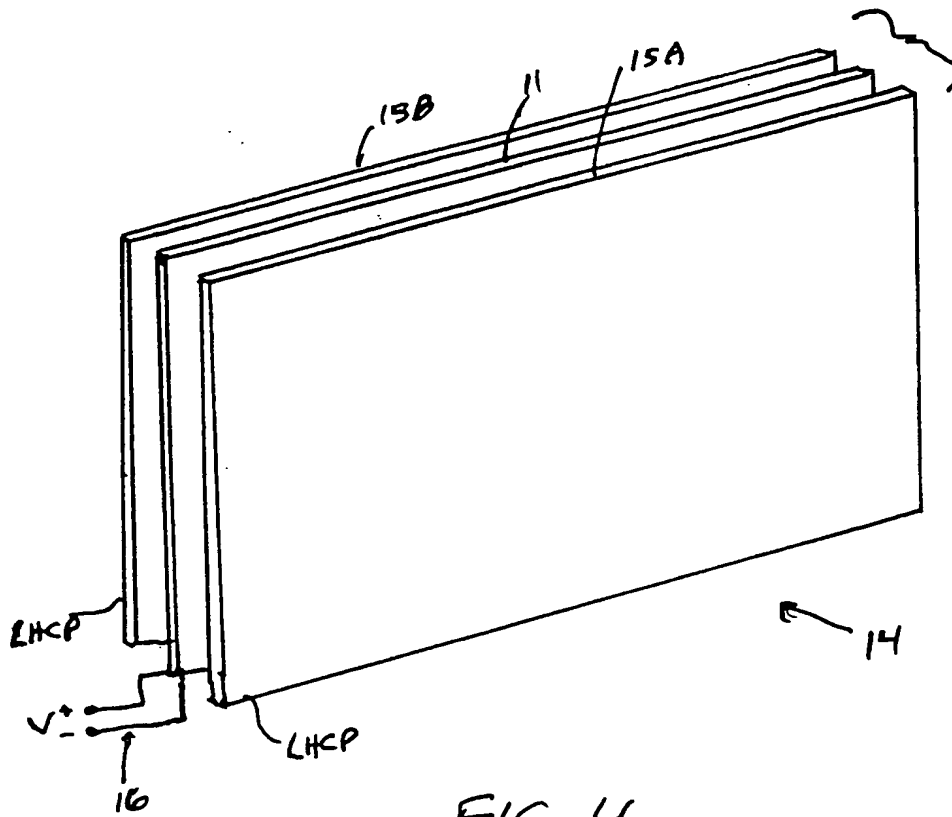


FIG. 4A

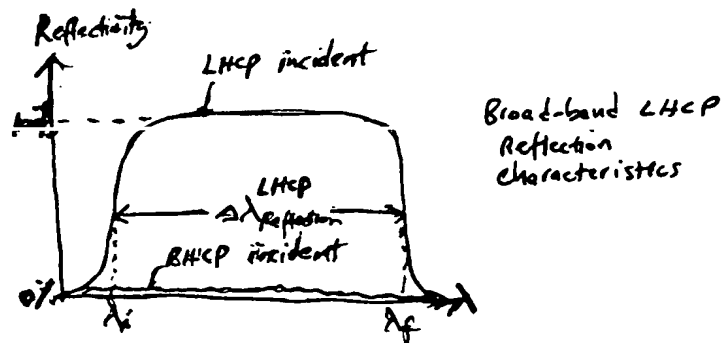
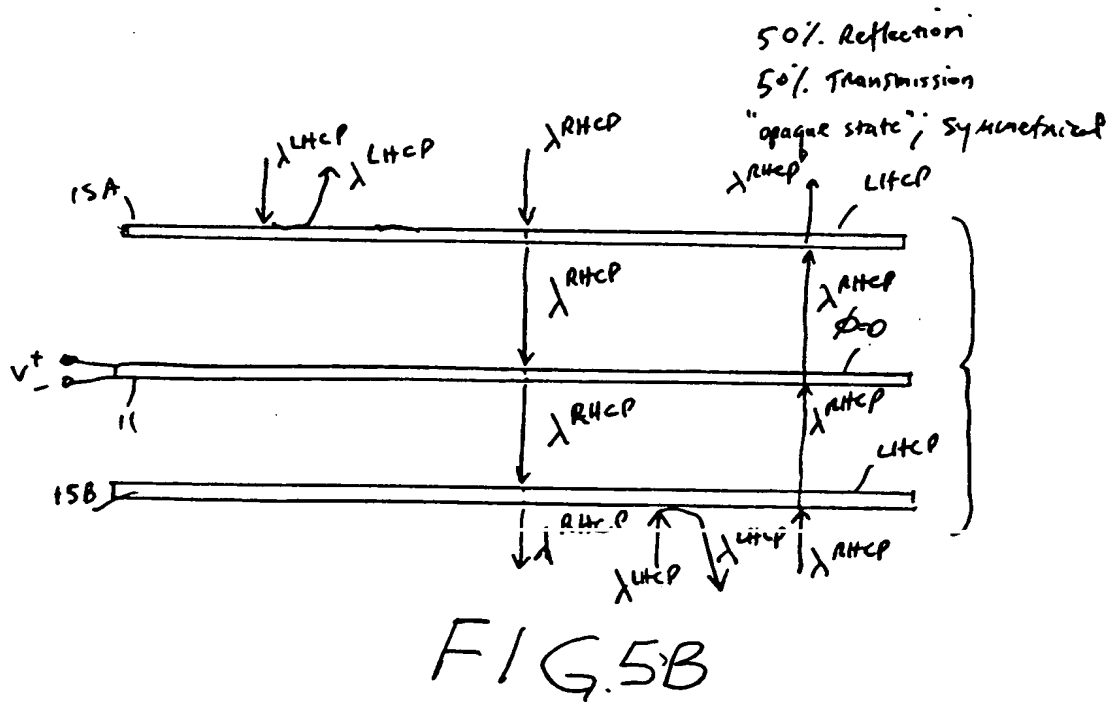
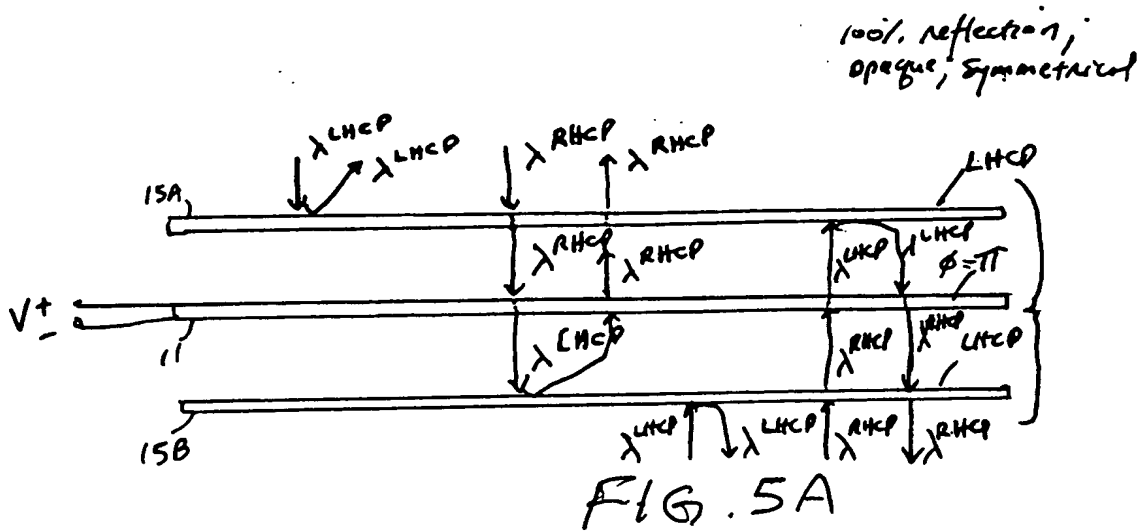
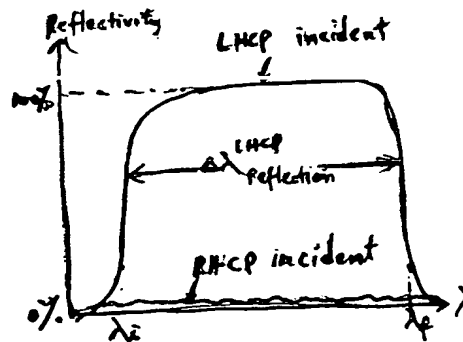
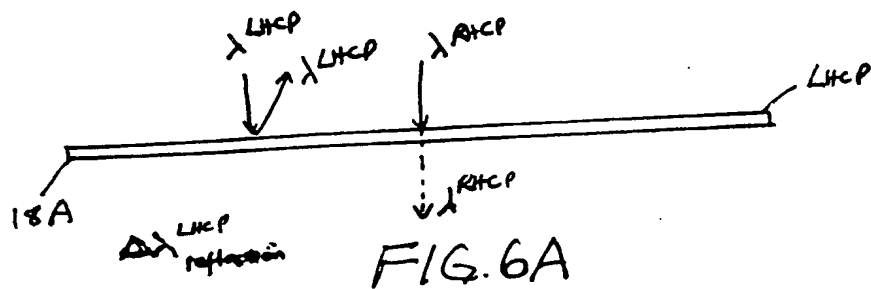
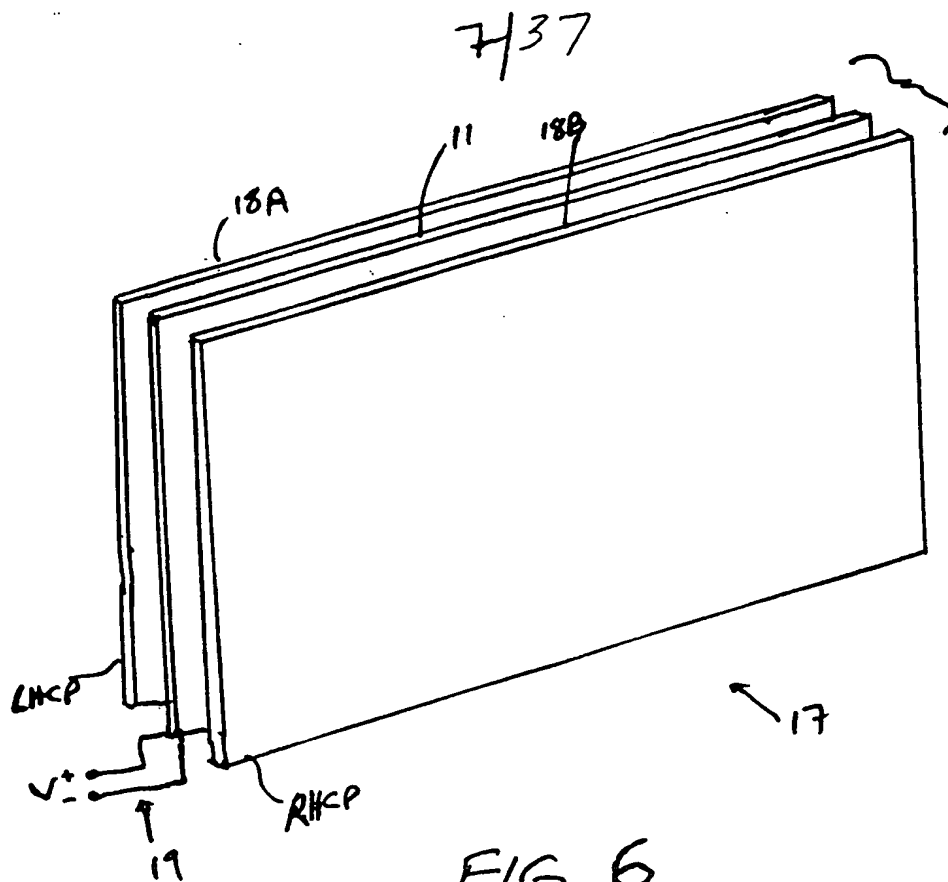


FIG. 4B

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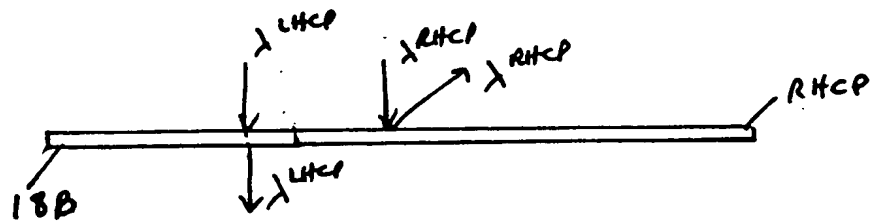


FIG. 6C

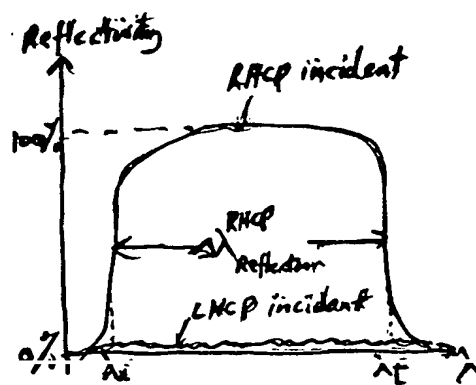


FIG. 6D

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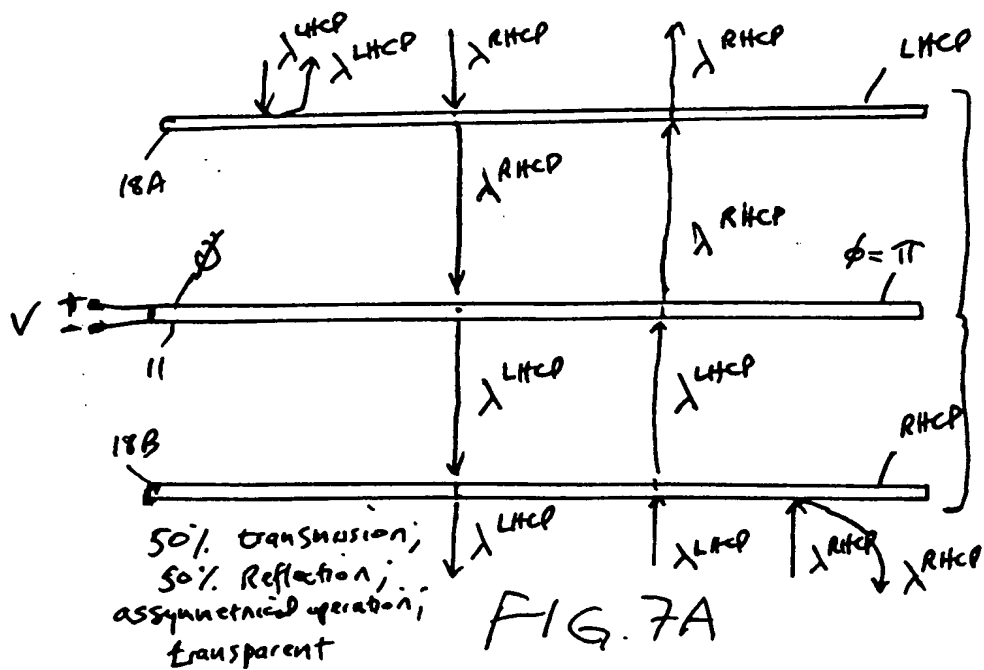


FIG. 7A

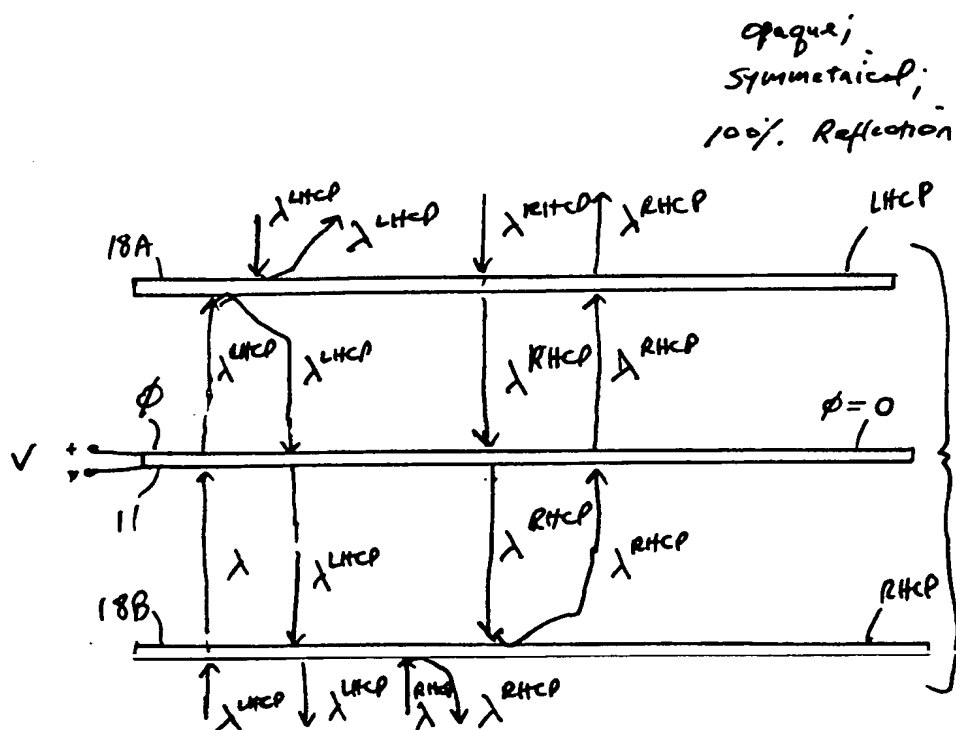


FIG. 7B

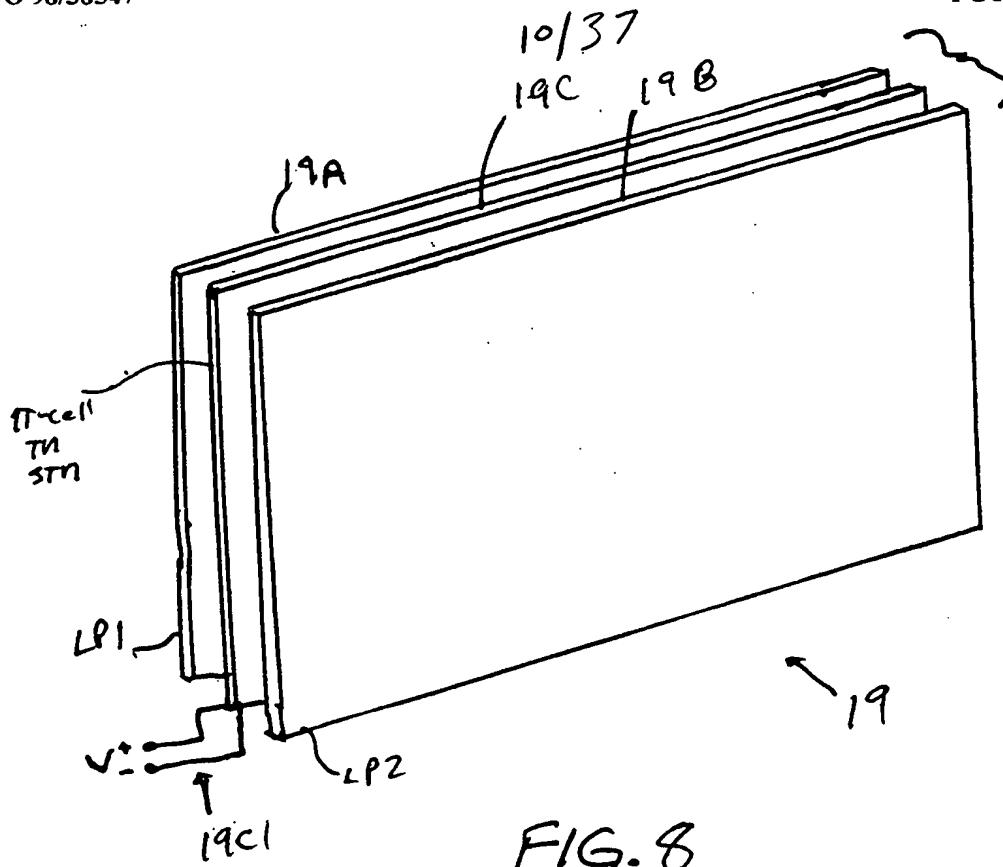


FIG. 8

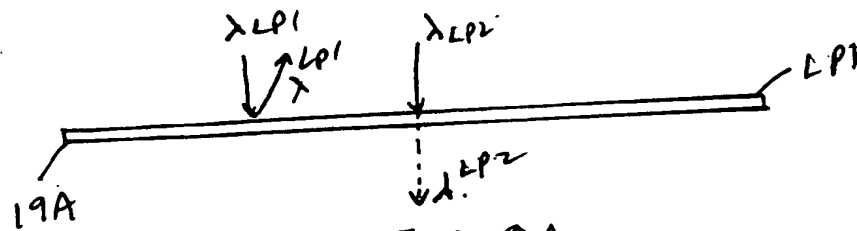


FIG. 8A

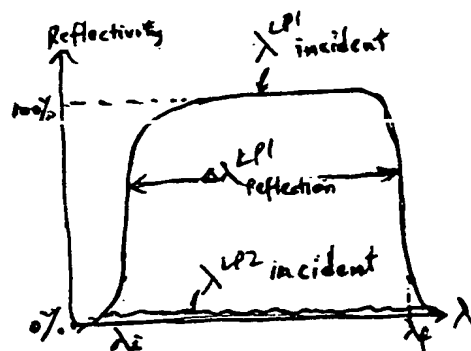


FIG. 8.B



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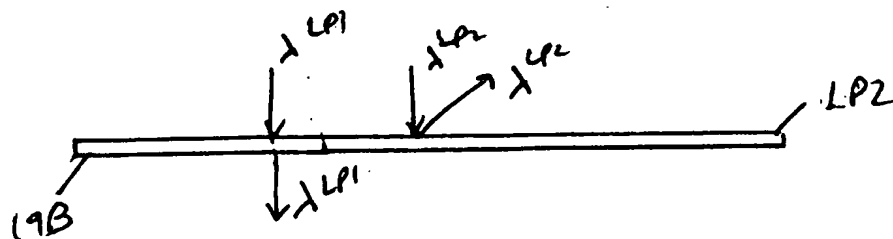


FIG. 8C

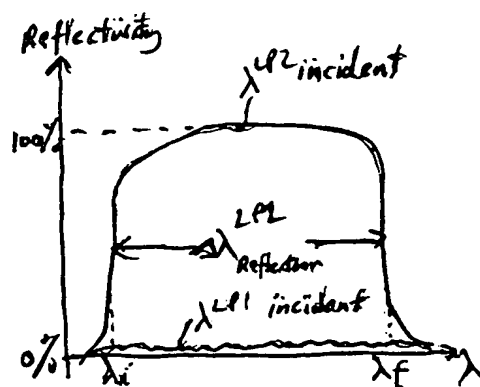


FIG. 8D

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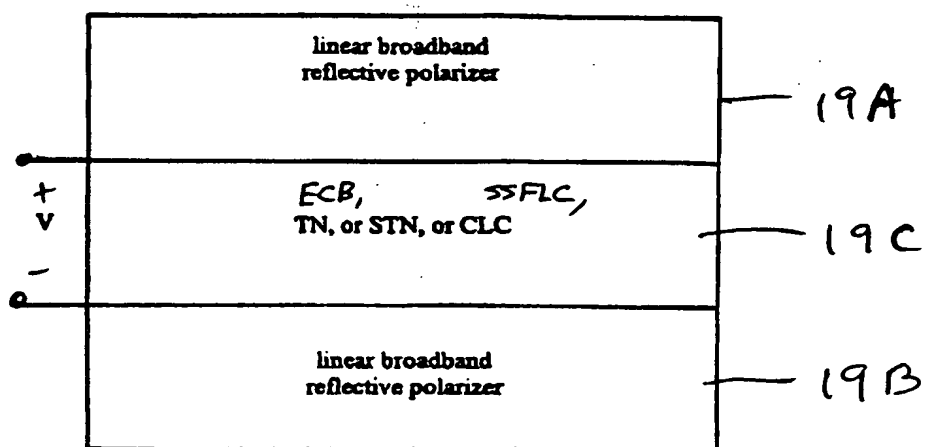
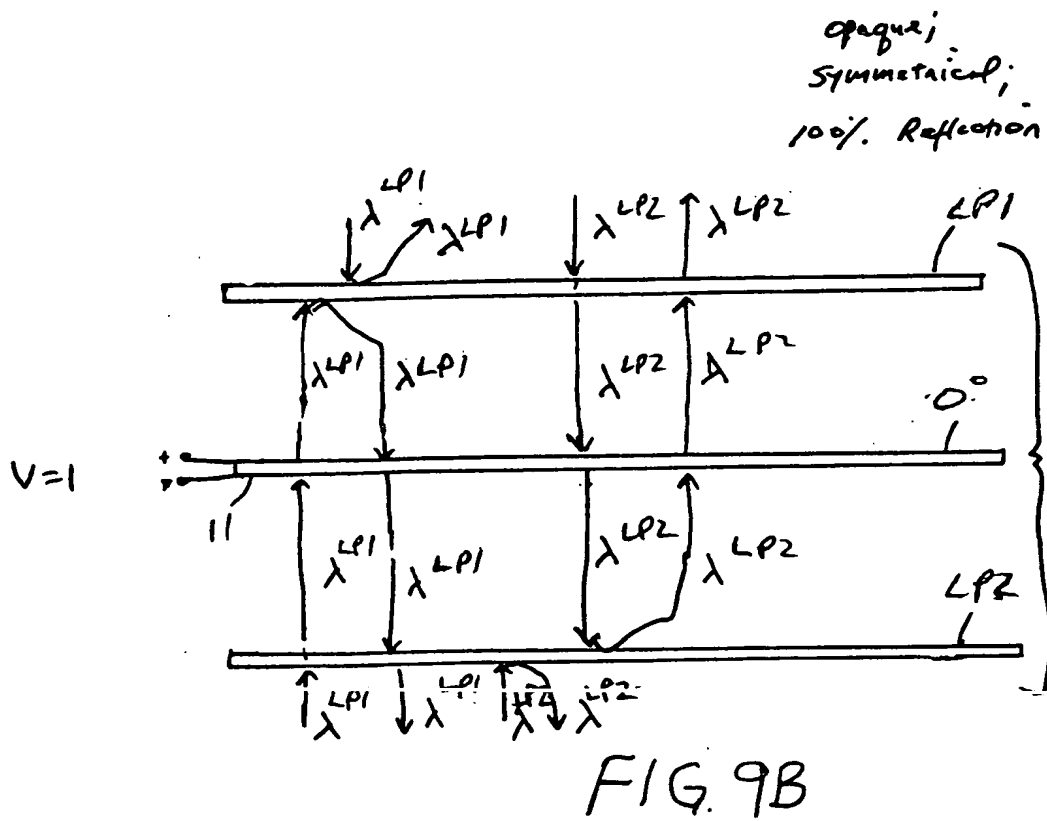
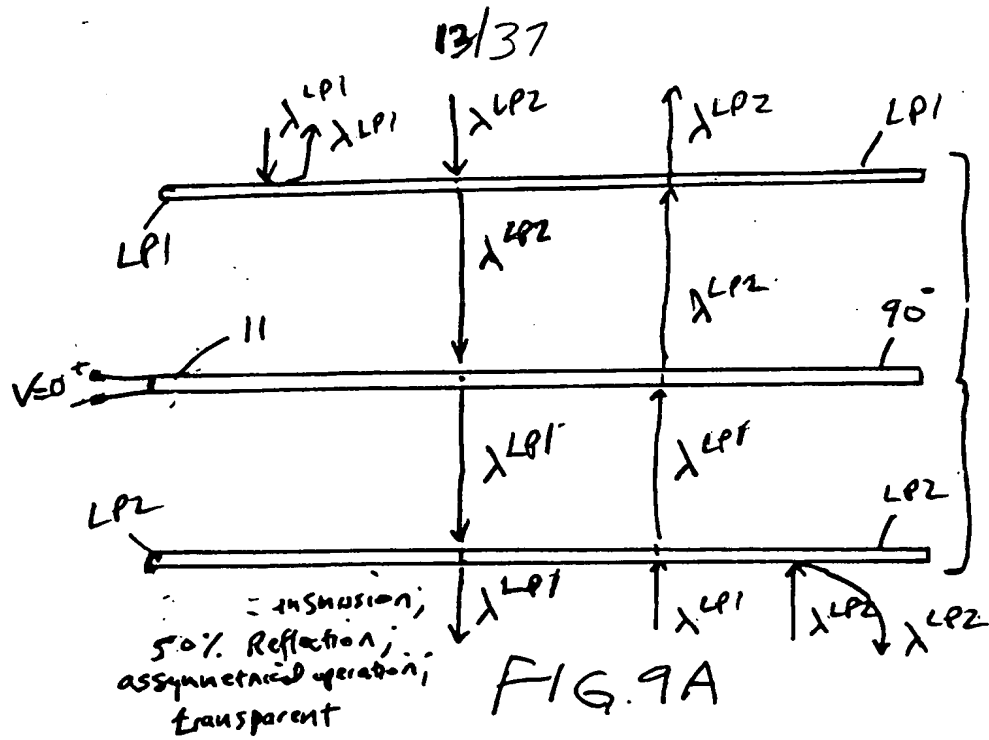


FIG. 8E



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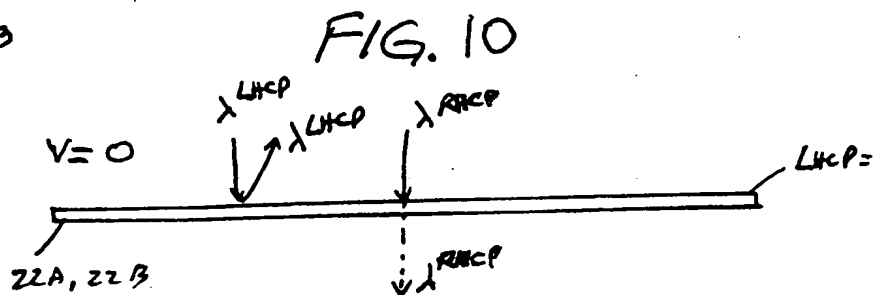
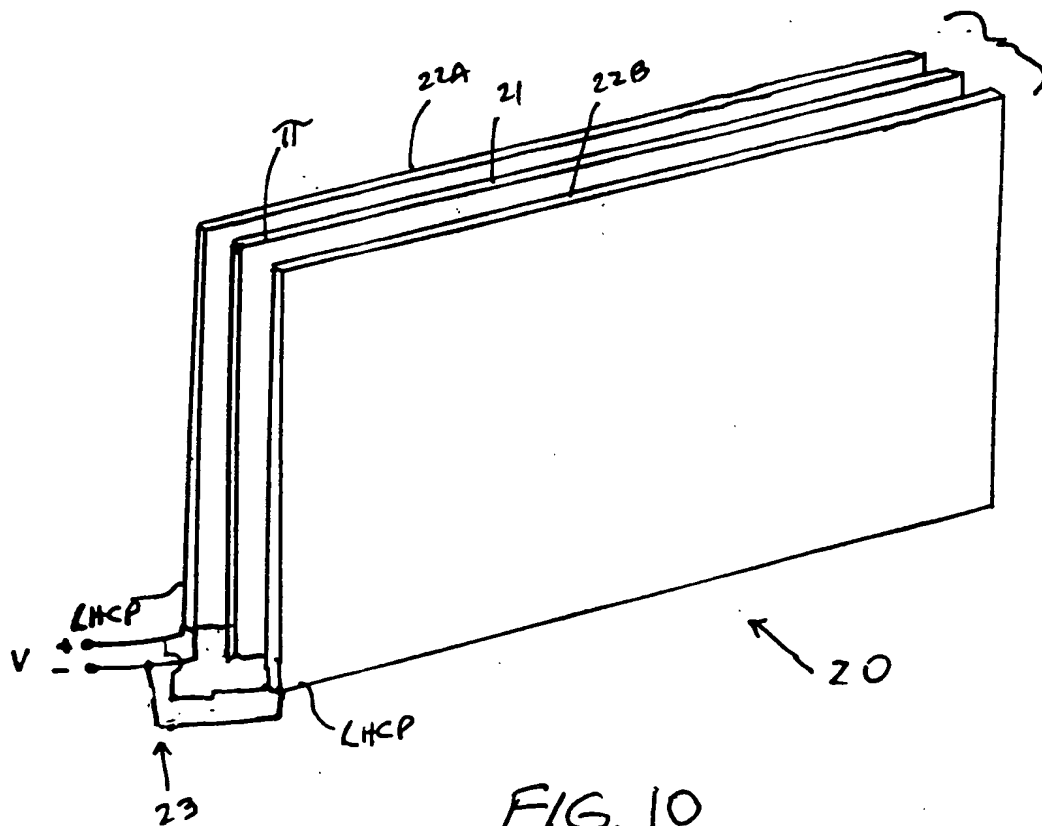


FIG. 10A

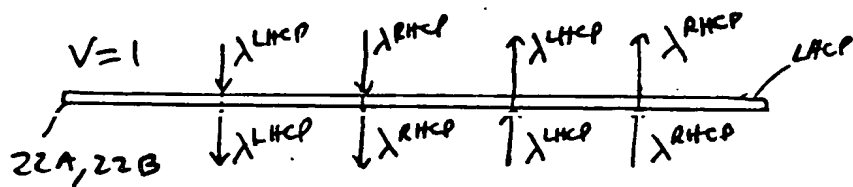


FIG. 10B

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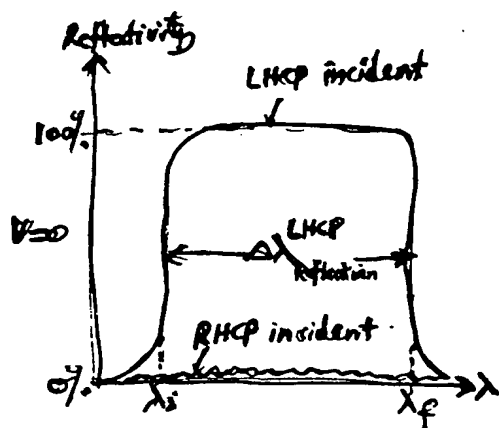


FIG. 10C

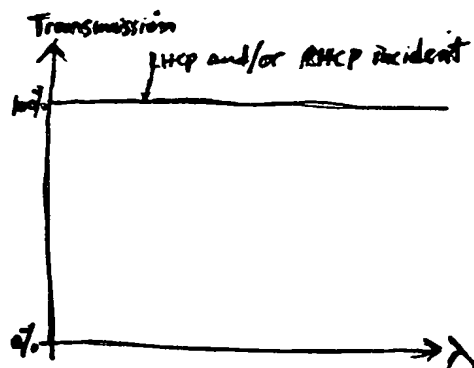


FIG. 10D

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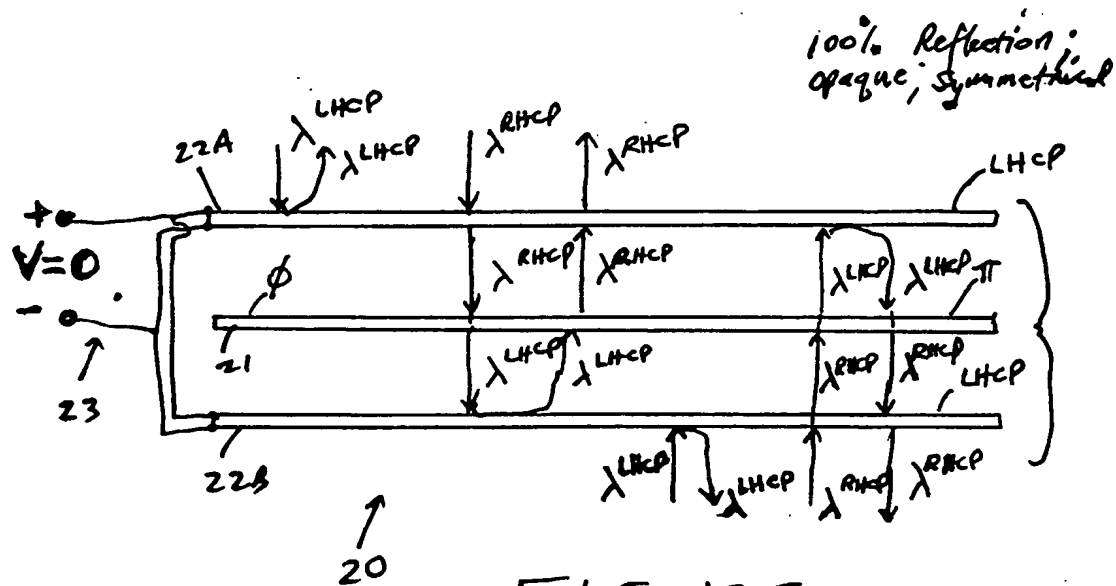


FIG. 10E

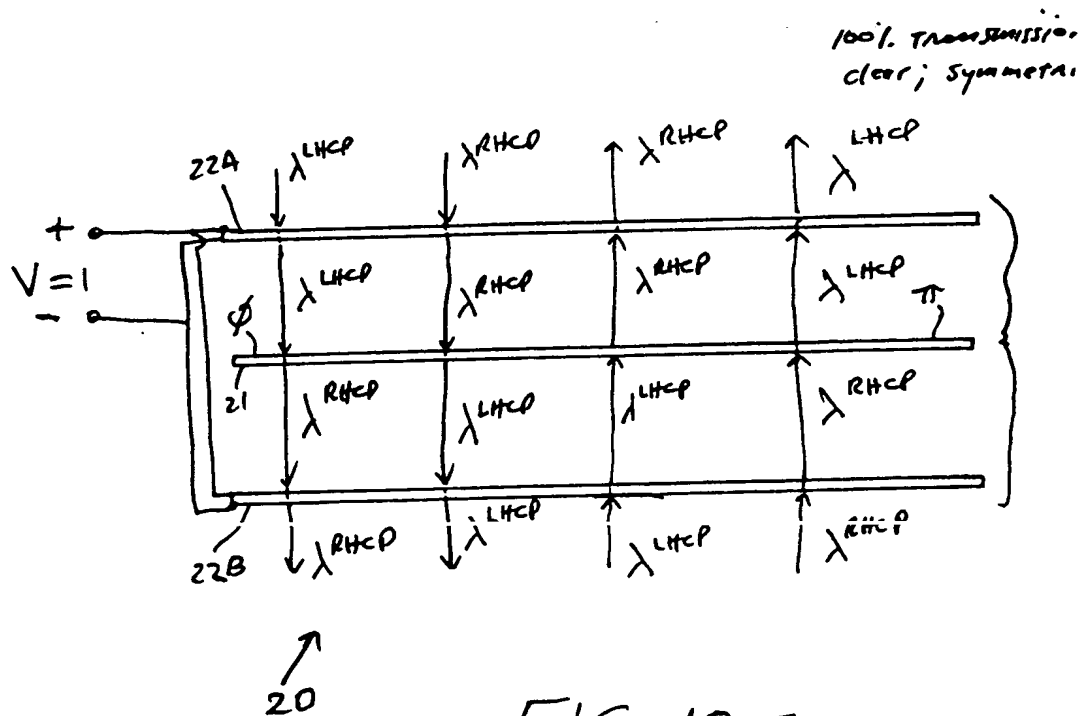


FIG. 10F

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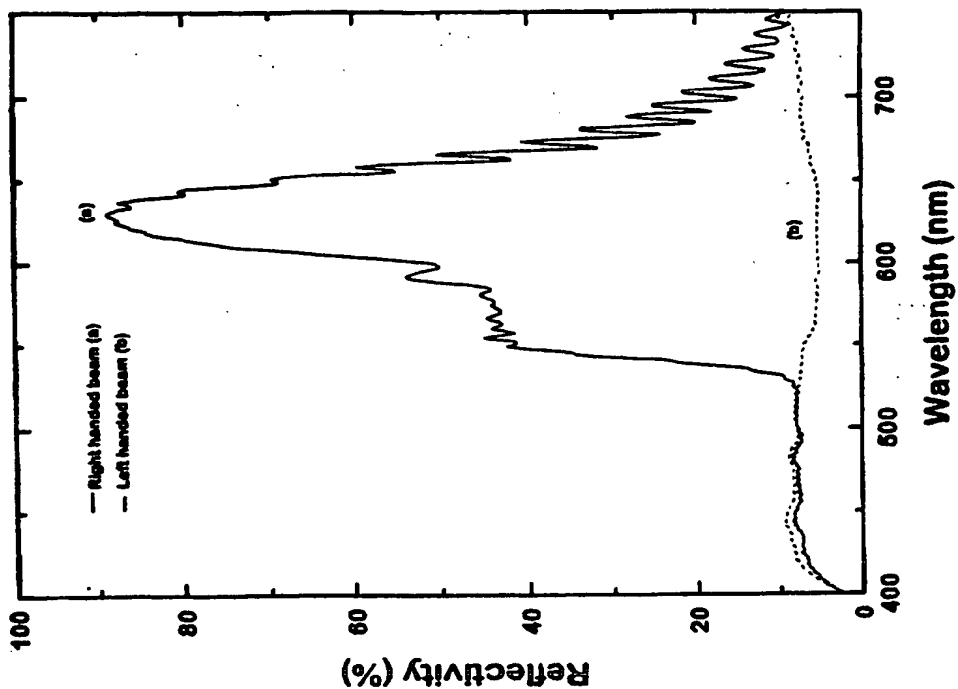


FIG. 11A2

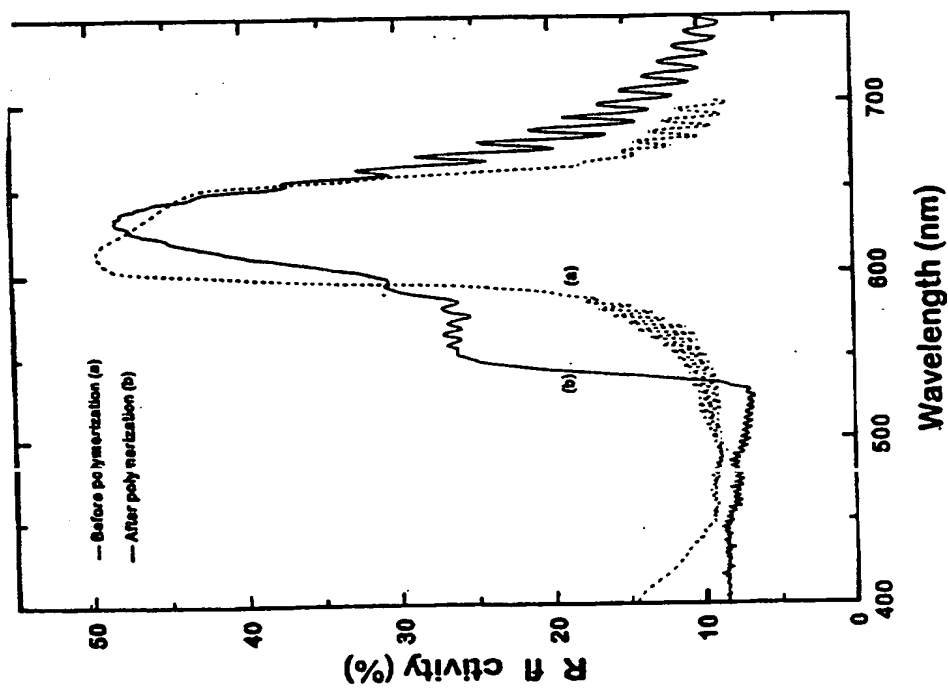


FIG. 11A1

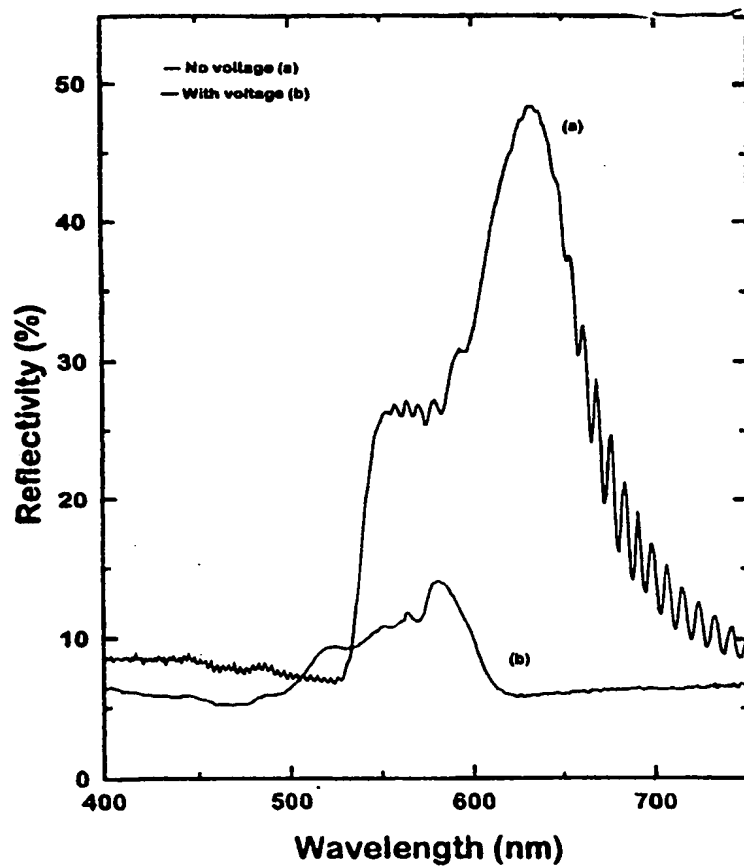
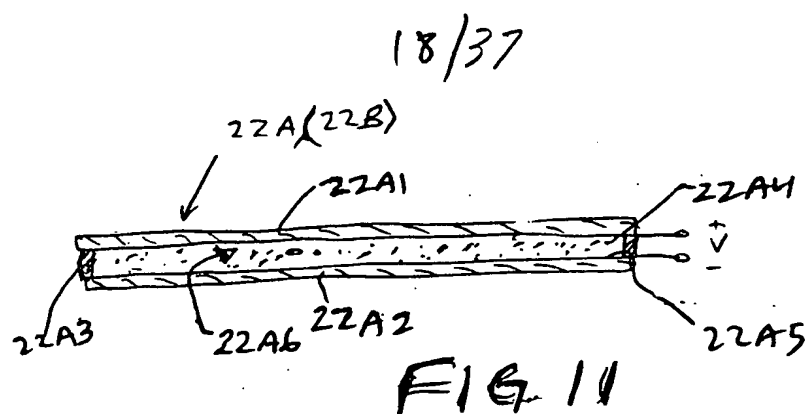
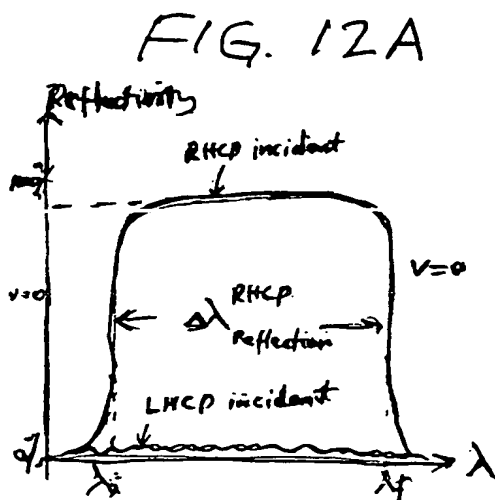
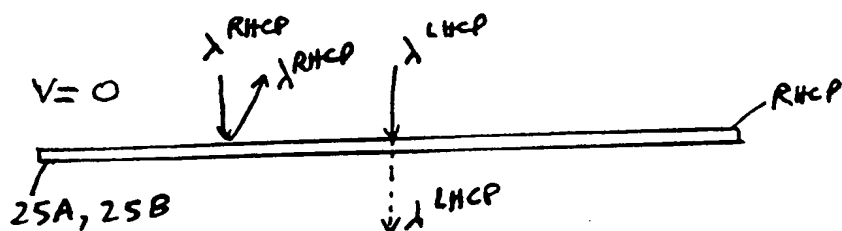
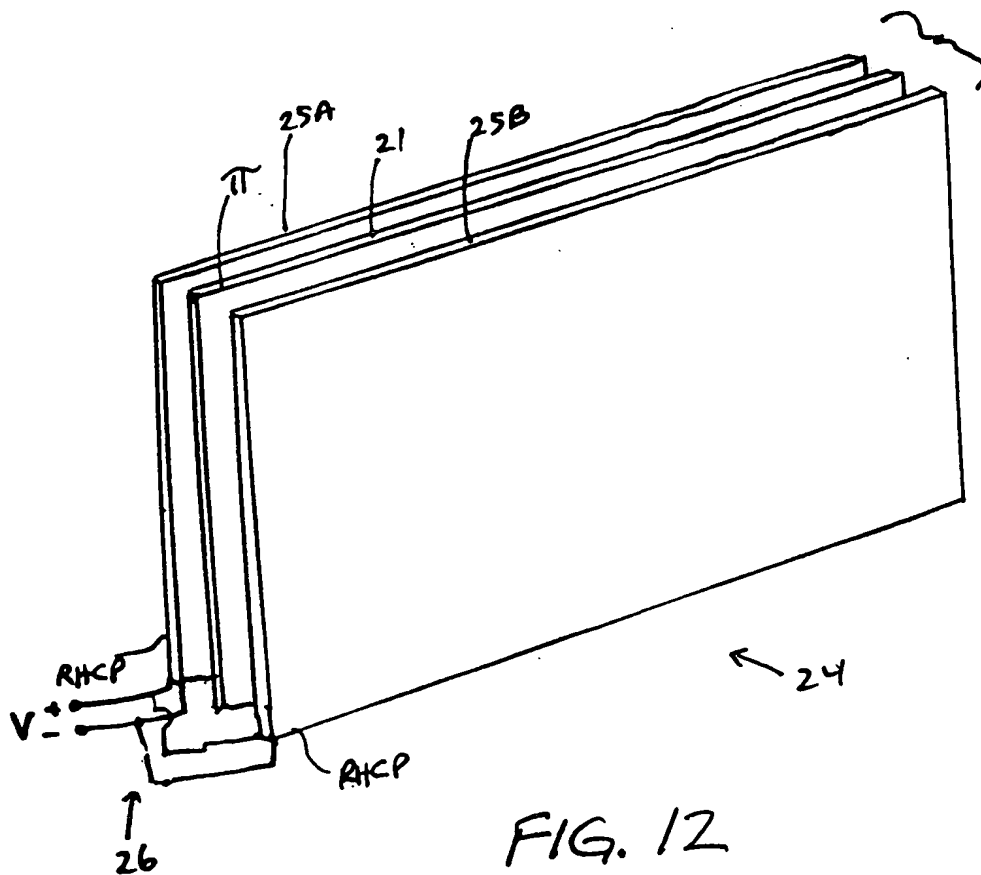


FIG. 11A3



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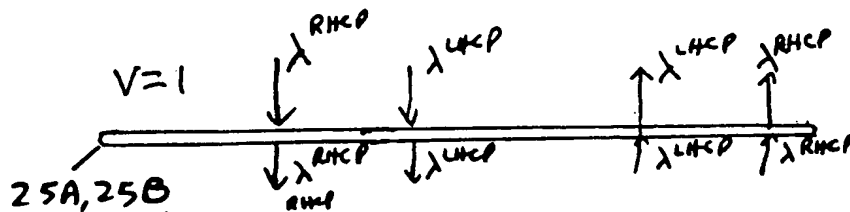


FIG. 12C

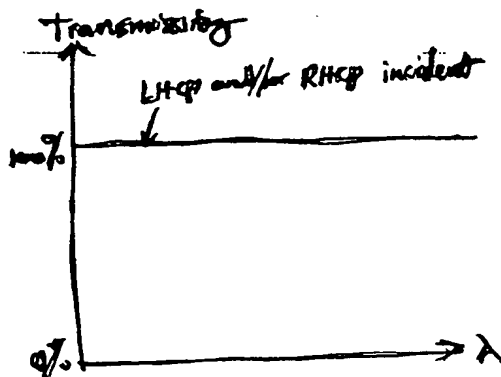


FIG. 12D

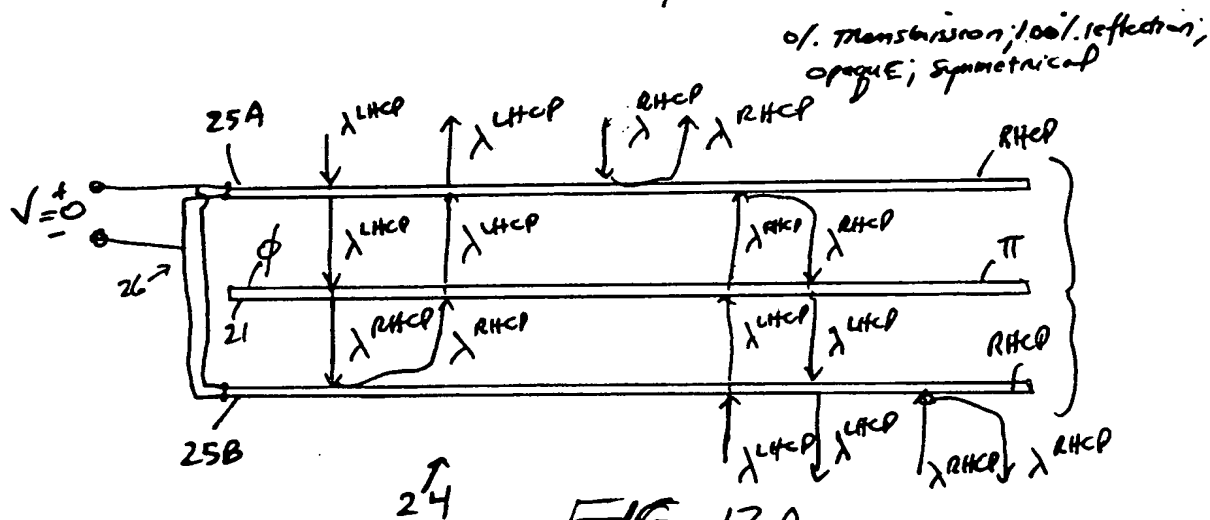


FIG. 13A

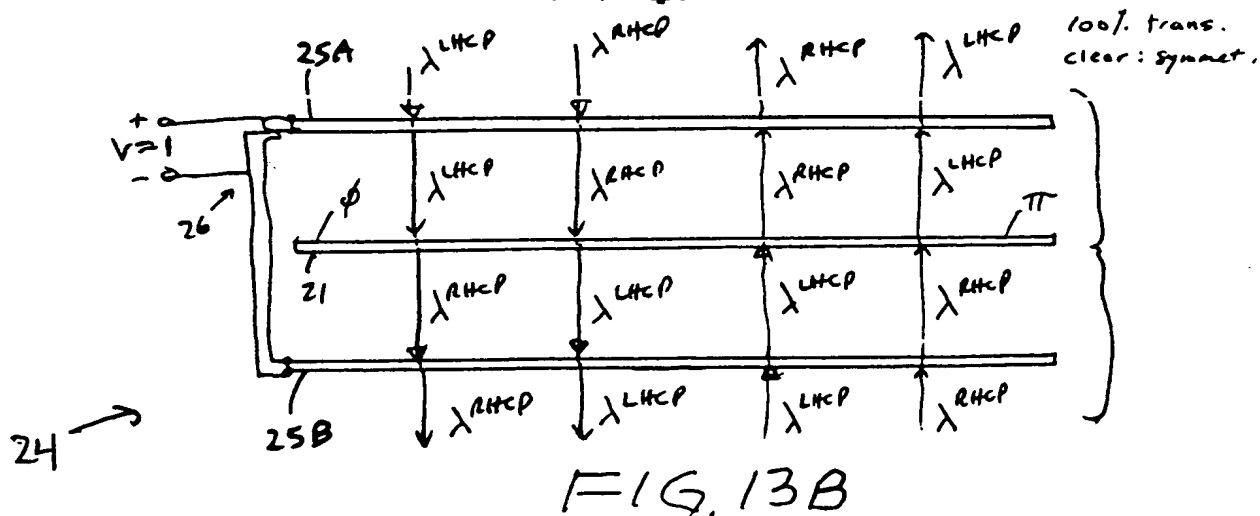
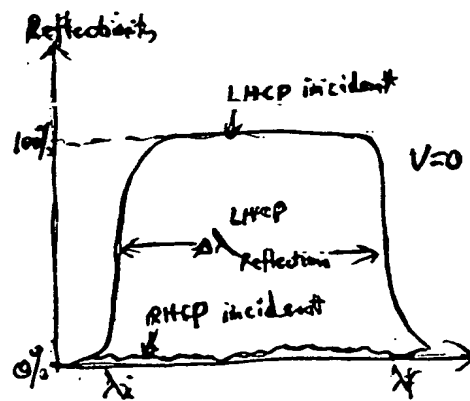
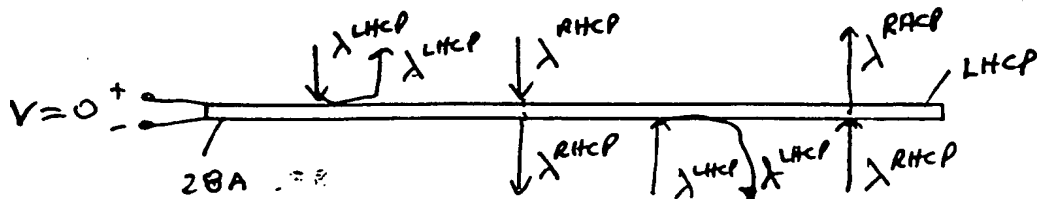
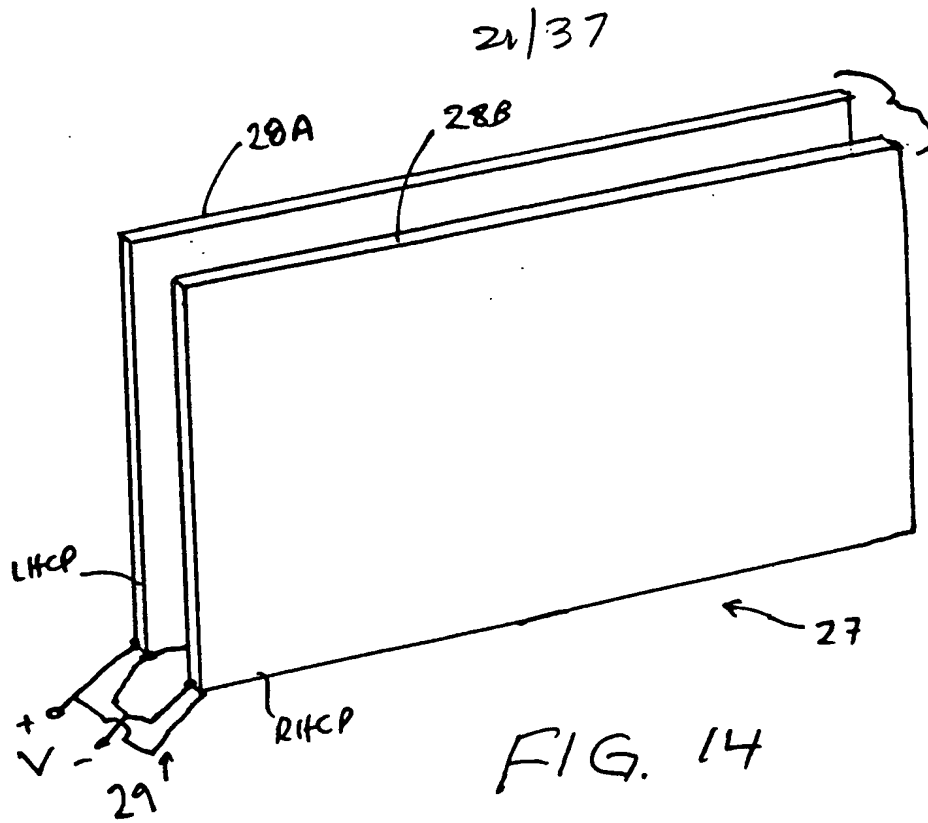


FIG. 13B



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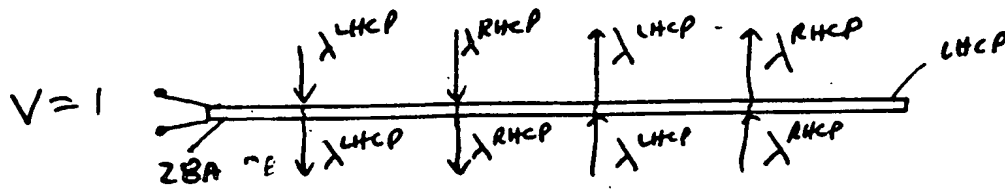


FIG. 14C

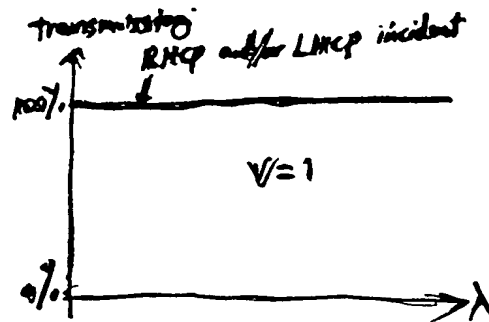


FIG. 14D

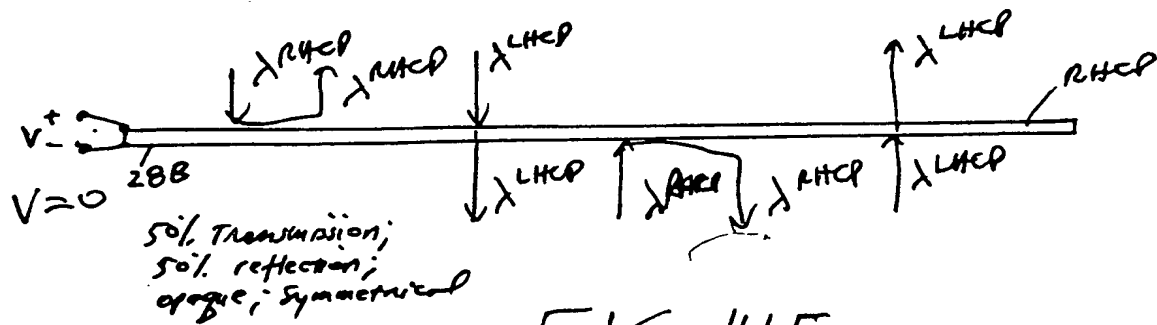


FIG. 14E

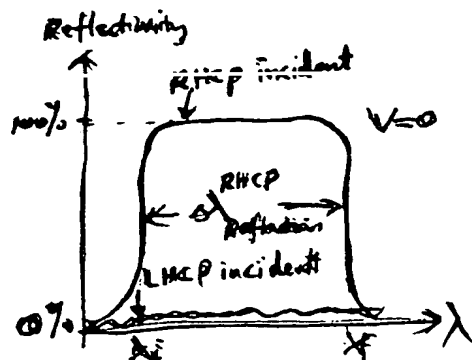


FIG. 14F

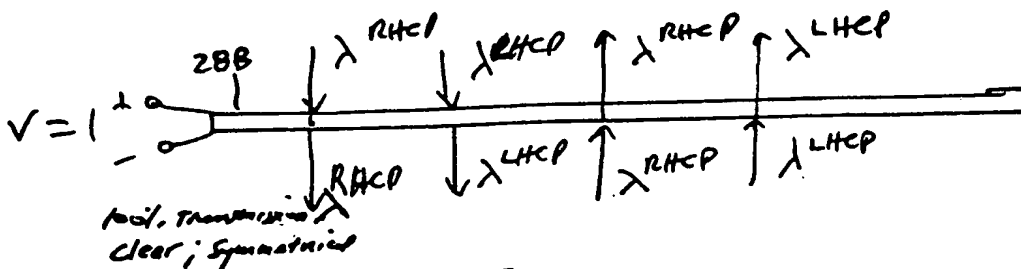


FIG. 14G

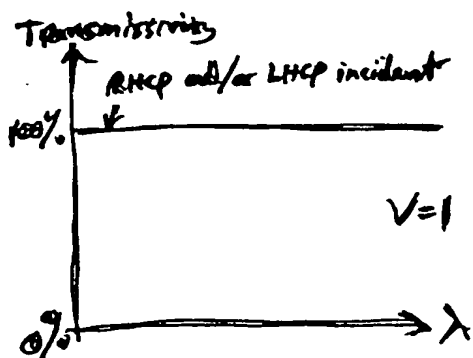


FIG. 14H

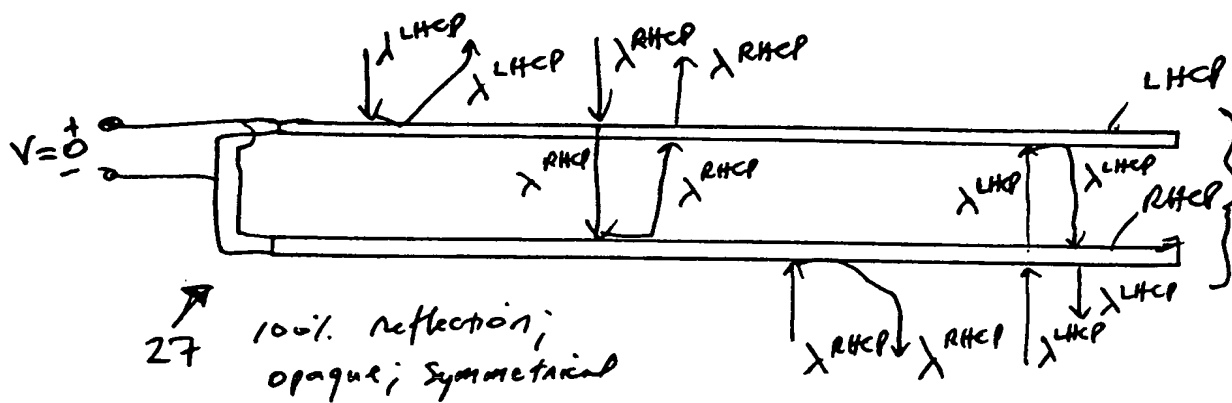


FIG. 15A

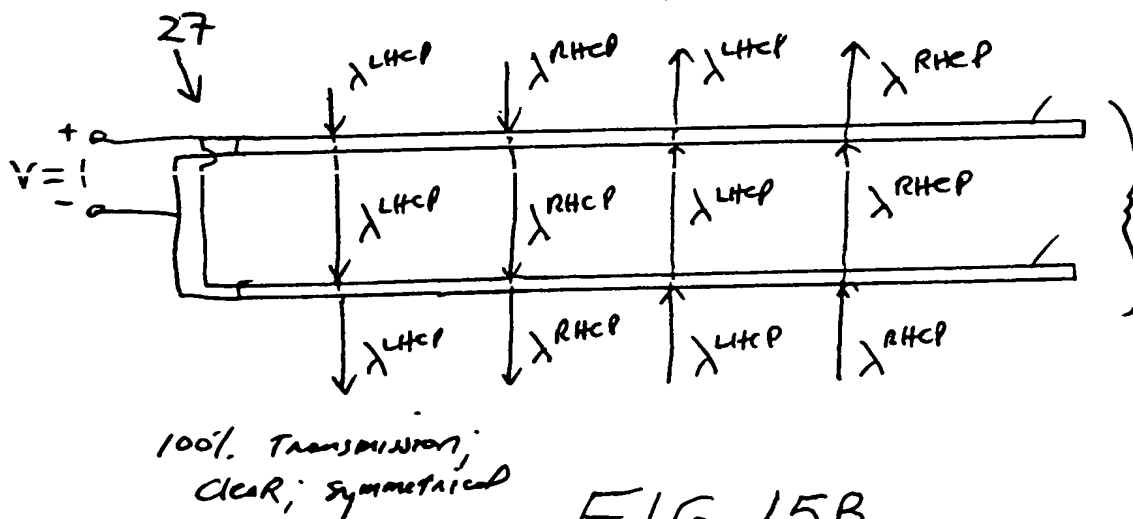
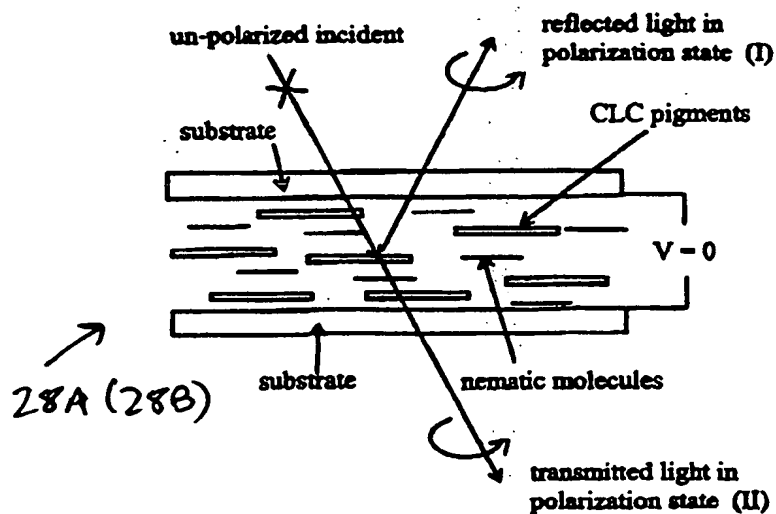


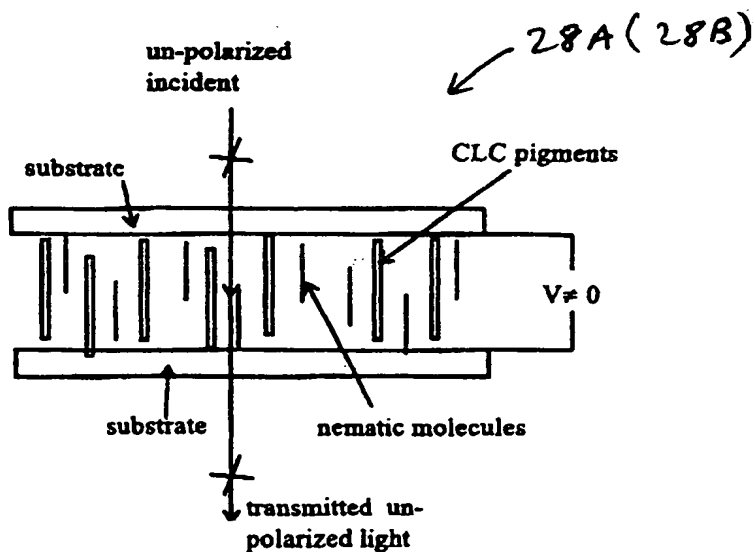
FIG. 15B

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Homogeneous alignment of host nematic molecules and parallel orientation of the CLC pigments;

FIG. 16A



homeotropic alignment of the nematic under an electric field and a vertical orientation of the CLC pigments.

FIG. 16B

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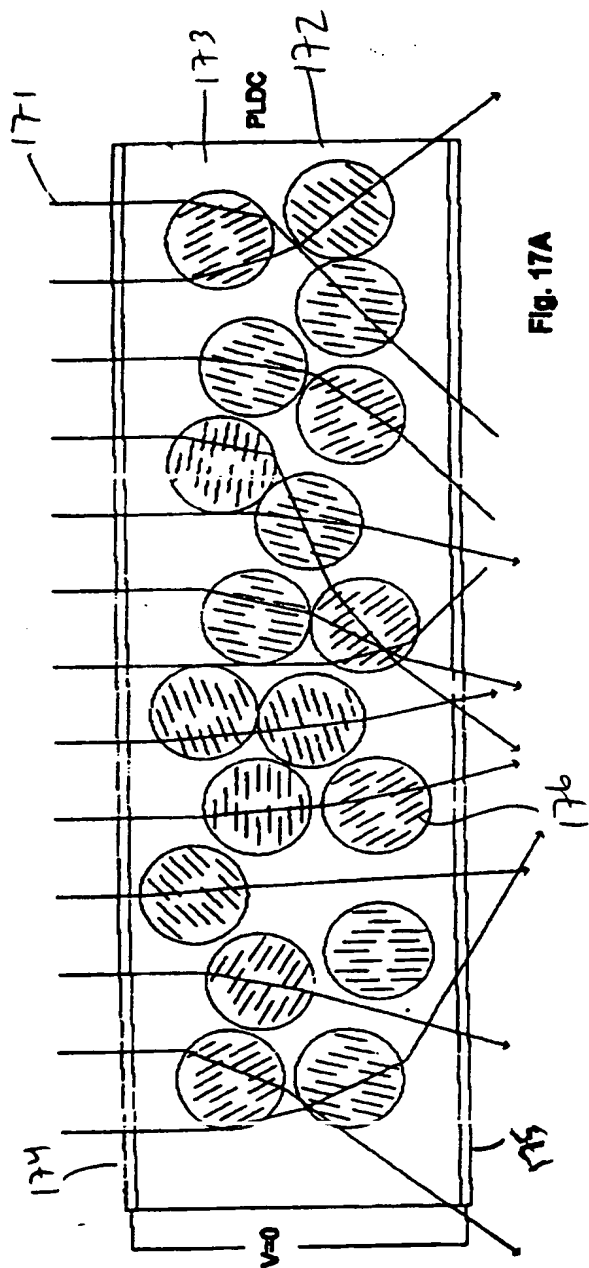


Fig. 17A

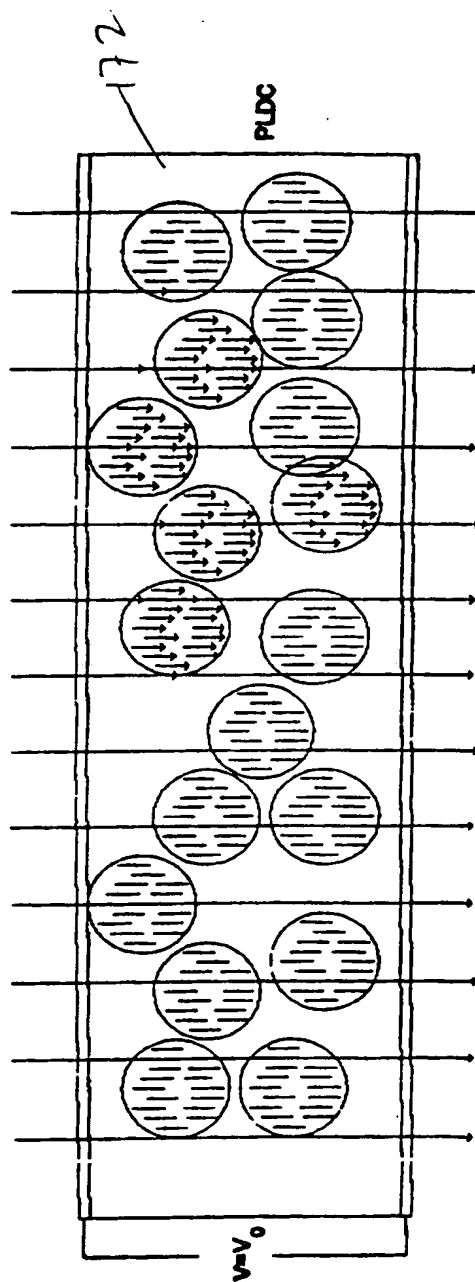


Fig. 17B

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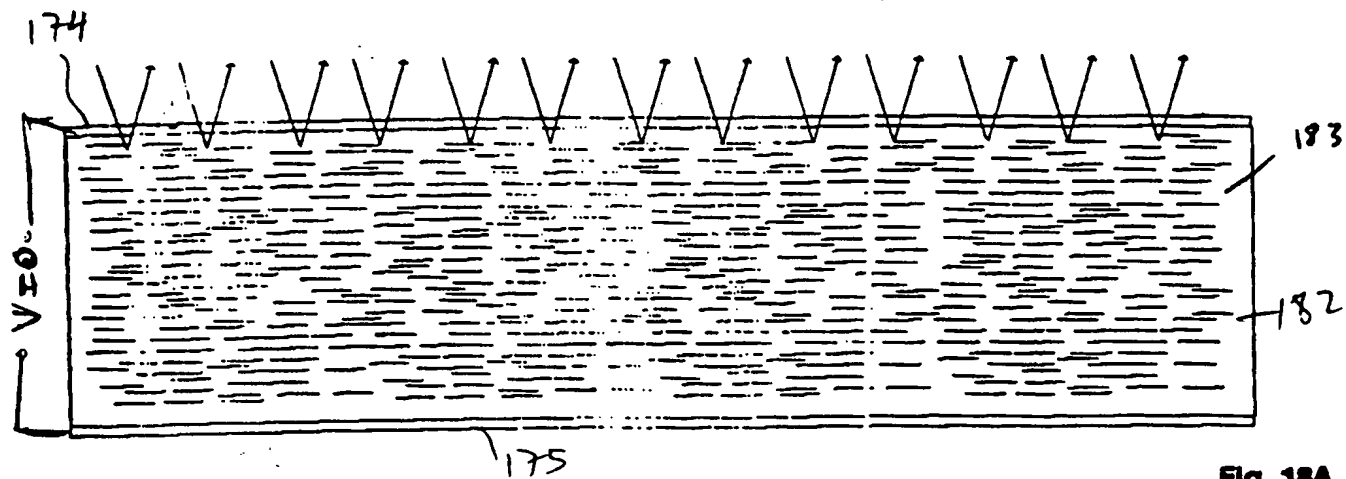


Fig. 18A

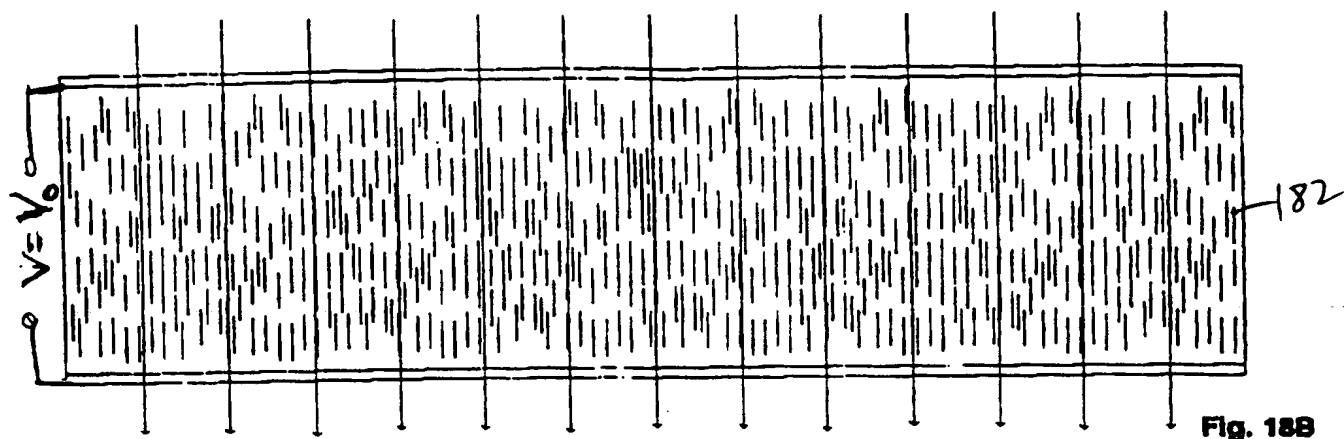


Fig. 18B

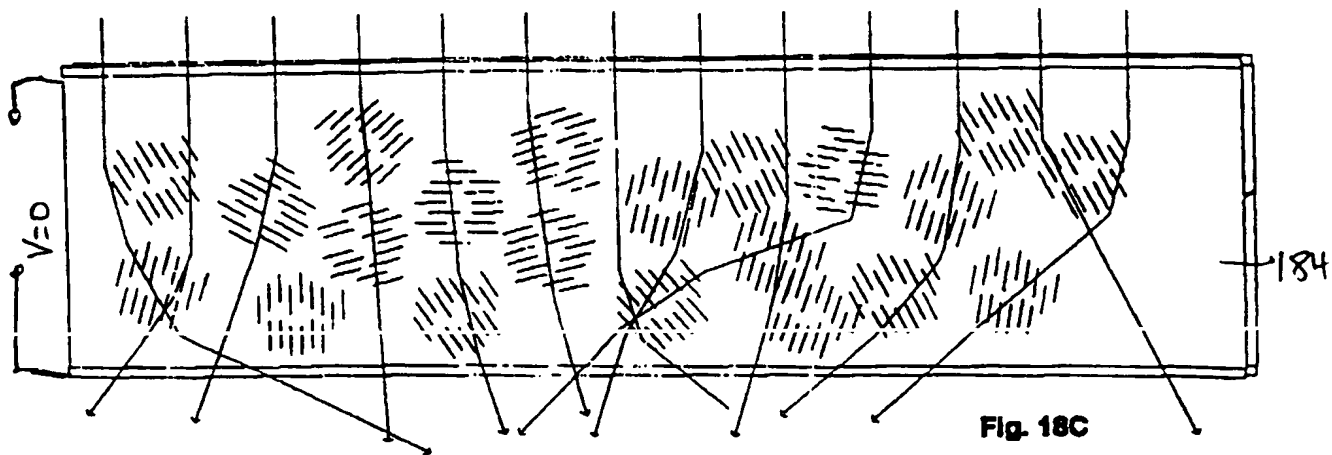


Fig. 18C



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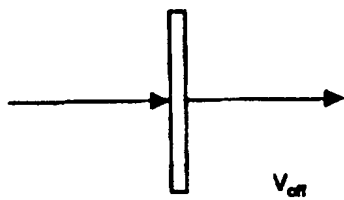


FIG. 19A

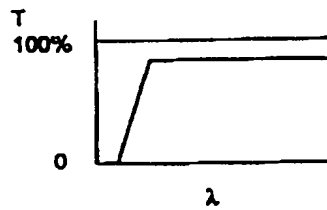


FIG. 19B

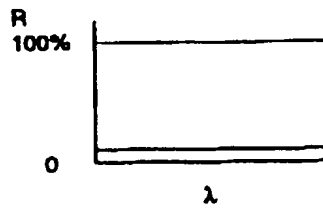


FIG. 19C

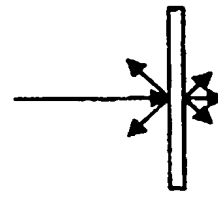


FIG. 19D

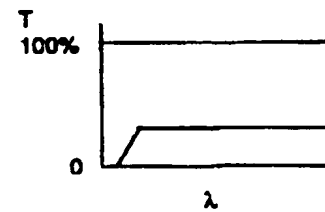


FIG. 19E

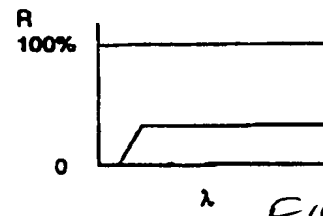


FIG. 19F

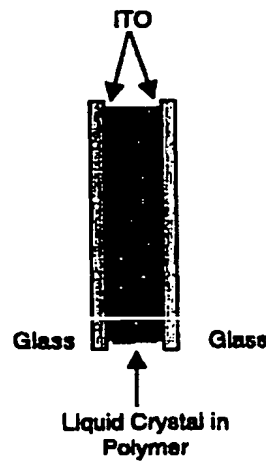


FIG. 19

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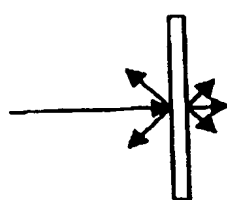
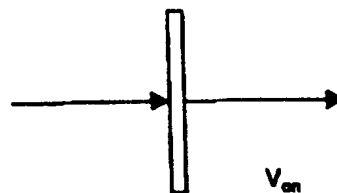
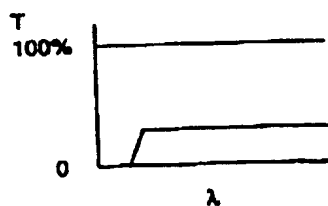
V<sub>off</sub> FIG. 20AV<sub>on</sub> FIG. 20D

FIG. 20B

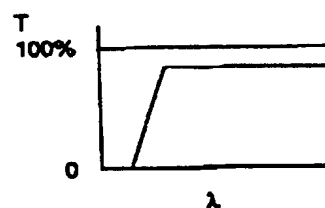


FIG. 20E

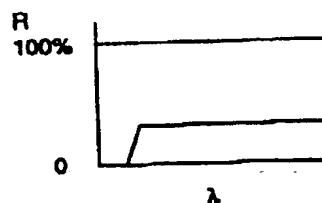


FIG. 20C

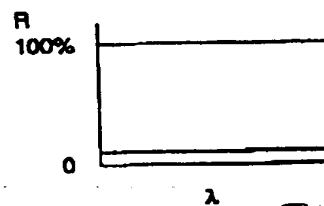


FIG. 20F

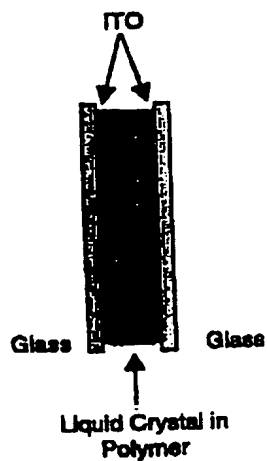
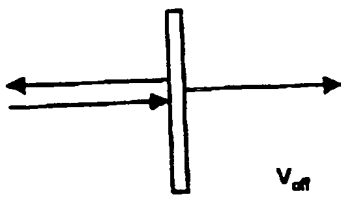
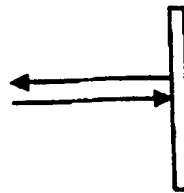


FIG. 20

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$v_{eff}$  FIG. 21A



$v_{eff}$  FIG. 21D

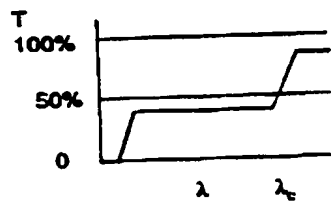


FIG. 21B

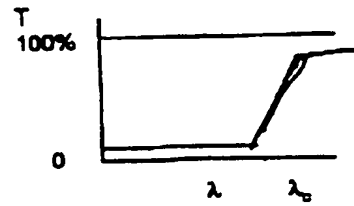


FIG. 21E

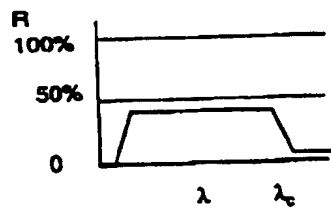


FIG. 21C

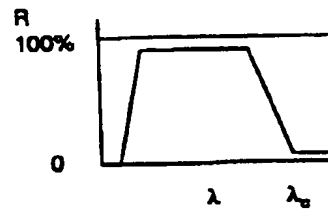


FIG. 21F

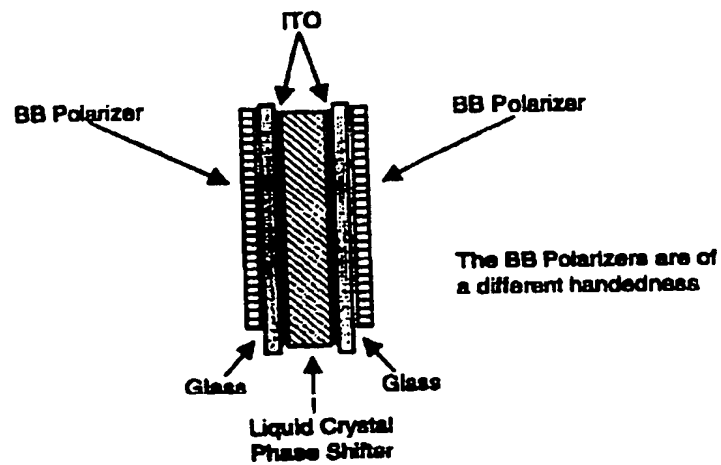


FIG 21

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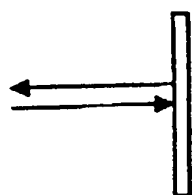


FIG. 22A

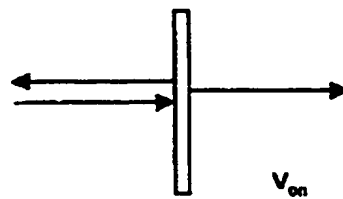


FIG. 22D

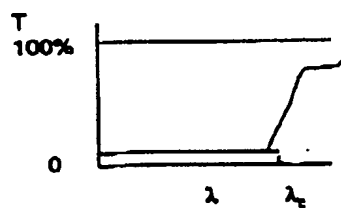


FIG. 22B

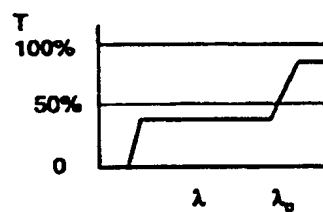


FIG. 22E

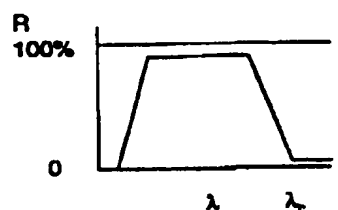


FIG. 22C

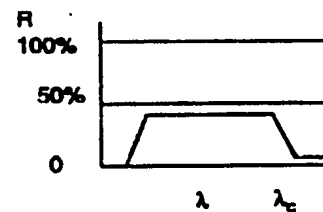


FIG. 22F

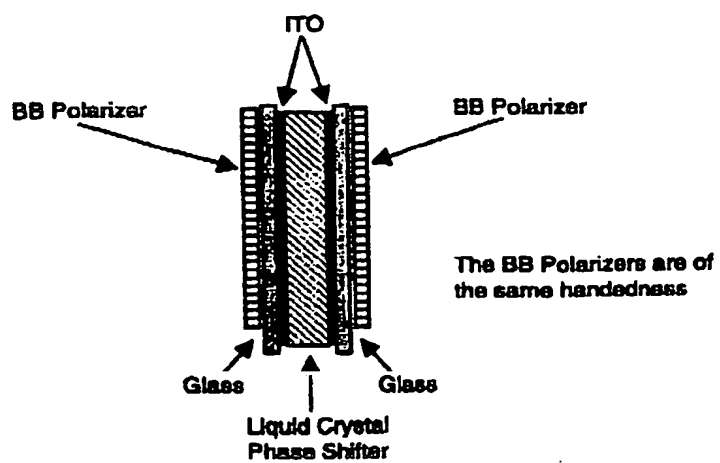
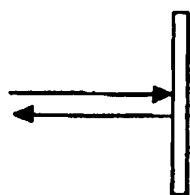
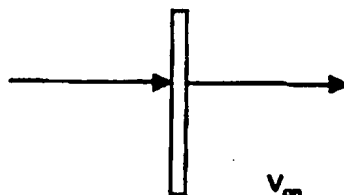


FIG. 22

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$V_{on}$  FIG. 23A



$V_{on}$  FIG. 23D

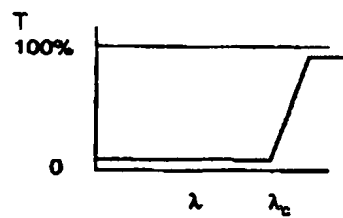


FIG. 23B

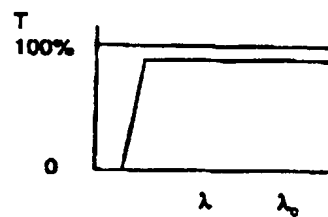


FIG. 23E

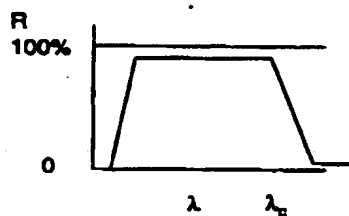


FIG. 23C

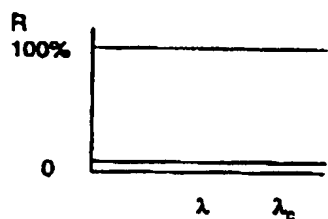


FIG. 23F

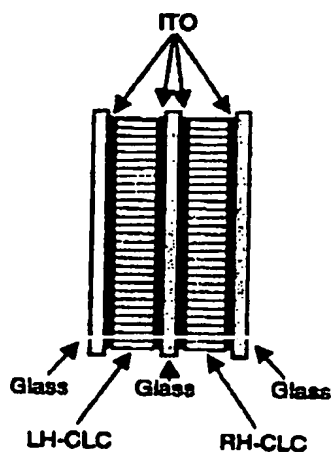
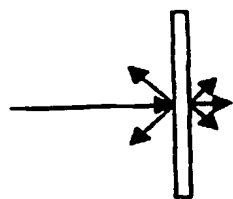
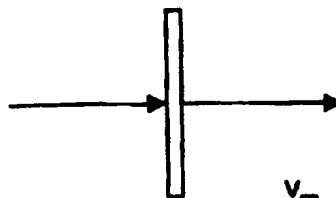


FIG. 23

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$V_{\text{off}}$  FIG 24A



$V_{\text{on}}$  FIG 24D

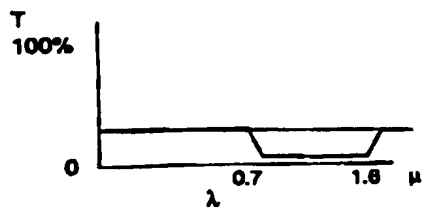


FIG 24B

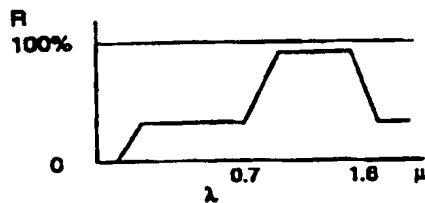


FIG 24C

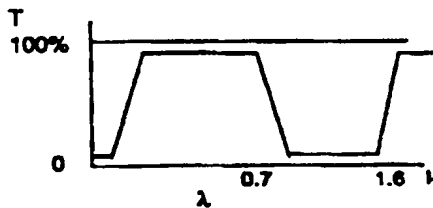


FIG 24E

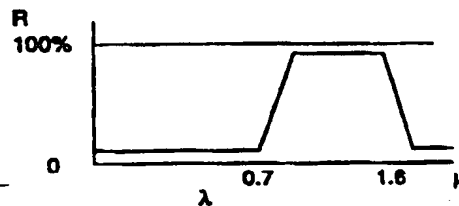


FIG 24F

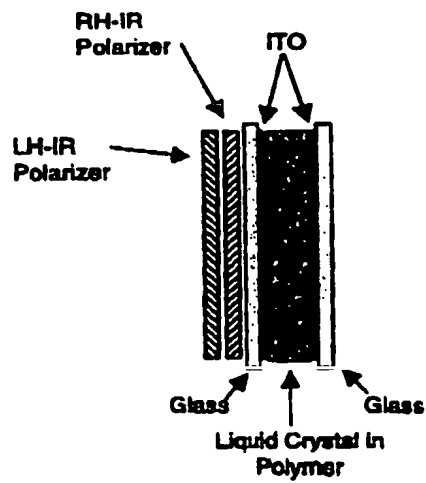
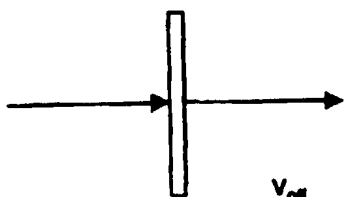
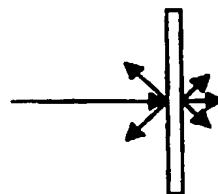


FIG 24

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$V_{off}$  FIG. 25A



$V_{on}$  FIG. 25D

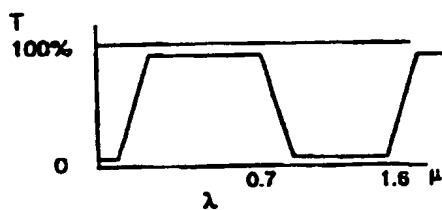


FIG. 25B

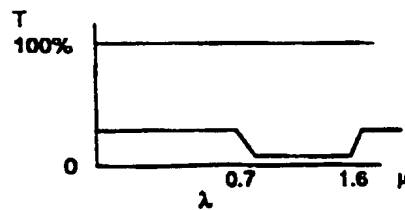


FIG. 25E

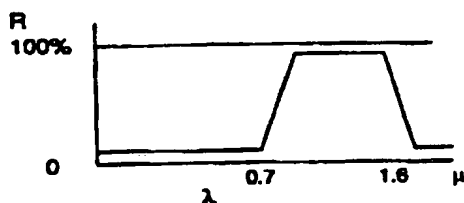


FIG. 25C

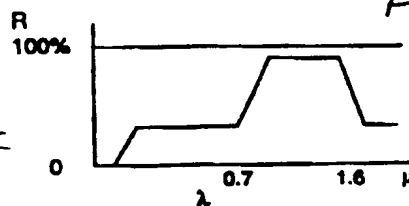


FIG. 25

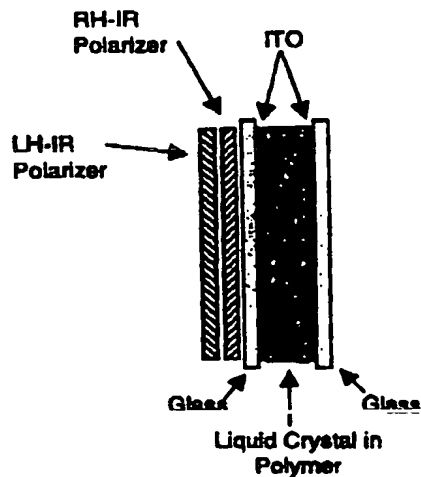
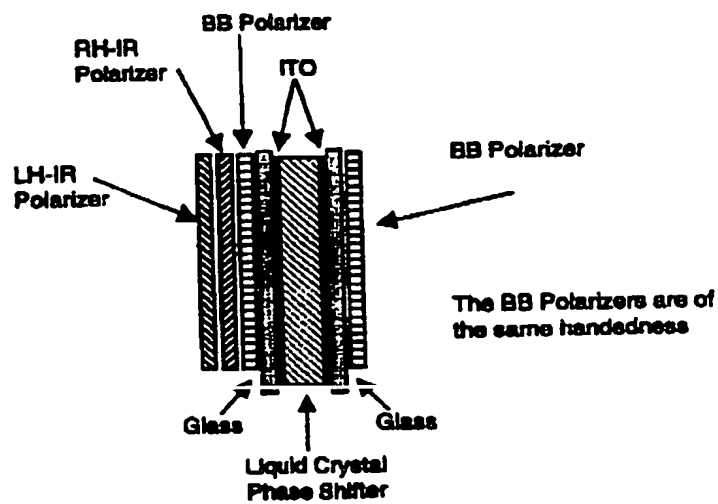
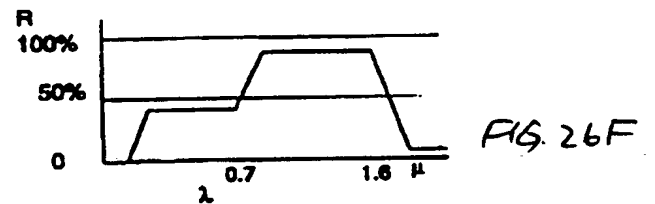
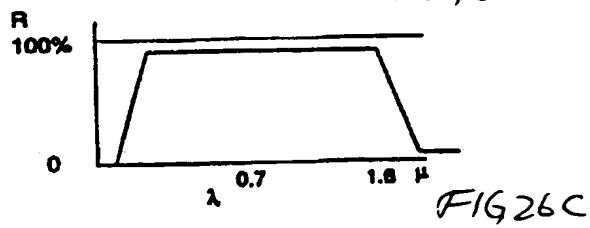
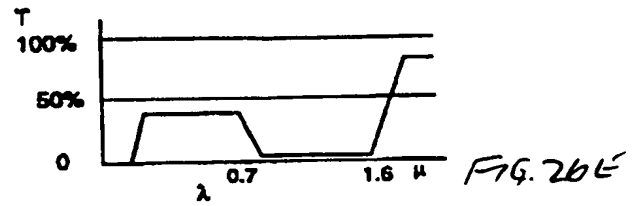
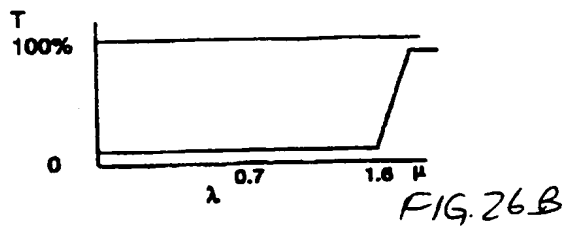
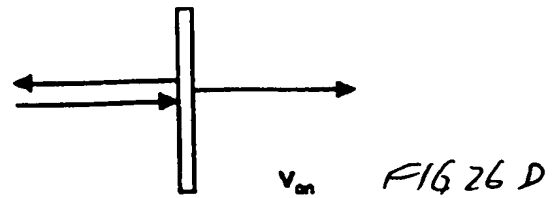
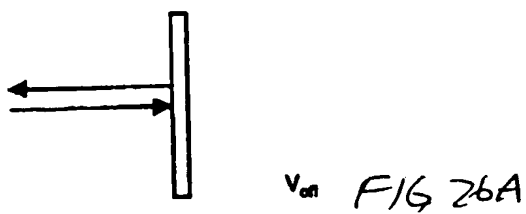


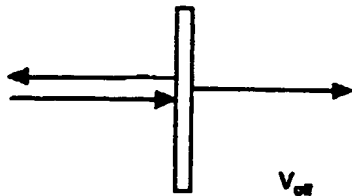
FIG. 25

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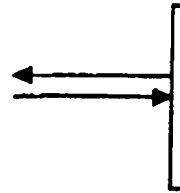




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$V_{\text{on}}$  FIG 27A



$V_{\text{on}}$  FIG 27D

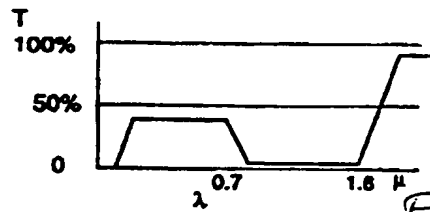


FIG 27B

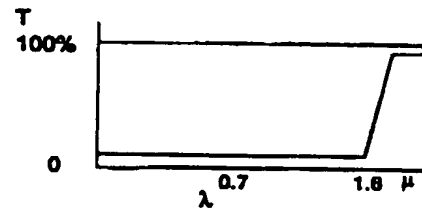


FIG 27E

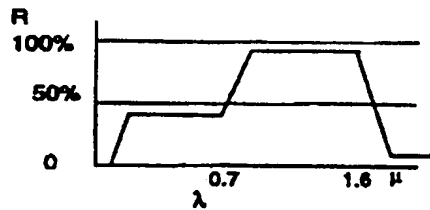


FIG 27C

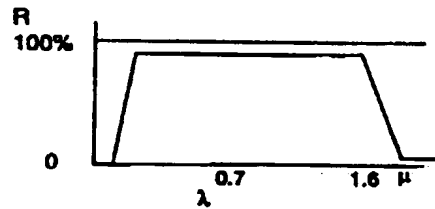


FIG 27F

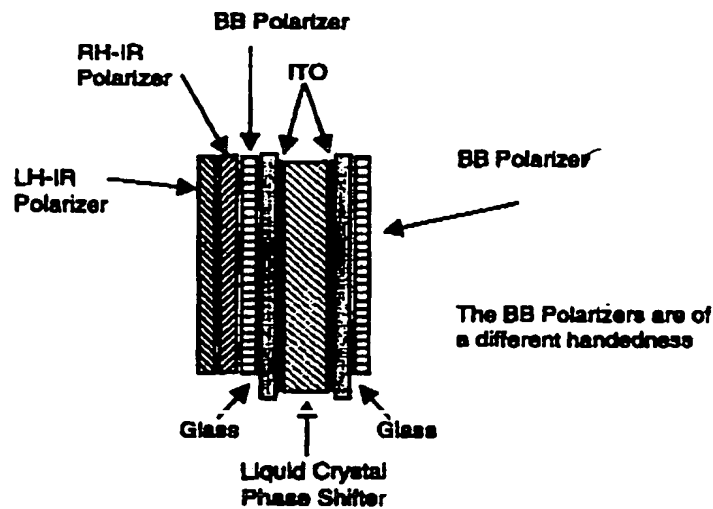


FIG 27

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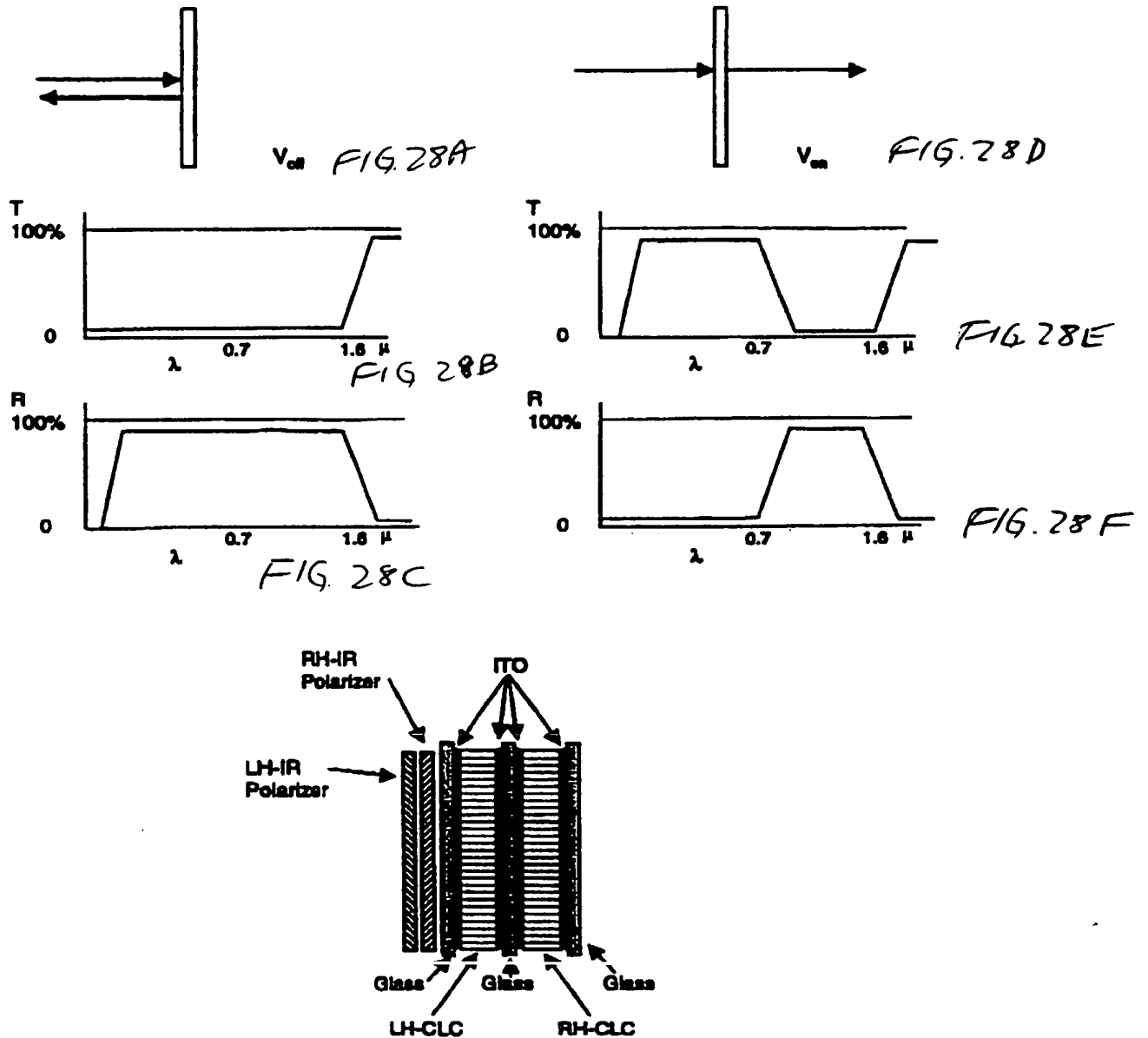


FIG. 28

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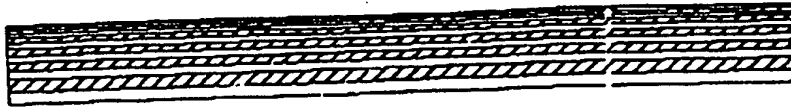


FIG. 29A

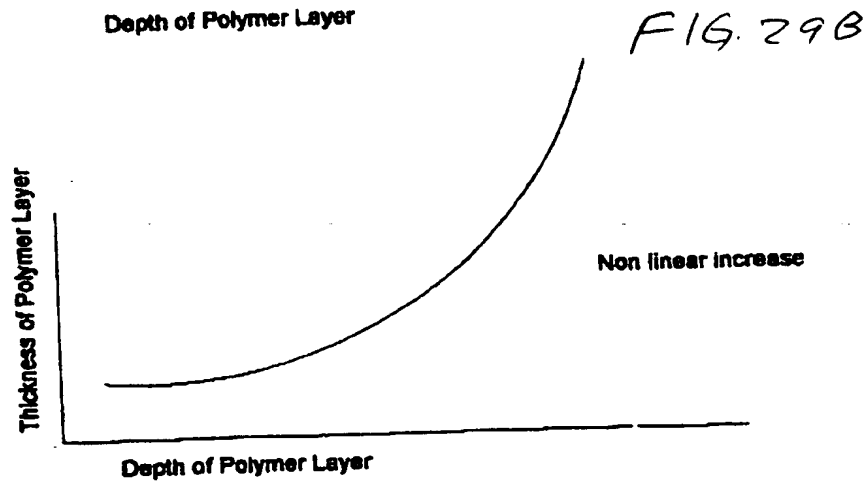
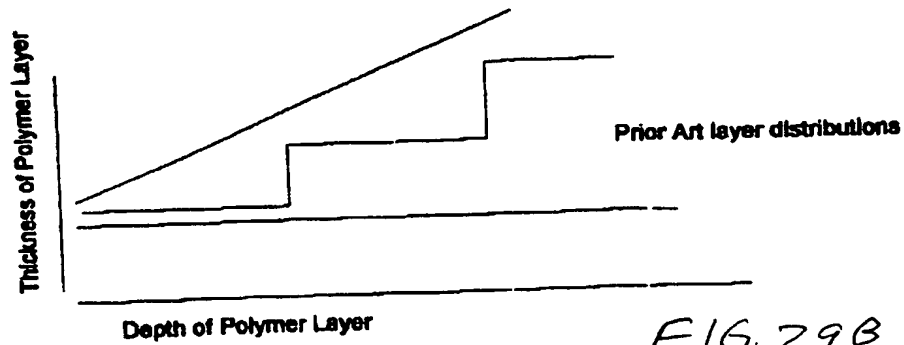


FIG 29C